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JANUARY 1990

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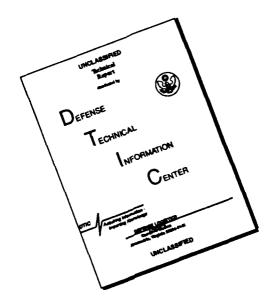
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JANUARY 1990

PREPARED BY NAVAL OCEANOGRAPHY COMMAND DETACHMEN ASHEVILLE, NC

PREPARED UNDER THE AUTHORITY OF COMMANDER, NAVAL OCEANOGRAPHY COMMAI STENNIS SPACE CENTER, MS 39529-5000

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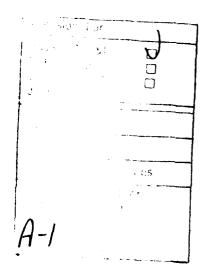
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FOREWORD

The U.S. Navy Hindcast Spectral Ocean Wave Model Climatic Atlas: Mediterranean Sea was prepared for the Commander, Naval Oceanography Command (CNOC) by the Officer in Charge, Naval Oceanography Command Detachment, Asheville, North Carolina. The work was performed in Asheville at the National Oceanic and Atmospheric Administration's (NOAA) National Climatic Data Center (NCDC).

Special acknowledgement is given to the following named meteorologists of Global Climate Laboratory (GCL): Peter M. Steurer for serving as project leader; Phala Franks for performing the parameterization of the data; and Thomas R. Karl who was instrumental in completion of work on the project. Specific acknowledgement is also made to GCL's Ronald G. Baldwin, computer programmer/analyst, for production of the computer-generated graphic presentation, and Michael G. Burgin and Scott J. Miller, Meteorological Technicians, for their drafting skills in preparation of this publication for printing.





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		ISOPLETHS	JAN
		WIND SPEED (≤ 10 and ≥ 34 KNOTS)	1
		WAVE HEIGHT (<5 and <8 FEET)	14
		WAVE HEIGHT (≥ 12 and ≥ 20 FEET)	27
		WAVE SLOPE (a) (≤ 0.05 and ≥ 0.10)	40
TABLE OF CONTENTS		CONTINGENCY TABLES	
		WIND DIRECTION AND SPEED	53
	Page	WAVE HEIGHT AND WIND SPEED	66
Foreword	iii	WAVE HEIGHT AND WAVE SLOPE (α)	92
Background	v	WAVE HEIGHT AND PERIOD	118
Overview	vi		
Isopleth Presentations	1-52	WAVE HEIGHT AND DIRECTIONALITY	144
Contingency Tables	53-208	WAVE HEIGHT AND PRIMARY WAVE DIRECTION	170
Duration-Interval Tables	209-298	PRIMARY WAVE DIRECTION AND WIND DIRECTION	196
Appendix A-SOWM Development	299-300	PRIMARY WAVE DIRECTION AND WIND DIRECTION	190
Appendix B-Parameter Derivations	301-303	DURATION-INTERVAL TABLES	
Appendix C-Some Applications of		DONATION INTERVAL TRADES	
Contingency Tables	304-305	WIND SPEED DURATION	
Appendix D-Duration and Interval Tables	306-308	WIND SPEED INTERVALS	
Bibliography	309	WAVE HEIGHT DURATIONS	
		WAVE HEIGHT INTERVALS	
		WAVE SLOPE (a) DURATIONS	
		WAVE SLOPE (a) INTERVALS	

iv /

PAGE INDEX

	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	ANN	
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	14	15	16	17	18	19	20	21	22	23	24	25	26	
Γ)	27	28	29	30	31	32	33	34	35	36	37	38	39	
.10)	40	41	42	43	44	45	46	47	48	49	50	51	52	
	53	54	55	56	57	58	59	60	61	62	63	64	65	
	66	68	70	72	74	76	78	80	82	84	86	88	90	
ι)	92	94	96	98	100	102	104	106	108	110	112	114	116	
	118	120	122	124	126	128	130	132	134	136	138	140	142	
I TY	144	146	148	150	152	154	156	158	160	162	164	166	168	
E DIRECTION	170	172	174	176	178	180	182	184	186	188	190	192	194	
WIND DIRECTION	196	197	198	199	200	201	202	203	204	205	Ž06	207	208	
TABLES		WINTE	R	s	PRING		s	UMMER			FALL	AL	L DATA	į.
		209			212			215			218		221	
		224			227			230			233		236	
		239			242			245			248		251	
		254			257			260			263		266	
		269			272			275			278		281	
		284			287			290			293		296	

., E

BACKGROUND

In December 1974 the Fleet Numerical Oceanography Center FLENUMOCEANCEN conjunction with the Naval Oceanographic Office (NAVOCEANO) adopted the Spectral Ocean Wave Model (SOWM) developed by Dr. Willard J. Pierson and others to produce operational spectral wave data for the Northern Hemisphere. The SOWM is a computer-based procedure that produces a directional variance spectrum at specified grid points spaced at up to 180 nautical intervals. This spectrum defines the through at each grid point two-dimensional (direction/frequency) matrix of 12 directions and 15 frequency bands. information on the theoretical basis of the SOWM is contained in Appendix A.

At the Seakeeping Workshop in July 1975, the rationale and structure of a hindcast wind and wave climatology were developed. It was concluded at that time that the hindcast climatology be intended to provide a statistical basis for evaluating the effects of the environment.

In order to summarize a set of spectra, it is often useful to generalize the most significant characteristics. The David Taylor Naval Ship Research and Development Center (DTNSRDC), with Operations Research, Inc. (ORI), developed computer programs to derive a number of numerical parameters from the spectral wave data. The National Climatic Data Center (NCDC) used many of the concepts from these programs and others written by FLENUMOCEANCEN to devise a parameterization routine which was used for this atlas.

OVERVIEW 1. PARAMETERS

This atlas contains climatological summaries for seven parameters. Four of these parameters have already been summarized in other climatic atlases (U.S. Navy, 1974 and 1987). These include wind speed and direction, significant wave height (hereafter referred to as the wave height), and wave direction, i.e., the direction waves are from which the highest (bereafter referred as primary to wave direction). The other three parameters contained in the wave climate summaries for this atlas are: wave slope parameter, modal wave period, and directionality of the waves (hereafter referred to as the directionality). These three parameters have not appeared in previous U. S. Navy climatological atlases, because they cannot be directly derived from visual observations. However, they can be very important operating considerations. Appendix B provides a complete description of all seven parameters. A brief description of the wave slope parameter, modal wave period, directionality follows.

The wave slope of a regular wave is defined as the ratio of wave height to wave length. is not normally reported, but it can be obtained trom the output of the SOWM or from the trequency spectrum of a wave record. rolling and hence stability is affected by the wave slopes of the higher waves encountered. The wave slope parameter is directly related to the wave slope. Therefore, the higher the wave slope parameter, the higher the wave slope. Table B3 in Appendix B relates the wave slope parameter to values of the wave slope at a fixed point. Steep waves are usually associated with wave slope parameters of 0.10 or more, while values of less than 0.05 are usually associated with more moderate conditions.

The modal wave period is defined in terms of the frequency spectrum. It is the period associated with the maximum wave energy in the wave spectrum. Modal wave periods associated with wave lengths about 0.75 and 1.25 ship lengths (depending on ship course and speed) can cause resonance pitching and heaving. The modal

wave period is not necessarily equal to the wave period associated with the higher of the two waves, the sea or the swell as summarized in the past U. S. Navy climatologies (U. S. Navy, 1974).

The directionality is a measure of the uniformity of the direction of movement of the waves. If the waves are all moving in a uniform direction then the directionality is equal to one. When there is no preferred direction of wave movement (a completely confused sea state) the directionality takes on the value of 0. Obviously, ship response and maneuverability can be affected by the directional spread of the wave energy.

II. DATA

Data in this atlas are derived using winds and waves from the period January 1973 to December 1982, i.e., 10 years. Computer processing difficulties during the generation of the SOWM hindcast data caused the number of hindcasts to vary among grid points. As a result, approximately 10% of all the data were lost during the 10-year hindcast period, 1973-1982 (Steurer, 1988).

ISOPLETH ANALYSES

Isopleth analyses were completed for various thresholds for the percent frequency of wind speed, wave height, and the wave slope parameter. These analyses were based on nearly 220 grid points, 63 of which are also used in tabular presentations. All points are depicted on the Mediterranean Sea map (Fig. 1). The 63 grid points also used in tabular summaries are listed in Table 1.

The Mediterranean Sea contains many areas of shallow water (< 100 fathoms) due to the large number of peninsulas and island groups. Since SOWM is a general purpose deep-water model, care should be taken when interpreting the analyses for shallow-water applications. The gray line in Figure 1 is in fact the 100 fathom isobath.

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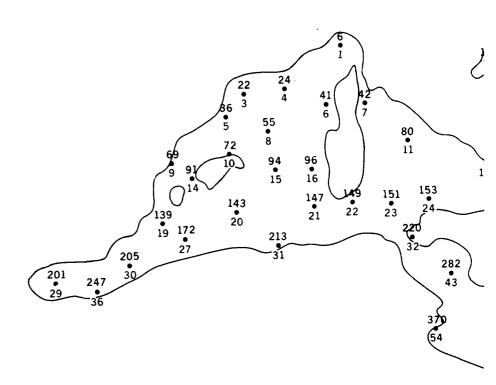
Unlike previous SOWM atlases (U.S. Navy, 1983 and 1985), isopleth analyses are shown in areas of less than 100 fathoms. This was done in order to provide more continuous analyses which would be less confusing to the user.

CONTINGENCY TABLES

Contingency tables for 63 grid points are presented for the following elements:

- (1) Wind direction and speed;
- (2) Wave height and wind speed;
- (3) Wave height and wave slope parameter;
- (4) Wave height and period;
- (5) Wave height and directionality;
- (6) Wave height and primary wave direction;
- (7) Primary wave direction and wind direction.

Fig. 1 GRID POINT AND SEC



 $N_{\rm g}^{\rm l}$ 1 Grid Point and sequence numbers

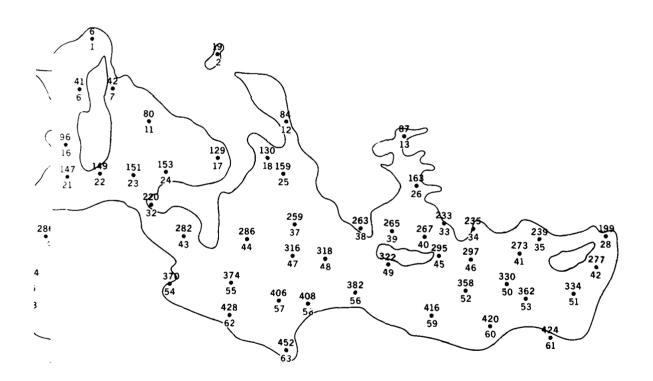


Table 1
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12 084 40.6N 18.8E 44 286 35.9N 16.8E 13 087 40.1N 24.9E 45 295 35.2N 26.6E 14 091 39.5N 02.2E 46 297 35.0N 28.3E 15 094 39.8N 05.7E 47 316 35.2N 19.2E 16 096 39.8N 07.4E 48 318 35.1N 20.8E 17 129 39.3N 15.2E 49 322 34.8N 24.1E 18 130 39.3N 17.8E 50 330 34.0N 30.5E 19 139 38.0N 00.7E 51 334 33.5N 33.6E 20 143 38.3N 04.1E 52 358 33.7N 28.0E 21 147 38.5N 07.5E 53 362 33.3N 31.1E 22 149 38.6N 09.2E 54 370 34.0N 12.7E 23 151 38.6N 10.9E	10	072	40.3N	03.8E	1	42	277	34.7N	34.8E						
13 087 40.1N 24.9E 45 295 35.2N 26.6E 14 091 39.5N 02.2E 46 297 35.0N 28.3E 15 094 39.8N 05.7E 47 316 35.2N 19.2E 16 096 39.8N 07.4E 48 318 35.1N 20.8E 17 129 39.3N 15.2E 49 322 34.8N 24.1E 18 130 39.3N 17.8E 50 330 34.0N 30.5E 19 139 38.0N 00.7E 51 334 33.5N 33.6E 20 143 38.3N 04.1E 52 358 33.7N 28.0E 21 147 38.6N 07.5E 53 362 33.3N 31.1E 22 149 38.6N 09.2E 54 370 34.0N 12.7E 23 151 38.6N 10.9E 55 374 34.0N 15.9E 24 153 38.7N 12.6E	11	080	40.7N	11.7E		43	282	36.0N	13.5E						
14 091 39.5N 02.2E 46 297 35.0N 28.3E 15 094 39.8N 05.7E 47 316 35.2N 19.2E 16 096 39.8N 07.4E 48 318 35.1N 20.8E 17 129 39.3N 15.2E 49 322 34.8N 24.1E 18 130 39.3N 17.8E 50 330 34.0N 30.5E 19 139 38.0N 00.7E 51 334 33.5N 33.6E 20 143 38.3N 04.1E 52 358 33.7N 28.0E 21 147 38.5N 07.5E 53 362 33.3N 31.1E 22 149 38.6N 09.2E 54 370 34.0N 12.7E 23 151 38.6N 10.9E 55 374 34.0N 15.9E 24 153 38.7N 12.6E 56 382 33.6N 22.3E 25 159 38.6N 18.6E	12	084	40.6N	18.8E		44	286	35.9N	16.8E						
15 094 39.8N 05.7E 47 316 35.2N 19.2E 16 096 39.8N 07.4E 48 318 35.1N 20.8E 17 129 39.3N 15.2E 49 322 34.8N 24.1E 18 130 39.3N 17.8E 50 330 34.0N 30.5E 19 139 38.0N 00.7E 51 334 33.5N 33.6E 20 143 38.3N 04.1E 52 358 33.7N 28.0E 21 147 38.5N 07.5E 53 362 33.3N 31.1E 22 149 38.6N 09.2E 54 370 34.0N 12.7E 23 151 38.6N 10.9E 55 374 34.0N 15.9E 24 153 38.7N 12.6E 56 382 33.6N 22.3E 25 159 38.6N 18.6E 57 406 33.2N 18.3E 26 163 38.1N 25.4E 58 408 33.1N 19.9E 27 172 37.4N 01.7E 59 416 32.6N 26.2E <	13	087	40.1N	24.9E		45	295	35.2N	26.6E						
16 096 39.8N 07.4E 48 318 35.1N 20.8E 17 129 39.3N 15.2E 49 322 34.8N 24.1E 18 130 39.3N 17.8E 50 330 34.0N 30.5E 19 139 38.0N 00.7E 51 334 33.5N 33.6E 20 143 38.3N 04.1E 52 358 33.7N 28.0E 21 147 38.5N 07.5E 53 362 33.3N 31.1E 22 149 38.6N 09.2E 54 370 34.0N 12.7E 23 151 38.6N 10.9E 55 374 34.0N 15.9E 24 153 38.7N 12.6E 56 382 33.6N 22.3E 25 159 38.6N 18.6E 57 406 33.2N 18.3E 26 163 38.1N 25.4E 58 408 33.1N 19.9E 27 172 37.4N 01.7E	14	091	39.5N	02.2E		46	297	35.0N	28.3E						
17 129 39.3N 15.2E 49 322 34.8N 24.1E 18 130 39.3N 17.8E 50 330 34.0N 30.5E 19 139 38.0N 00.7E 51 334 33.5N 33.6E 20 143 38.3N 04.1E 52 358 33.7N 28.0E 21 147 38.5N 07.5E 53 362 33.3N 31.1E 22 149 38.6N 09.2E 54 370 34.0N 12.7E 23 151 38.6N 10.9E 55 374 34.0N 15.9E 24 153 38.7N 12.6E 56 382 33.6N 22.3E 25 159 38.6N 18.6E 57 406 33.2N 18.3E 26 163 38.1N 25.4E 58 408 33.1N 19.9E 27 172 37.4N 01.7E 59 416 32.6N 26.2E 28 199 36.0N 35.2E	15	094	39.8N	05.7E		47	316	35.2N	19.2E						
18 130 39.3N 17.8E 50 330 34.0N 30.5E 19 139 38.0N 00.7E 51 334 33.5N 33.6E 20 143 38.3N 04.1E 52 358 33.7N 28.0E 21 147 38.5N 07.5E 53 362 33.3N 31.1E 22 149 38.6N 09.2E 54 370 34.0N 12.7E 23 151 38.6N 10.9E 55 374 34.0N 15.9E 24 153 38.7N 12.6E 56 382 33.6N 22.3E 25 159 38.6N 18.6E 57 406 33.2N 18.3E 26 163 38.1N 25.4E 58 408 33.1N 19.9E 27 172 37.4N 01.7E 59 416 32.6N 26.2E 28 199 36.0N 35.2E 60 420 32.2N 29.3E 29 201 36.0N 04.0W	16	096	39.8N	07.4E	İ	48	318	35.1N	20.8E						
19 139 38.0N 00.7E 51 334 33.5N 33.6E 20 143 38.3N 04.1E 52 358 33.7N 28.0E 21 147 38.5N 07.5E 53 362 33.3N 31.1E 22 149 38.6N 09.2E 54 370 34.0N 12.7E 23 151 38.6N 10.9E 55 374 34.0N 15.9E 24 153 38.7N 12.6E 56 382 33.6N 22.3E 25 159 38.6N 18.6E 57 406 33.2N 18.3E 26 163 38.1N 25.4E 58 408 33.1N 19.9E 27 172 37.4N 01.7E 59 416 32.6N 26.2E 28 199 36.0N 35.2E 60 420 32.2N 29.3E 29 201 36.0N 04.0W 61 424 31.7N 32.4E 30 205 36.5N 00.7W 62 428 32.6N 15.9E 31 213 37.1N 05.9E 63 452 31.2N 18.9E <td>17</td> <td>129</td> <td>39.3N</td> <td>15.2E</td> <td>İ</td> <td>49</td> <td>322</td> <td>34.8N</td> <td>24.1E</td> <td></td>	17	129	39.3N	15.2E	İ	49	322	34.8N	24.1E						
20 143 38.3N 04.1E 52 358 33.7N 28.0E 21 147 38.5N 07.5E 53 362 33.3N 31.1E 22 149 38.6N 09.2E 54 370 34.0N 12.7E 23 151 38.6N 10.9E 55 374 34.0N 15.9E 24 153 38.7N 12.6E 56 382 33.6N 22.3E 25 159 38.6N 18.6E 57 406 33.2N 18.3E 26 163 38.1N 25.4E 58 408 33.1N 19.9E 27 172 37.4N 01.7E 59 416 32.6N 26.2E 28 199 36.0N 35.2E 60 420 32.2N 29.3E 29 201 36.0N 04.0W 61 424 31.7N 32.4E 30 205 36.5N 00.7W 62 428 32.6N 15.9E 31 213 37.1N 05.9E 63 452 31.2N 18.9E	18	130	39.3N	17.8E	ļ	50	330	34.0N	30.5E						
21 147 38.5N 07.5E 53 362 33.3N 31.1E 22 149 38.6N 09.2E 54 370 34.0N 12.7E 23 151 38.6N 10.9E 55 374 34.0N 15.9E 24 153 38.7N 12.6E 56 382 33.6N 22.3E 25 159 38.6N 18.6E 57 406 33.2N 18.3E 26 163 38.1N 25.4E 58 408 33.1N 19.9E 27 172 37.4N 01.7E 59 416 32.6N 26.2E 28 199 36.0N 35.2E 60 420 32.2N 29.3E 29 201 36.0N 04.0W 61 424 31.7N 32.4E 30 205 36.5N 00.7W 62 428 32.6N 15.9E 31 213 37.1N 05.9E 63 452 31.2N 18.9E	19	139	38.0N	00.7E		51	334	33.5N	33.6E						
22 149 38.6N 09.2E 54 370 34.0N 12.7E 23 151 38.6N 10.9E 55 374 34.0N 15.9E 24 153 38.7N 12.6E 56 382 33.6N 22.3E 25 159 38.6N 18.6E 57 406 33.2N 18.3E 26 163 38.1N 25.4E 58 408 33.1N 19.9E 27 172 37.4N 01.7E 59 416 32.6N 26.2E 28 199 36.0N 35.2E 60 420 32.2N 29.3E 29 201 36.0N 04.0W 61 424 31.7N 32.4E 30 205 36.5N 00.7W 62 428 32.6N 15.9E 31 213 37.1N 05.9E 63 452 31.2N 18.9E	20	143	38.3N	04.1E		52	358	33.7N	28.0E						
23 151 38.6N 10.9E 55 374 34.0N 15.9E 24 153 38.7N 12.6E 56 382 33.6N 22.3E 25 159 38.6N 18.6E 57 406 33.2N 18.3E 26 163 38.1N 25.4E 58 408 33.1N 19.9E 27 172 37.4N 01.7E 59 416 32.6N 26.2E 28 199 36.0N 35.2E 60 420 32.2N 29.3E 29 201 36.0N 04.0W 61 424 31.7N 32.4E 30 205 36.5N 00.7W 62 428 32.6N 15.9E 31 213 37.1N 05.9E 63 452 31.2N 18.9E	21	147	38.5N		1	53	362	33.3N	31.1E						
24 153 38.7N 12.6E 56 382 33.6N 22.3E 25 159 38.6N 18.6E 57 406 33.2N 18.3E 26 163 38.1N 25.4E 58 408 33.1N 19.9E 27 172 37.4N 01.7E 59 416 32.6N 26.2E 28 199 36.0N 35.2E 60 420 32.2N 29.3E 29 201 36.0N 04.0W 61 424 31.7N 32.4E 30 205 36.5N 00.7W 62 428 32.6N 15.9E 31 213 37.1N 05.9E 63 452 31.2N 18.9E	22	149	38.6N	09.2E	İ	54	370	34.0N	12.7E	1					
25 159 38.6N 18.6E 57 406 33.2N 18.3E 26 163 38.1N 25.4E 58 408 33.1N 19.9E 27 172 37.4N 01.7E 59 416 32.6N 26.2E 28 199 36.0N 35.2E 60 420 32.2N 29.3E 29 201 36.0N 04.0W 61 424 31.7N 32.4E 30 205 36.5N 00.7W 62 428 32.6N 15.9E 31 213 37.1N 05.9E 63 452 31.2N 18.9E	23	151	38.6N	10.9E		55	374	34.0N	15.9E						
26 163 38.1N 25.4E 58 408 33.1N 19.9E 27 172 37.4N 01.7E 59 416 32.6N 26.2E 28 199 36.0N 35.2E 60 420 32.2N 29.3E 29 201 36.0N 04.0W 61 424 31.7N 32.4E 30 205 36.5N 00.7W 62 428 32.6N 15.9E 31 213 37.1N 05.9E 63 452 31.2N 18.9E	24	153	38.7N	12.6E		56	382	33.6N	22.3E						
27 172 37.4N 01.7E 59 416 32.6N 26.2E 28 199 36.0N 35.2E 60 420 32.2N 29.3E 29 201 36.0N 04.0W 61 424 31.7N 32.4E 30 205 36.5N 00.7W 62 428 32.6N 15.9E 31 213 37.1N 05.9E 63 452 31.2N 18.9E	25	159	38.6N	18.6E		57	406	33.2N	18.3Ē						
28 199 36.0N 35.2E 60 420 32.2N 29.3E 29 201 36.0N 04.0W 61 424 31.7N 32.4E 30 205 36.5N 00.7W 62 428 32.6N 15.9E 31 213 37.1N 05.9E 63 452 31.2N 18.9E	26	163	38.1N	25.4E		58	408	33.1N	19.9E	·					
29 201 36.0N 04.0W 61 424 31.7N 32.4E 30 205 36.5N 00.7W 62 428 32.6N 15.9E 31 213 37.1N 05.9E 63 452 31.2N 18.9E	27	172	37.4N	01.7E		59	416	32.6N	26.2E						
30 205 36.5N 00.7W 62 428 32.6N 15.9E	28	199	36.0N	35.2E		60	420	32.2N	29.3E						
31 213 37.1N 05.9E 63 452 31.2N 18.9E	29	201	36.0N	04.0W		61	424	31.7N	32.4E						
	30	205	36.5N	00.7W		62	428	32.6N	15.9E						
32 220 37.3N 11.8E	31	213	37.1N	05.9E		63	452	31.2N	18.9Έ						
	32	220	37.3N	11.8E]					

viii 🔑

The values in these tables are percent frequencies rounded to the nearest whole percent. Values less than 0.5% but greater than 0% are depicted by a '+'.

The left side of each contingency table has a percentage scale for the bar graphs associated with the categories indicated along the bottom of the table. The height of the bar graphs was determined by adding the values within each column. Similarly, the percent frequencies in the column denoted by a 'T' (total) were obtained by summing the percent frequencies across each row. Rounding may cause minor differences between printed totals and total cell counts. By adding down or up the 'T' column or across the bar graphs at the bottom of the table, it is possible to obtain cumulative percent frequency of a parameter below or above some specified threshold value.

In the following four contingency tables: wind direction and speed, wave height and wind speed, wave height and wave slope, and wave height and directionality the mean value of one of the two parameters associated with each contingency table is displayed just above the upper left corner. The number of hindcasts that was available for all seven tables is also shown at the top of each table. When SOWM hindcast data were not retained due to insufficient wave energy, all parameters were assumed to be zero including the wind speed and direction. speeds were rounded to the nearest whole knot before tabulating the frequency Directions are those from which the wind or wave is coming. Detailed instructions describing how to read each of the various types of contingency tables are contained in the 'Legends potential Tables'. Some uses for the contingency demonstrated in tables are Appendix c.

DURATION AND INTERVAL TABLES

Duration and Interval Tables were prepared for:

- (1) Wind speed;
- (2) Significant wave height;
- (3) Wave slope parameter.

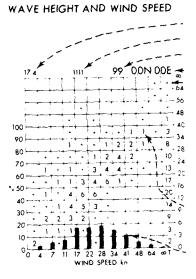
The tables contain objective compilations for 63 grid points on a seasonal basis, and also without regard to season (All Data). Since grid points may be representative of relatively small geographical areas surrounding the points, interpolation may be necessary if data are required for areas between grid points.

Episodes of durations (continuous hours or days) of events and episodes of intervals (continuous hours or days) between events were tallied for various thresholds. These tables give an indication of how long an episode is likely to last once it has begun. convenience, the time an episode persisted above a given threshold is arbitrarily referred to as a "duration" of the event. The times in between episodes have been termed "intervals." have been summarized on a seasonal basis as opposed to monthly summaries. This was deemed most appropriate because even with 10 years of hindcast data the embedded missing data makes the sample too small to provide representative durations and intervals for long episodes of wind and wave conditions. The winter season consisted of months January through spring - April through June, summer - July through September, and autumn October through December, (World Meteorological Organization, 1981). Additional information on the construction and use of the duration and interval tables, including examples of their applications, is included in Appendix D and in the 'Legends for Tables.'

LEGENDS FOR TABLES

WIND DIRECTION AND SPEED ____Scalar mean speed (kn). - Number of hindcasts. Sequence number. LATITUDE AND LONGITUDE Direction frequency (left scale): Bars are percentages for each wind direction. Speed frequency (right + 2 1 scale). Numbers are percentages of wind speed by direction. C = Calm wind. T = Total. + Means >0 but <0.5%. <0.5% Of the winds were ≥64 kn. .3% Of the winds were from the NW with speeds ≥11 kn. and <17 kn. -22% Of the winds were from the

~2% Of the winds were calm.



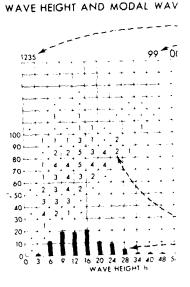
._Number of hindcasts. Sequence number. -Latitude and longitude 00N 00E 🛫

WAVE HEIGHT AND WAVE SLOPE α

Wave slope a frequency (left scale): Bars are percentages for each wave slope category. Wave height frequency (right scale): Numbers are percentages of wave height vs. wave slope a. T = Total + Means >0 but <0.5%. <0.5% Of the wave heights were ≥64 ft.

(19.5m). 4% Of the wave slopes (a) were ≥.11 but <.12 with wave heights ≥28 ft (8.5m) but <34 ft. (10.4m).

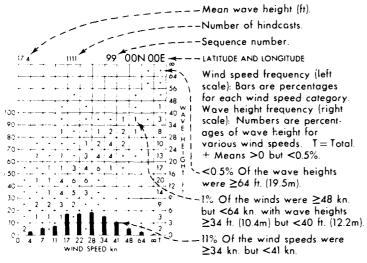
17% Of the wave slopes (a) were ≥.10 but <.11.



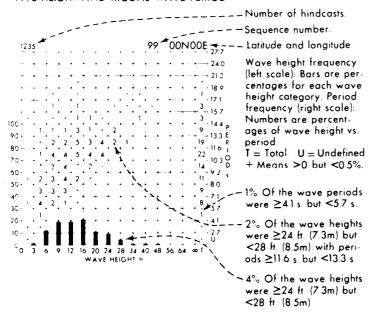
feet 0 3 6 12 20 28 34 40 48 56 64 meters 0 1837 61 85 12 2 14.6 17 1 19 5

FOR TABLES

WAVE HEIGHT AND WIND SPEED

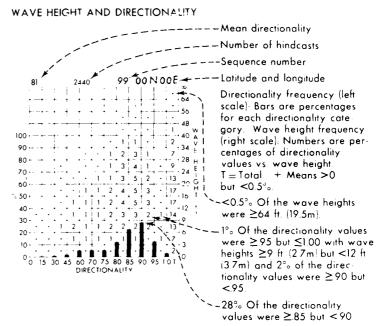


WAVE HEIGHT AND MODAL WAVE PERIOD

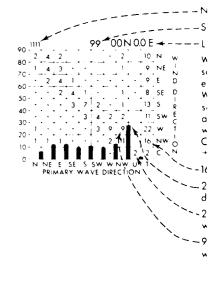


24 0 28 34 40 48 56 64 1 85 12 2 14 6 17 1 19 5 7 3 10 4

LEGENDS FOI



PRIMARY WAVE DIRECTION AND WIND



feet 036 12 20 28 3 meters 0 1837 61 85 09274973 10

XI P

LEGENDS FOR TABLES

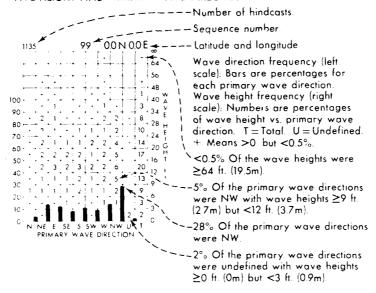
WAVE HEIGHT AND PRIMARY WAVE DIRECTION

tean directionality comber of hindcasts. equence number attude and longitude

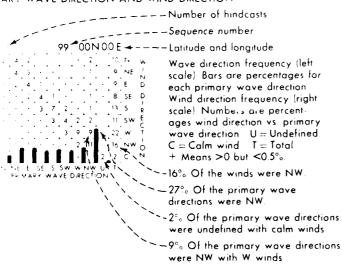
Frectionality frequency (left cale Bars are percentages or each directionality cate-tory Wave height frequency cahr scale). Numbers are percentages of directionality causes wave height Total — Means >0

<0.5° Of the wave heights were ≥64 ft !19.5m!

Of the directionality values were ≥ 95 but ≤1 00 with wave eights ≥9 ft 12 7m² but <12 ft 17m² and 2°c of the directionality values were ≥ 90 but <95



MARY WAVE DIRECTION AND WIND DIRECTION



feet 0 3 6 12 20 28 34 40 48 56 64 meters 0 18 37 61 85 12 2 14 6 17 1 19 5

LEGENDS FOR TABLES

WIND SPEED DURATIONS SEASONAL

LATITUDE AND LONGITUDE 3 13 12 25 20 ≥ 48 ≥ 41 24-21 21 48 1 39 78 1 79 1235 1235 1235 1235 1250 3 9 15 25 3 10 38 105 105 ≥ 34 231 6. 9. 14. 2. 2. 440 144 1 1 114 656 354 1 107 945 SEA 2 77 1078 SEA 2 41 1336 670 959 1258 1269 1153 Event with wind speeds ≥7 kn. persisted 12 hours; 26 events persisted ≥96 hours The longest event with wind speeds ≥7 km. persisted for 1 season or more and it occurred 2 times -

The longest event with wind speeds ≥48 kn. persisted 18 hours and it occurred 1 time. ---

4) Events had wind speeds ≥4 kn. which comprised a total of 1,336 hindcasts. -----

1,483 Hindcasts were examined, and 1,443 had wind speeds ≥4 kn

Durations for a particular season extend from the time the event begins (or the first day of the season if already in progress), and terminate when the event ends. Events become undefined if missing data is encountered. Durations lasting a season or more are categorized together. Durations may persist into the next season.

WAVE HEIGHT INTERVALS SCASONIAL

SEQUENCE NUMBER	A TITLING AND A DOLLAR OF
	LATITUDE AND LONGITUDE
264	9 SEA 9 9 1116 1235 1235
w≥56,	9 SEA 9 7 1116 1235 1235
A ≥ 48	9 SEA 91 9 1116 1235 1235
€ ≥40	9 SEA 9 10 1129 1248 1249
≥34	12 SEA 10 14: 1323 1355 1367
H > 28	14 SEA 10 18 1512 1537 1563
7 ≥ 24 . 1. 1. 1	17 SEA 6 29 1454 1475 1549
$G \stackrel{>}{=} 20$, 2, 2, 5, 3, 1, 1, 2, 1, 1, 2, 1, 1, 1	21 SEA 1 45 1376 1395 1575
$H \ge 16 - 5 - 7 - 4 - 4 - 1 - 1 - 1 - 1 - 2 - 2 - 1 - 1$	24, 690 1 55 1071 1083 1400
1 ≥12 18 11 3 3 1 3 4 1 5 4 2 2 5	12 309 1 74 675 675 1254
+ ≥9 12 13 5 8 5 6 8 4 2 7 3	4 1861 1 72 431 431 1241
' ≥6 11.418 8 6 4 2, 4 1 1 1	1 132 1 47 189 189 1235
≥3 _8, 2, 2, 1	30 1 13 23 23 1235
6 12 18 24 30 36 42 48 54 60 66 72 78 84 90	
HOURS INTERVALS BETWEEN EVE	NIS,
(The) The Total To	

There were 13 12-hour intervals between events of wave heights\ ≥9 ft. (2.7m); 4 intervals persisted 96 hours or more

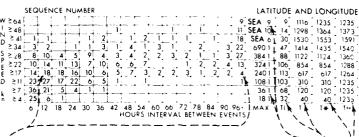
The longest interval between events of wave heights ≥6 ft. (1.8m) was 132 hours and it occurred 1 time. — — — The longest interval between events of wave heights ≥64 ft. (19.5m) was 1 season or more and it occurred 9 times.—

There were 13 intervals between events of wave heights ≥3 ft (0.9m) which comprised a total of 23 hindcasts. ~-

1,235 Hindcasts were examined, and 23 had wave heights <3 ft.

Intervals for a particular season extend from the time the event ends (or the first day of the season if the event is not in progress), and terminate when the event begins. Intervals become undefined if missing data is encountered. Intervals lasting a season or more are categorized together. Intervals may persist into the next season

WIND SPEED INTERVALS - SEASONAL



There were 18 12-hour intervals between events of wind speeds ≥17 kn.; 4 intervals persisted 96 hours or more.

The longest interval between events of wind speeds ≥7 kn. was 36 hours and it occurred 1 time. -

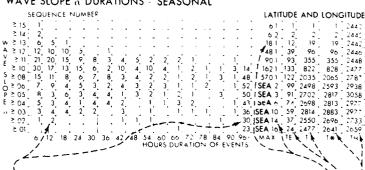
The longest interval between events of wind speeds ≥64 kn. was 1 season or more and it occurred 9 times. --

There were 32 intervals between events of wind speeds ≥4 kn which comprised a total of 40 hindcasts. — -

1,235 Hindcasts were examined, and 40 had wind speeds <4 kn

Intervals for a particular season extend from the time the event ends (or the first day of the season the event is not in progress), and terminate when the event begins. Intervals become undefined if missing data is encountered. Intervals lasting a season or more are categorized together. Intervals may persist into the next season

WAVE SLOPE a DURATIONS - SEASONAL



-2 Events with $\alpha \ge 0.02$ persisted 12 hours; 30 events persisted

The longest event with $\alpha \ge 0.13$ persisted 18 hours and it occurred, The longest event with $\alpha \ge 0.02$ persisted for 1 season or more and

it occurred 14 times -----

24 Events had a ≥0.01 which comprised a total of 2,477 hindcasts 2,659 Hindcasts were examined, and 2,641 had a ≥001 --

Durations for a particular season extend from the time the event begins (or the first day of the season if already in progress), and terminate when the event ends. Events become undefined if missing data is encountered. Durations lasting a season or more are categorized together. Durations may persist into the next season

ABBREVIATIONS (See text for details)

MAX. Maximum duration or interval, followed by the number of occurrences

TE or Th. Total number of events or intervals.

T: Total number of hindcasts included in TE or TI.

Total number of hindcasts that met the stated criteria

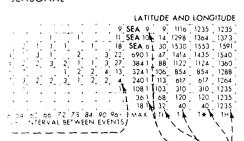
TH: Total number of hindcasts examined.

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DS FOR TABLES

SEASONAL



intervals perween events of wind speeds irsisted 96 hours or more.

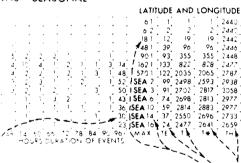
etween events of wind speeds ≥7 kn ccurred 1 time. -

etween events of wind speeds ≥64 kn. was it occurred 9 times. -- -

als between events of wind speeds ≥4 kn tal of 40 hindcasts. ----

examined, and 40 had wind speeds <4 kn. lar season extend from the time the event ends eseason the event is not in progress), and termi begins. Intervals become undefined if missing Intervals lasting a season or more are Intervals may persist into the next season

INS SEASONAL



12 persisted 12 hours, 30 events persisted

th $\alpha \ge 0.13$ persisted 18 hours and it occurred,

th a ≥0.02 persisted for 1 season or more and

01 which comprised a total of 2,477 hindcasts 4 e examined, and 2,641 had a ≥0.01 ----

icular season extend from the time the event ay of the season if already in progress), and termiends. Events become undefined if missing data ations lasting a season or more are categorized may persist into the next season

currences

WAVE HEIGHT DURATIONS - SEASONAL LATITUDE AND LONGITUDE ≥ 56 ≥ 48 ≥28 ≥24 ≥20 4 Events with wave heights ≥6 ft. (1.8m) persisted 12 hours; 22 events persisted ≥96 hours. The longest event with wave heights ≥3 ft. (0.9m) persisted 1 season or more and it occurred 8 times. -The longest event with wave heights ≥40 ft. (12.2m) persisted for 6 hours and it occurred 1 time -----22 Events had wave heights ≥3 ft. (0.9m) which comprised a total of 1,524 hindcasts. -----1,649 Hindcasts were examined, and 1,626 had wave heights ≥3 ft.

Durations for a particular season extend from the time the event begins (or the first day of the season if already in progress), and terminate when the event ends. Events become undefined if missing data is encountered. Durations lasting a season or more are categorized together. Durations may persist into the next season

WAVE SLOPE a INTERVALS - SEASONAL

SEQUENCE NUMBER LATITUDE AND LONGITUDE 19 2319 2557 2558

There were 18 12-hour intervals between events of wave slopes ≥0.06; 2 intervals persisted 96 hours or more.

The longest interval between events of wave slopes ≥0.10 was 474 hours and it occurred 1 time. The longest interval between events of wave slopes ≥0.15 was 1 season or more and it occurred 18 times.

There were 6 intervals between events of wave slopes ≥0.01 which comprised a total of 12 hindcasts.

2,440 Hindcasts were examined, and 12 had wave slopes < 0.01.

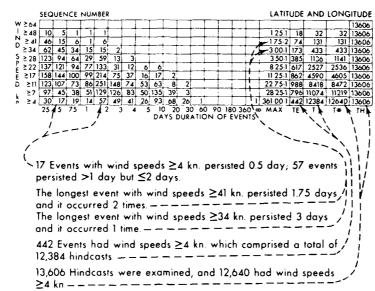
Intervals for a particular season extend from the time the event ends (or the first day of the season if the event is not in progress), and terminate when the event begins. Intervals become undefined if missing data is encountered. Intervals lasting a season or more are categorized together. Intervals may persist into the next season

Feet 0.3 6 12 20 28 34 40 48 56 64 meters 0.9 27 49 7 3 10 4

LEGENDS FOR TA

WIND SPEED INTERVALS - ENTIRE DATA SET

WIND SPEED DURATIONS - ENTIRE DATA SET



Durations extend from the time the event begins and terminate when the event ends. Events become undefined if missing data is encountered

WAVE HEIGHT INTERVALS - ENTIRE DATA SET

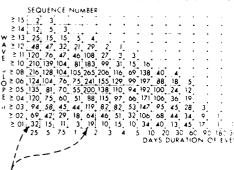
SEQUENCE NUMBER		LATITUDE	AND LO	NGITUDE
≥64/	· · · · · · · · · · · · · · · · · · ·		136	06 13606
w ≥ 56			136	06 13606
A ≥ 48				06 13606
V ≥40		308 25 1 2	1239 135	96 13606
≥34 1 2	3 1 7 7		2793 135	
H ≥282 \4 3 1 1	5 2 1 3 2 3 2		8571 135	
≥24 <u>3</u> 4 <u>7</u> 5 1 5 7 3	2 13 12 4 11 1 5 1	338 00 1 76		
G ≥ 20 7 8 7 2 16 14 10	6 18 20 11 9 1 3 5 1	232 25 1 134		
H ≥16 18 17 16 6 32 26 13	14 33 31 11 4 2 2 1	205 75 1 226		
	23,40,29, 7, 7, 3, 2, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	180 7 5 1 363		
1 ≥9 <u>57 45 32 36 93 49 28</u>	16 34 24 8 7 3 2	128 50 1 434		90 13606
26 72 56 39 46 92 47 21	17 40 35 6 4	50 50 1,475		13606
≥3 73 67 35 31 85 35 24		18 25 2 401		08 13606
25 5/75) 2 3 4	5 10 20 30 60 90 180 360 4	O MAX X II	K []K 1	* * IH
	DAYS INTERVAL BETWEEN EVEN	15.		· \ \
				~\ \!
1				- 77 T
>1 inierval between ev	ents of wave heights ≥34	ft. (10.4m) persis	ted \ \ i'
0.5 day, 2 intervals	persisted >1 day but ≤2 c	ave	-	iil
0.5 day; 2 liller vals (301313100 × 1 007 001 <u>-</u> 2 0			117
The longest interval b	between events of wave h	eiahts >3	ft. (0.9)	n) //:
was 18.25 days and				_'/!!
				/1!
The longest interval b	petween events of wave hi	eights ≥4	0 H. ,	/ j !
was 308.25 days and	t it occurred 1 time			/ 1
•				/ 1
There were 401 inter	vals between events of wo	ive heigh	ts .	/ 1
	omprised a total of 3,133			1
≥3 ii. (0.7iii) Which C	omprised a loid of 5,155	imacusis.		1
13,606 Hindcasts wer	e examined, and 3,208 ha	id wave l	neights	<3/

Intervals extend from the time the event ends and terminate when the event begins. Intervals become undefined if missing data is encountered.

The longest interval between events of wind sp 6.25 days and it occurred 1 time ----The longest interval between events of wind sp 8.75 days and it occurred 2 times -----

There were 451 intervals between events of w ≥4 kn which comprised a total of 963 hindco: 13,606 Hindcasts were examined, and 966 had Intervals extend from the time the event ends at the event begins. Intervals become undefined encountered

WAVE SLOPE a DURATIONS - ENTIRE DATA SET



-32 Events with α ≥0.01 persisted 25 day, 19 e day but ≤2 days.

The longest event with $\alpha \ge 0.12$ persisted 3.25 occurred 1 time. -----The longest event with $\alpha \ge 0.13$ persisted 1.50 of 2 times. ----

267 Events had a ≥0.01 which comprised a to hindcasts. -----

29,016 Hindcasts were examined, and 28,054

Durations extend from the time the event beginner the event ends. Events become undefinition encountered.

ABBREVIATIONS (See text for details)

MAX: Maximum duration or interval, followed by the number of occurrences

TE or TI: Total number of events or intervals.

T. Total number of hindcasts included in TE or TI.

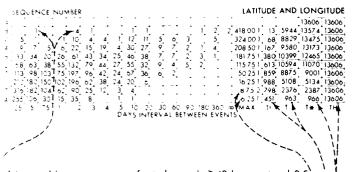
Two Total number of hindcasts that met the stated criteria

TH: Total number of hindcasts examined

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LEGENDS FOR TABLES

4D SPEED INTERVALS - ENTIRE DATA SET

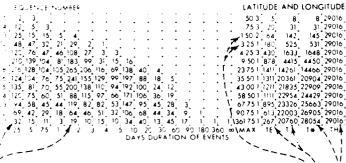


-1 Interval between events of wind speeds ≥48 km persisted 0.5 day, 4 intervals persisted >1 day but ≤2 days

There were 45t intervals between events of wind speeds 24 kn which comprised a total of 963 hindcasts

13.606 Hindcasts were examined, and 966 had wind speeds <4 kn
Intervals extend from the time the event ends and terminate when
the event begins. Intervals become undefined if missing data is
encountered.

AVE SLOPE α DURATIONS - ENTIRE DATA SET



~32 Events with α ≥0.01 persisted 25 day, 19 events persisted > day but ≤2 days.

267 Events had a ≥0.01 which comprised a total of 20,760

29,016 Hindcasts were examined, and 28,054 had $\alpha \ge 0.01$ —

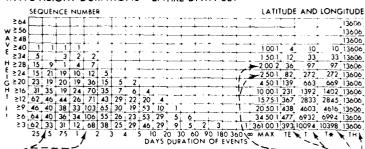
Durations extend from the time the event begins and terminate when the event ends. Events become undefined if missing data is encountered.

for details)

by the number of occurrences

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WAVE HEIGHT DURATIONS - ENTIRE DATA SET



-33 Events with wave heights ≥3 ft. (0.9m) persisted 0.5 day; 68 events persisted >1 day but ≤2 days.

393 Events had wave heights \geq 3 ft. (0.9m) which comprised a total of 10,094 hindcasts.

Durations extend from the time the event begins and terminate when the event ends. Events become undefined if missing data is encountered.

WAVE SLOPE α INTERVALS \times ENTIRE DATA SET

WAVE SLOPE & INTERVALS - ENTIRE DATA SET										
SEQUENCE NUMBER					LATITUD	E AND	LONG	ITUDE		
≥ 15	1.	1			16 25 1	7.9	29008	29016		
. ≥14 > > 11	1.	. 3 1.	3	· · · · · · · · · · · · · · · · · · ·	44751	754	26985	29016		
$w \ge 13$ 2 2 3 $\frac{1}{2}$	5 1 1	3 10 4	6 2 2	6 73	87 75 1 4	11986	28871	29015		
A ≥ 12 6 8 5 2 16	6. 7. 7.	26 33 10	20 6 4	9 / 2	58 75 1 16	19432	28485	29016		
. ¥ ≥ 11 [34] 20 [15	40 31 19	54 58 29	22 7 10	3 1 2	02 25 1 41.	5 23046	27368	29016		
F ? 10 99 62 61 61 114	79 71 48	117 94 28	20 8 4	1.1	27 50 1 86	5,22585	24566	29016		
$-5 \ge 08[263]156[124]123[271]1$				11.	47.75 1,141	114399	14550	29016		
279 188 156 122 269	136 61 34	6. 4		- [I]	15 00 1 131	1 8040	8112	29016		
P ≥ 05 304 227 143 93 244				- [1]	14 50 1 121	1 6040	6107	29016		
E > 04 326 227 148 86 197	63 32 22	10 1		1	14 50 EHI.	4577	4587	29016		
≥ 03 318 173 113 72 151	43 26 6	8		1.	8 50 1 91	3347	3353	29016		
≥ 02 [231] 136 72¥60 88]	23 14 3	4		- i X	8 00 1 63	2109	2111	29016		
≥ 01 [112] 56 29 25 41 [13 7 1	2		1	5 75 2 28			29016		
25 5 75 1 2	3 4 5	10 20 30			MAX	K 1 K	1 * 7	€ THI		
,	D.A.	YS INTERV	AL RETWEEN	EVEN'S	' '		`.	` '		

~2 Intervals between events of wave slopes ≥0 13 persisted 0.5 day, 1 interval persisted >1 day but ≤2 days

The longest interval between events of wave slopes ≥015 was 16.25 days and it occurred 1 time.

The longest interval between events of wave slopes ≥001 was 5.25 days and it occurred 2 times.

There were 286 intervals between events of wave slopes ≥0.01, which comprised a total of 961 hindcasts.

29,016 Hindcasts were examined, and 962 had wave slopes < 0.01.

Intervals extend from the time the event ends and terminate when the event begins. Intervals become undefined if missing data is encountered.

feet 0 3 6 12 20 28 34 40 48 56 64 meters 0 18 37 61 85 12 2 14 6 17 1 19 5 0 9 27 4 9 7 3 10 4

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WIND SPEED (≤10 AND ≥34 KNOTS)

Solid Lines (dotted intermediates) - Percent frequency of wind speeds ≤10 knots

Dashed Lines (short intermediates) - Percent frequency of wind speeds ≥34 knots



15



Solid Lines (dotted intermediates) - Percent frequency of wind speeds ≤10 knots

Dashed Lines (short intermediates) - Percent frequency of wind speeds ≥34 knots



WIND SPEED (≤10 AND ≥34 KNOTS)

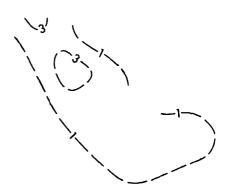


WIND SPEED (≤10 AND ≥34 KNOTS)

Solid Lines (dotted intermediates) - Percent frequency of wind speeds ≤10 knots

Dashed Lines (short intermediates) - Percent frequency of wind speeds ≥34 knots





Solid Lines (dotted intermediates) - Percent frequency of wind speeds ≤10 knots

Dashed Lines (short intermediates) - Percent frequency of wind speeds ≥34 knots

WIND SPEED (≤10 AND ≥34 KNOTS)

WIND SPEED (≤10 AND ≥34 KNOTS)



Solid Lines (dotted intermediates) - Percent frequency of wind speeds ≤10 knots

Dashed Lines (short intermediates) - Percent frequency of wind speeds ≥34 knots

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JUNE

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Solid Lines (dotted intermediates) - Percent frequency of wind speeds ≤10 knots

Dashed Lines (short intermediates) - Percent frequency of wind speeds ≥34 knots

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WIND SPEED (≤10 AND ≥34 KNOTS)

36

}



Solid Lines (dotted intermediates) - Percent frequency of wind speeds ≤10 knots

Dashed Lines (short intermediates) - Percent frequency of wind speeds ≥34 knots

JULY



AUGUST WINI

Solid Lines (dotted intermediates) - Percent frequency of wind speeds ≤10 knots

Dashed Lines (short intermediates) - Percent frequency of wind speeds ≥34 knots

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Solid Lines (dotted intermediates) - Percent frequency of wind speeds ≤10 knots

Dashed Lines (short intermediates) - Percent frequency of wind speeds ≥34 knots

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OCTOBER

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Solid Lines (dotted intermediates) - Percent frequency of wind speeds ≤10 knots

Dashed Lines (short intermediates) - Percent frequency of wind speeds ≥34 knots

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Solid Lines (dotted intermediates) - Percent frequency of wind speeds ≤10 knots

Dashed Lines (short intermediates) - Percent frequency of wind speeds ≥34 knots

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NOVEMBER



Solid Lines (dotted intermediates) - Percent frequency of wind speeds ≤10 knots

Dashed Lines (short intermediates) - Percent frequency of wind speeds ≥34 knots

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Solid Lines (dotted intermediates) - Percent frequency of wind speeds ≤10 knots

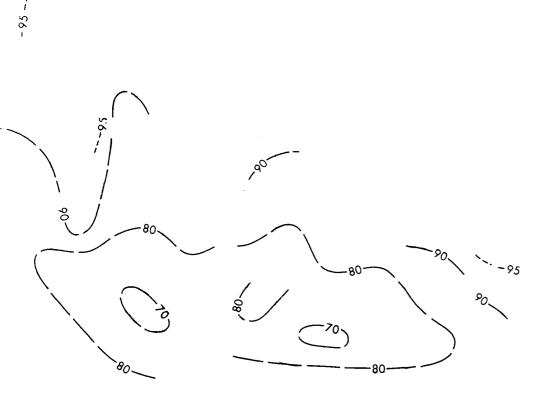
Dashed Lines (short intermediates) - Percent frequency of wind speeds ≥34 knots

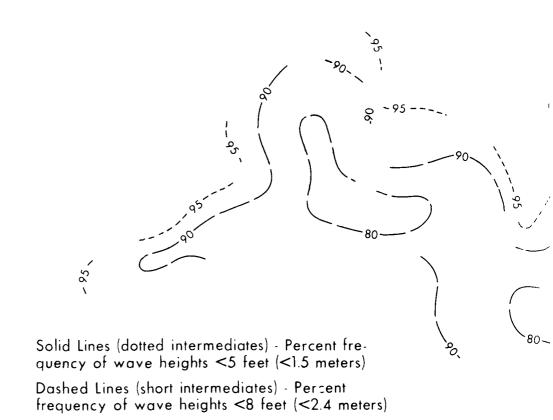
ANNUAL

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Solid Lines (dotted intermediates) - Percent frequency of wave heights <5 feet (<1.5 meters)

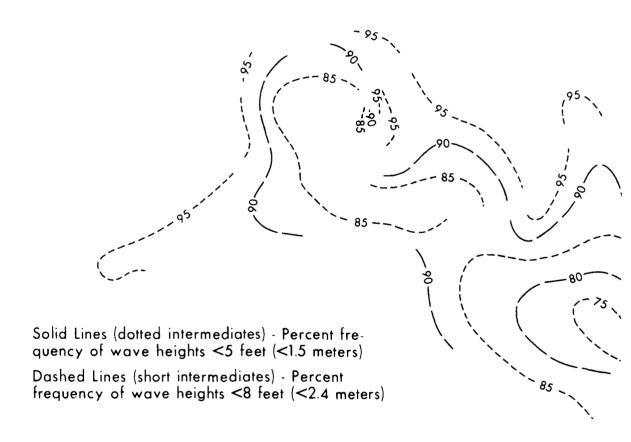
Dashed Lines (short intermediates) - Percent frequency of wave heights <8 feet (<2.4 meters)

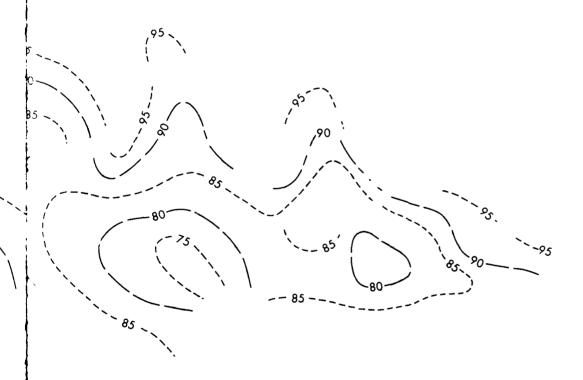




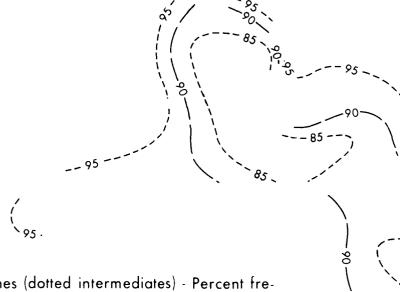
FEBRUARY







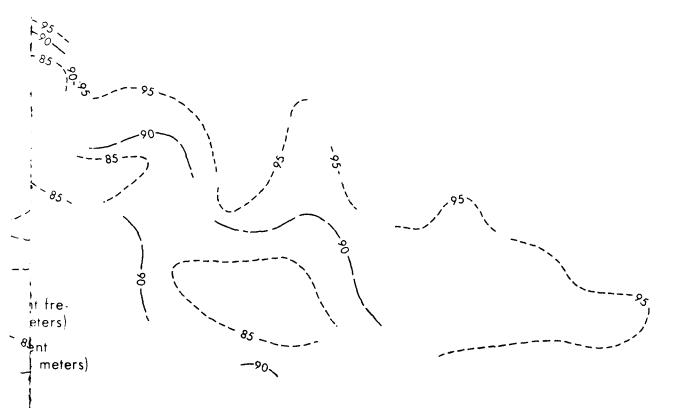
140 8

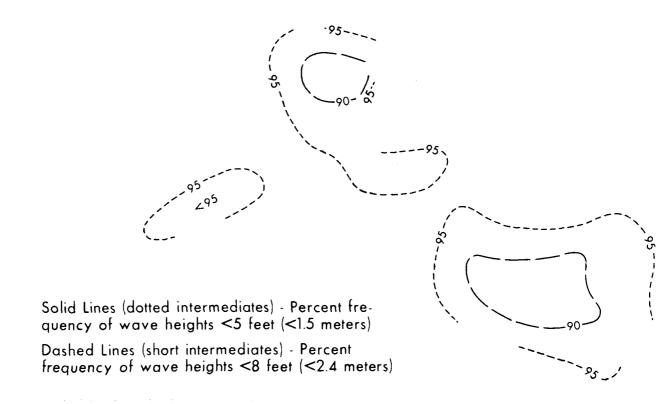


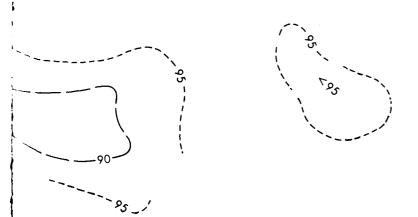
Solid Lines (dotted intermediates) - Percent frequency of wave heights <5 feet (<1.5 meters)

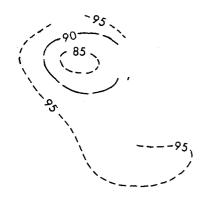
Dashed Lines (short intermediates) - Percent frequency of wave heights <8 feet (<2.4 meters)

100





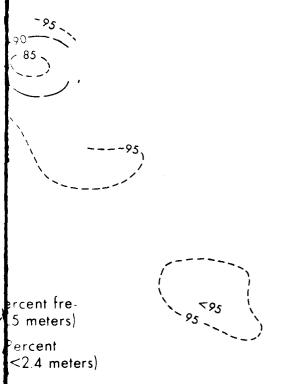


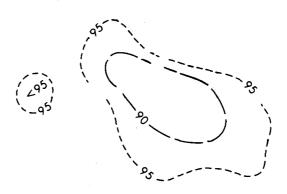


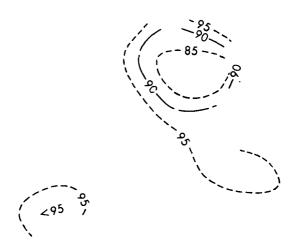
Solid Lines (dotted intermediates) - Percent frequency of wave heights <5 feet (<1.5 meters)

Dashed Lines (short intermediates) - Percent frequency of wave heights <8 feet (<2.4 meters)

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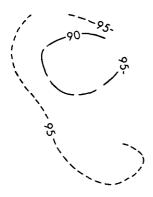


Solid Lines (dotted intermediates) - Percent frequency of wave heights <5 feet (<1.5 meters)

Dashed Lines (short intermediates) - Percent frequency of wave heights <8 feet (<2.4 meters)



206



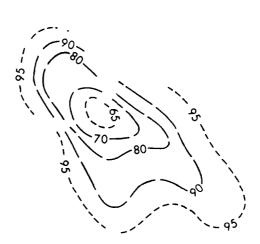
Solid Lines (dotted intermediates) - Percent frequency of wave heights <5 feet (<1.5 meters)

Dashed Lines (short intermediates) - Percent frequency of wave heights <8 feet (<2.4 meters)

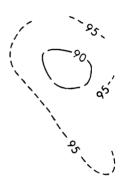
AUGUST

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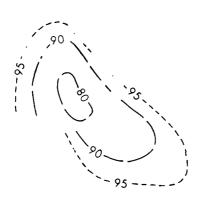


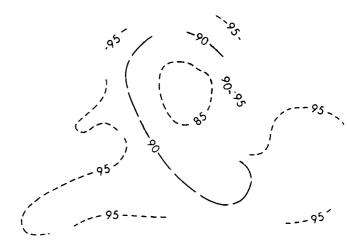
SEPTEMBER



Solid Lines (dotted intermediates) - Percent frequency of wave heights <5 feet (<1.5 meters)

Dashed Lines (short intermediates) - Percent frequency of wave heights <8 feet (<2.4 meters)

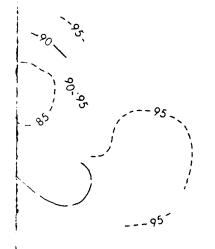


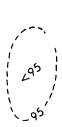


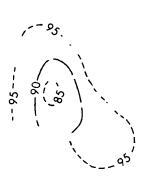
Solid Lines (dotted intermediates) - Percent frequency of wave heights <5 feet (<1.5 meters)

Dashed Lines (short intermediates) - Percent frequency of wave heights <8 feet (<2.4 meters)

OCTOBER



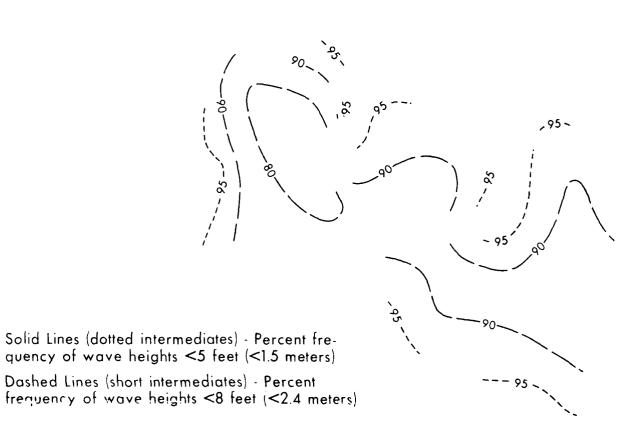




ent fremeters) cent 4 meters)

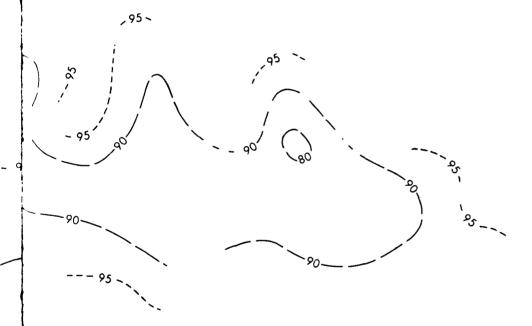
23 B

NOVEMBER



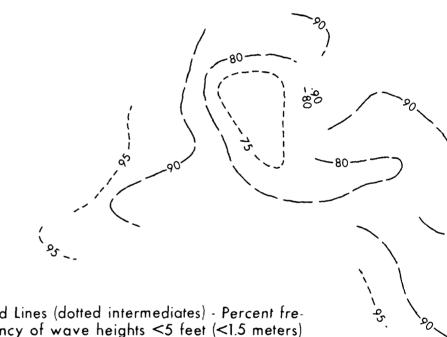
24 /

WAVE HEIGHT (<5 AND <8 FEET)



29 3

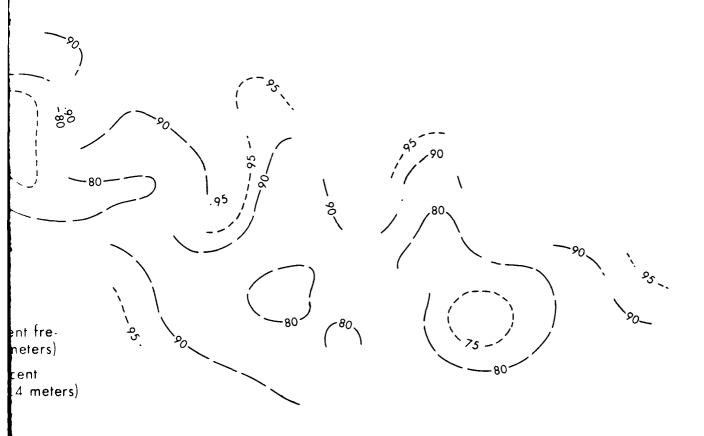
WAVE HEIGHT (<5 AND <8 FEET)



Solid Lines (dotted intermediates) - Percent frequency of wave heights <5 feet (<1.5 meters)

Dashed Lines (short intermediates) - Percent frequency of wave heights <8 feet (<2.4 meters)

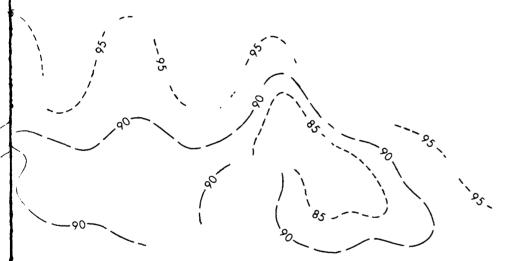
DECEMBER



Solid Lines (dotted intermediates) - Percent frequency of wave heights <5 feet (<1.5 meters)

Dashed Lines (short intermediates) - Percent frequency of wave heights <8 feet (<2.4 meters)

WAVE HEIGHT (<5 AND <8 FEET)



/-

- Percent fret (≥3.7 meters)

Solid Lines (dotted intermediates) - Percent frequency of wave heights ≥12 feet (≥3.7 meters)

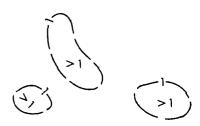
Dashed Lines - Percent frequency of wave

heights ≥20 feet (≥6.1 meters)

15

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FEBRUARY WAV



Solid Lines (dotted intermediates) - Percent frequency of wave heights ≥12 feet (≥3.7 meters)

Dashed Lines - Percent frequency of wave heights ≥20 feet (≥6.1 meters)





680

Solid Lines (dotted intermediates) - Percent frequency of wave heights ≥12 feet (≥3.7 meters)

Dashed Lines - Percent frequency of wave heights ≥20 feet (≥6.1 meters)

241



EET)

MARCH

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APRIL



Solid Lines (dotted intermediates) - Percent frequency of wave heights ≥12 feet (≥3.7 meters)

Dashed Lines - Percent frequency of wave heights ≥20 feet (≥6.1 meters)

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Solid Lines (dotted intermediates) - Percent frequency of wave heights ≥12 feet (≥3.7 meters)

Dashed Lines - Percent frequency of wave heights ≥20 feet (≥6.1 meters)

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Solid Lines (dotted intermediates) - Percent frequency of wave heights ≥12 feet (≥3.7 meters)

Dashed Lines - Percent frequency of wave heights ≥20 feet (≥6.1 meters)

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Solid Lines (dotted intermediates) - Percent frequency of wave heights ≥12 feet (≥3.7 meters)

Dashed Lines - Percent frequency of wave heights ≥20 feet (≥6.1 meters)

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AUGUST

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Solid Lines (dotted intermediates) - Percent frequency of wave heights ≥12 feet (≥3.7 meters)

Dashed Lines - Percent frequency of wave heights ≥20 feet (≥6.1 meters)

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Solid Lines (dotted intermediates) - Percent frequency of wave heights ≥12 feet (≥3.7 meters)

Dashed Lines - Percent frequency of wave heights ≥20 feet (≥6.1 meters)

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OCTOBER

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Solid Lines (dotted intermediates) - Percent frequency of wave heights ≥12 feet (≥3.7 meters)

Dashed Lines - Percent frequency of wave heights ≥20 feet (≥6.1 meters)

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368

Solid Lines (dotted intermediates) - Percent frequency of wave heights ≥12 feet (≥3.7 meters)

Dashed Lines - Percent frequency of wave heights ≥20 feet (≥6.1 meters)

27A

NOVEMBER

nt freneters)

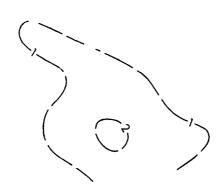
37 B

DECEMBER



Solid Lines (dotted intermediates) - Percent frequency of wave heights ≥12 feet (≥3.7 meters)

Dashed Lines - Percent frequency of wave heights ≥20 feet (≥6.1 meters)



0.0

< 1

Solid Lines (dotted intermediates) - Percent frequency of wave heights ≥12 feet (≥3.7 meters)

Dashed Lines - Percent frequency of wave heights ≥20 feet (≥6.1 meters)

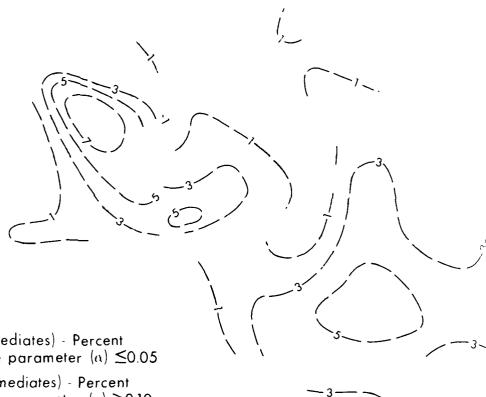
291

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39 F



Solid Lines (dotted intermediates) - Percent frequency of wave slope parameter (a) \leq 0.05

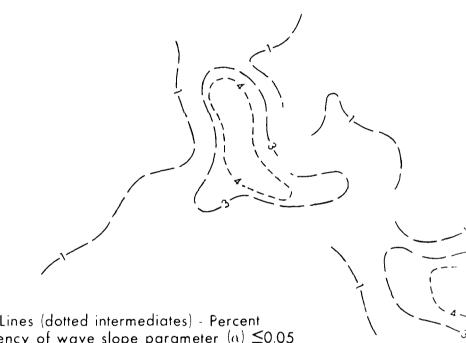
Dashed Lines (short intermediates) - Percent frequency of wave slope parameter (α) \geq 0.10

WAVE SLOPE (α) (\leq 0.05 AND \geq 0.10)



40B

WAVE SLOPE (α) (\leq 0.05 AND \geq 0.10)



Solid Lines (dotted intermediates) - Percent frequency of wave slope parameter (a) \leq 0.05

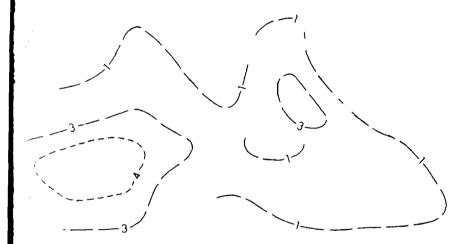
Dashed Lines (short intermediates) - Percent frequency of wave slope parameter (a) ≥ 0.10

FEBRUARY





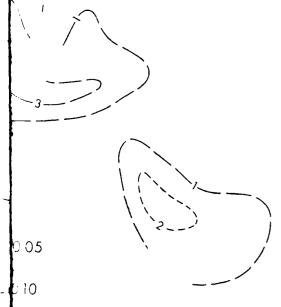
Solid Lines 'dotted intermediates' - Percent frequency of wave slope parameter (a) \leq 0.05 Dashed Lines (short intermediates) - Percent frequency of wave slope parameter (a) \geq 0.10



3-7

Solid Lines (dotted intermediates) - Percent frequency of wave slope parameter (a) ≤ 0.05

Dashed Lines (short intermediates) - Percent frequency of wave slope parameter $(\alpha) \ge 0.10$







Solid Lines (dotted intermediates) - Percent frequency of wave slope parameter (α) \leq 0.05 Dashed Lines (short intermediates) - Percent frequency of wave slope parameter (α) \geq 0.10





>1

44 B



Solid Lines (dotted intermediates) - Percent frequency of wave slope parameter (α) \leq 0.05 Dashed Lines (short intermediates) - Percent frequency of wave slope parameter (α) \geq 0.10

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10)

JUNE

ent ≤0.05 ent ≥0.10

45 F

JULY





Solid Lines (dotted intermediates) - Percent frequency of wave slope parameter (α) \leq 0.05 Dashed Lines (short intermediates) - Percent frequency of wave slope parameter (α) \geq 0.10





46P



Solid Lines (dotted intermediates) - Percent frequency of wave slope parameter $(\alpha) \leq 0.05$ Dashed Lines (short intermediates) - Percent frequency of wave slope parameter $(\alpha) \geq 0.10$

AUGUST

0.5

.10

47B

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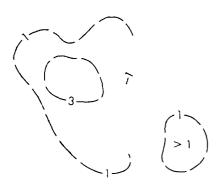
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SEPTEMBER WAV



Solid Lines (dotted intermediates) - Percent frequency of wave slope parameter (α) \leq 0.05 Dashed Lines (short intermediates) - Percent frequency of wave slope parameter (α) \geq 0.10





Solid Lines (dotted intermediates) - Percent frequency of wave slope parameter $(a) \le 0.05$ Dashed Lines (short intermediates) - Percent frequency of wave slope parameter $(a) \ge 0.10$

OCTOBER



ent ≤0.05 cent ≥0.10

49 -

NOVEMBER

ates) - Percent

Solid Lines (dotted intermediates) - Percent frequency of wave slope parameter (α) \leq 0.05

Dashed Lines (short intermediates) - Percent frequency of wave slope parameter (a) \geq 0.10





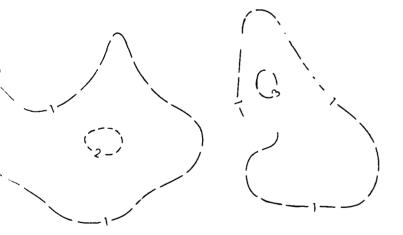
Solid Lines (dotted intermediates) - Percent frequency of wave slope parameter (a) \leq 0.05

Dashed Lines (short intermediates) - Percent frequency of wave slope parameter (a) \geq 0.10

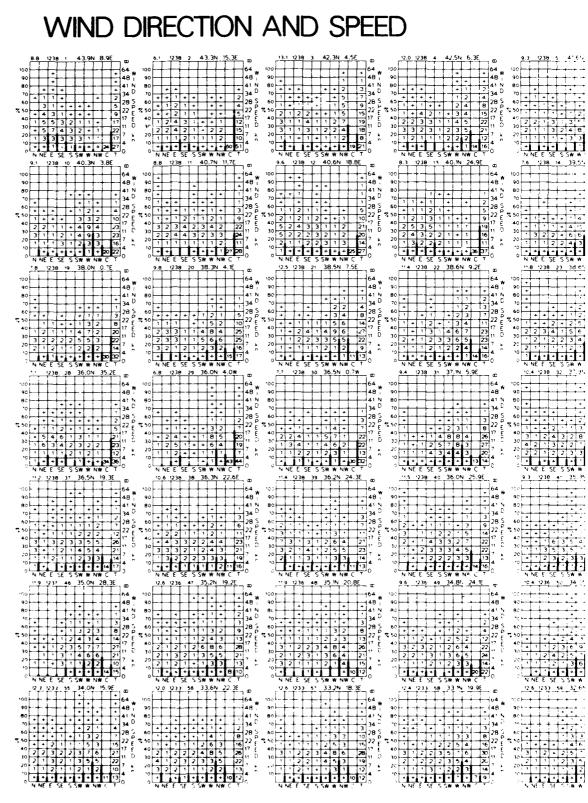


Solid Lines (dotted intermediates) - Percent frequency of wave slope parameter (a) ≤0.05

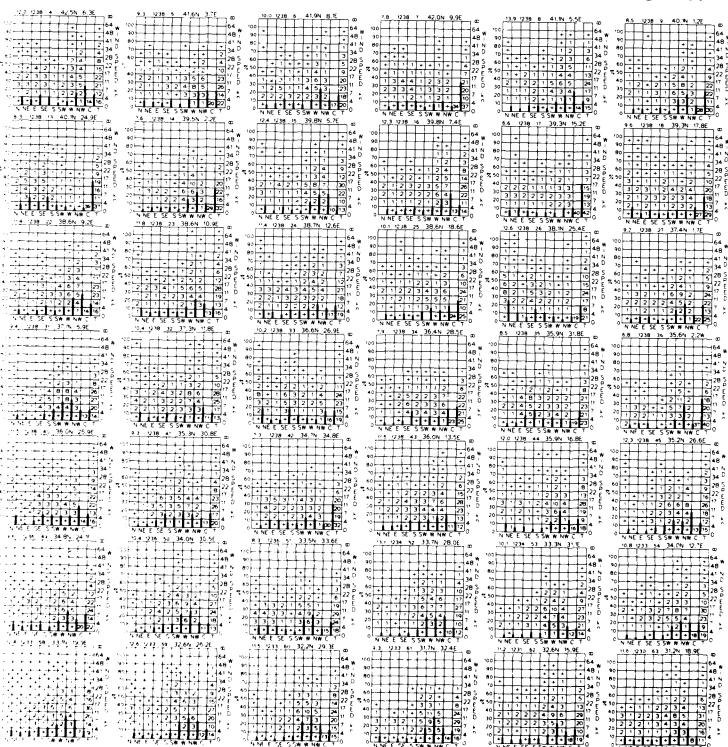
Dashed Lines (short intermediates) - Percent frequency of wave slope parameter (a) ≥0.10

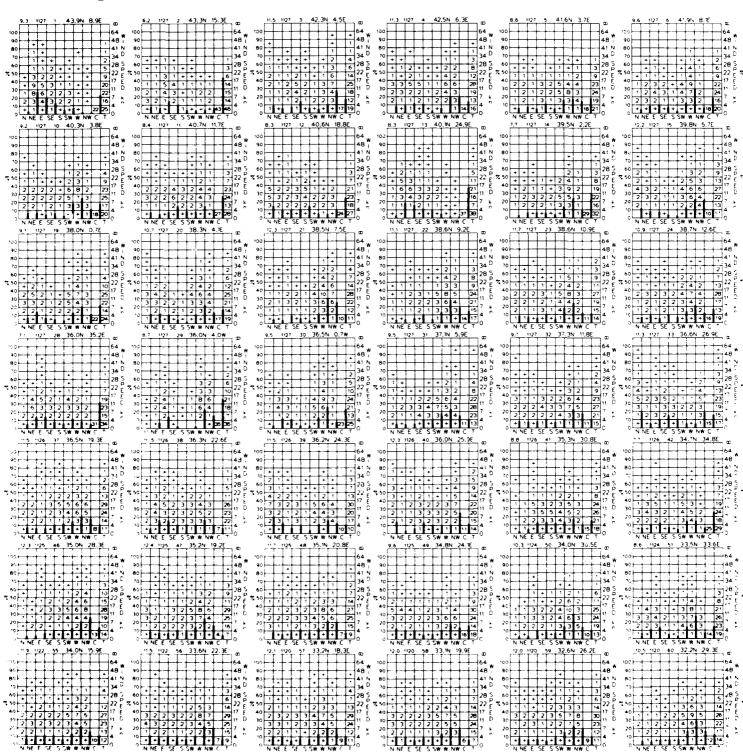


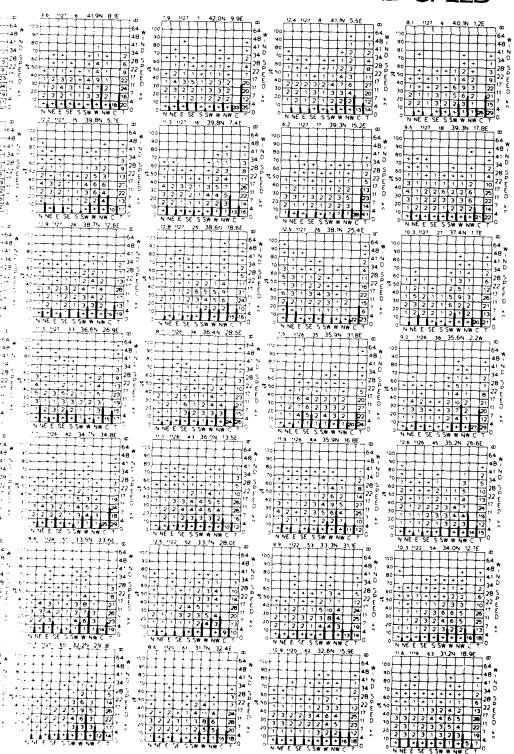
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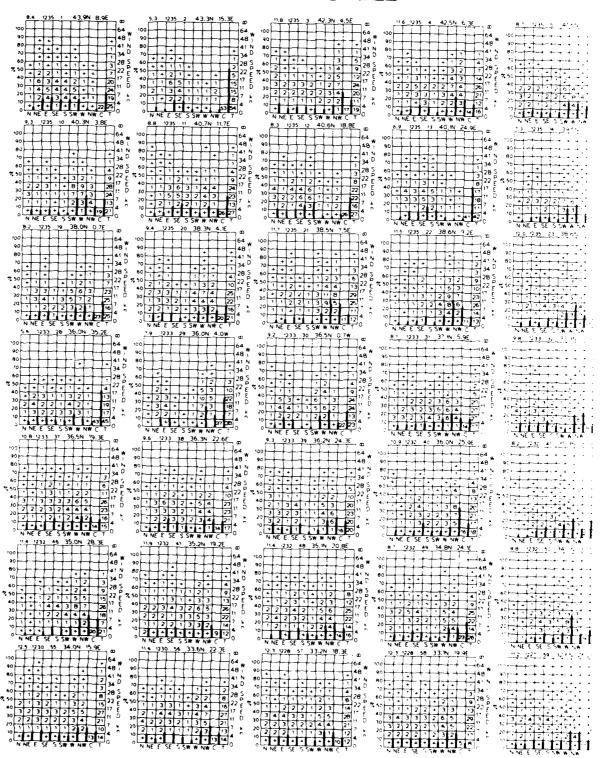


JANUARY

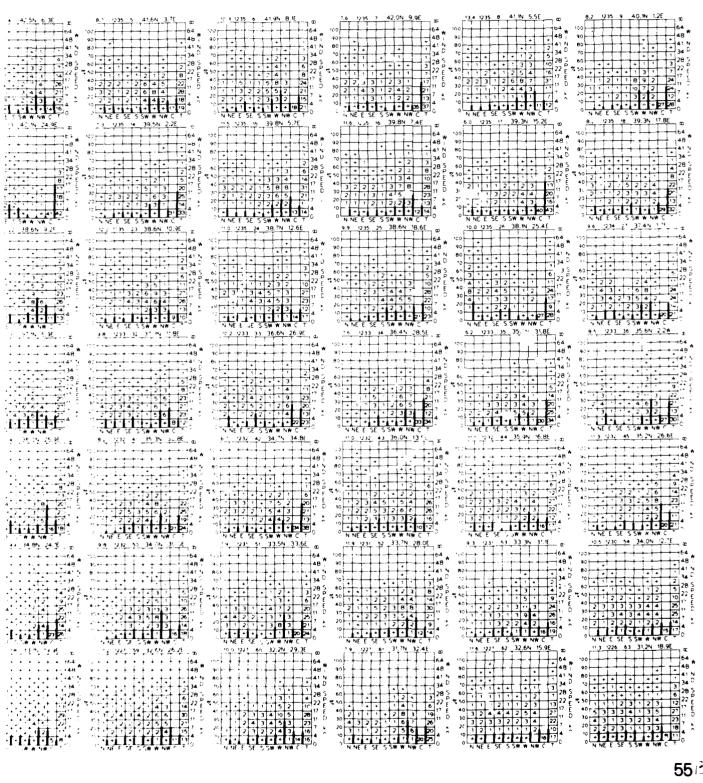


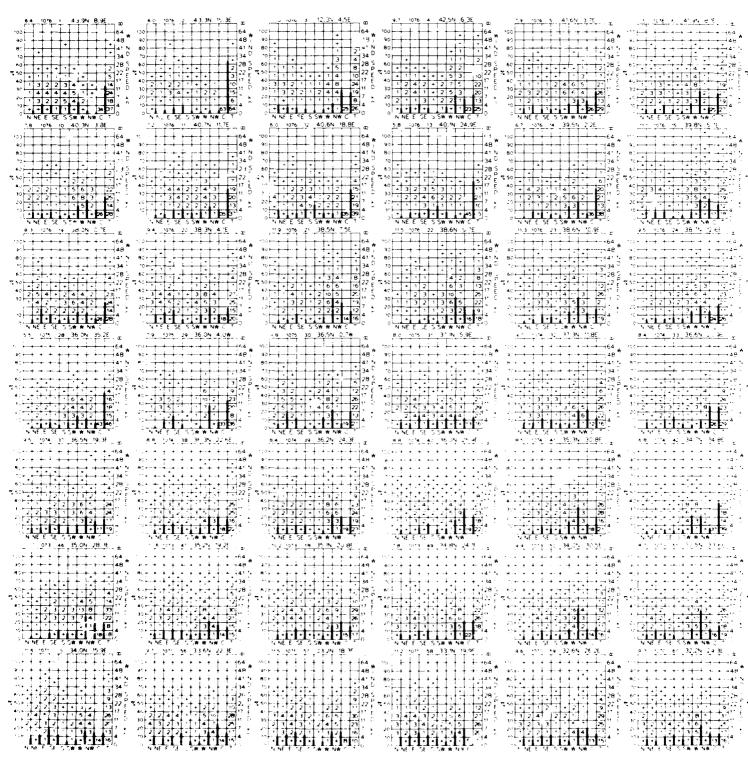


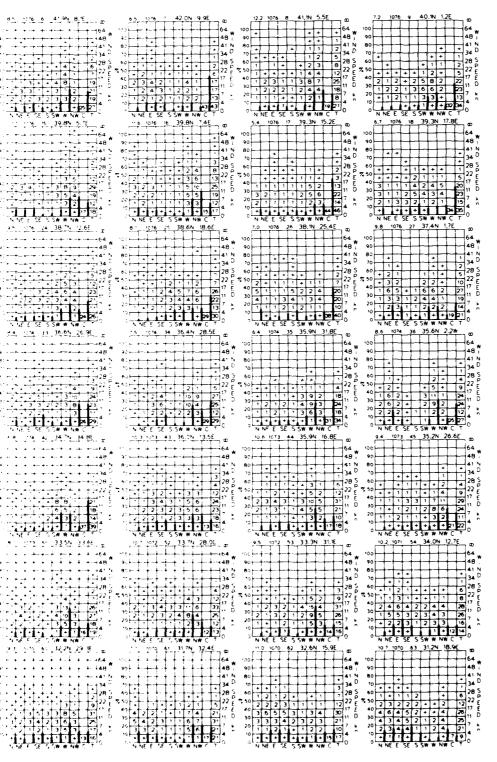


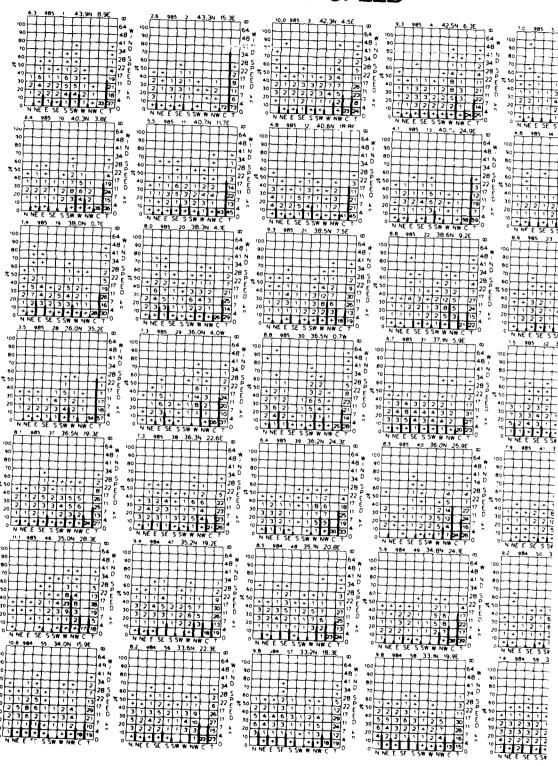


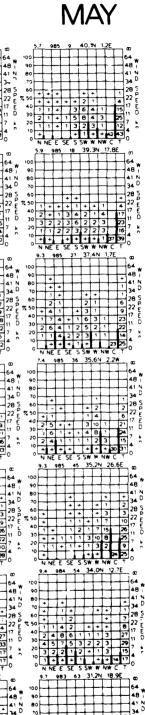
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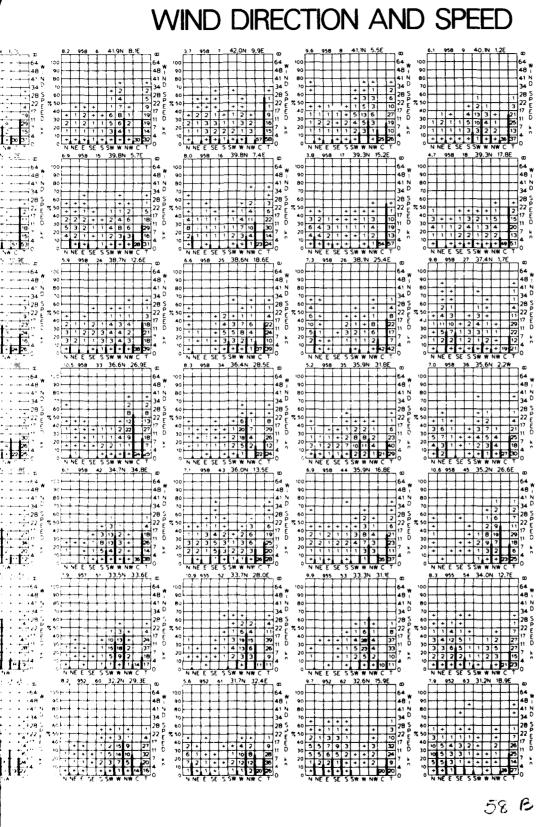


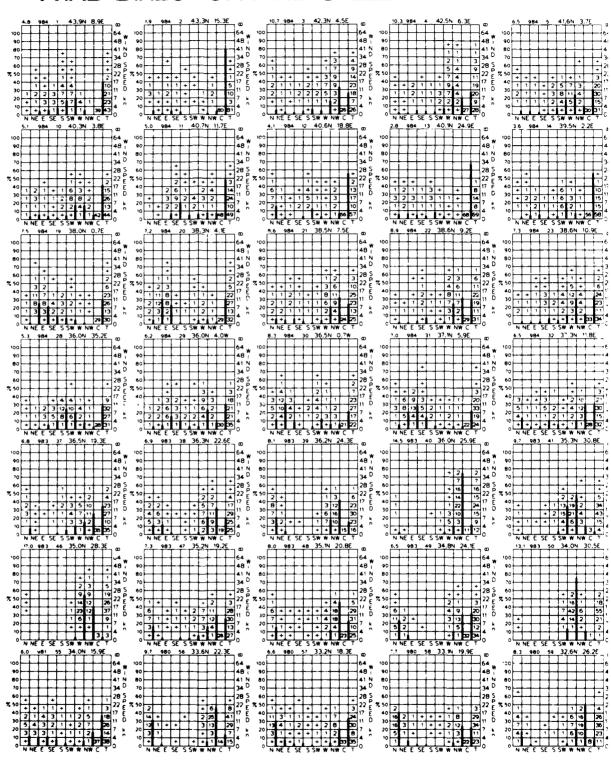


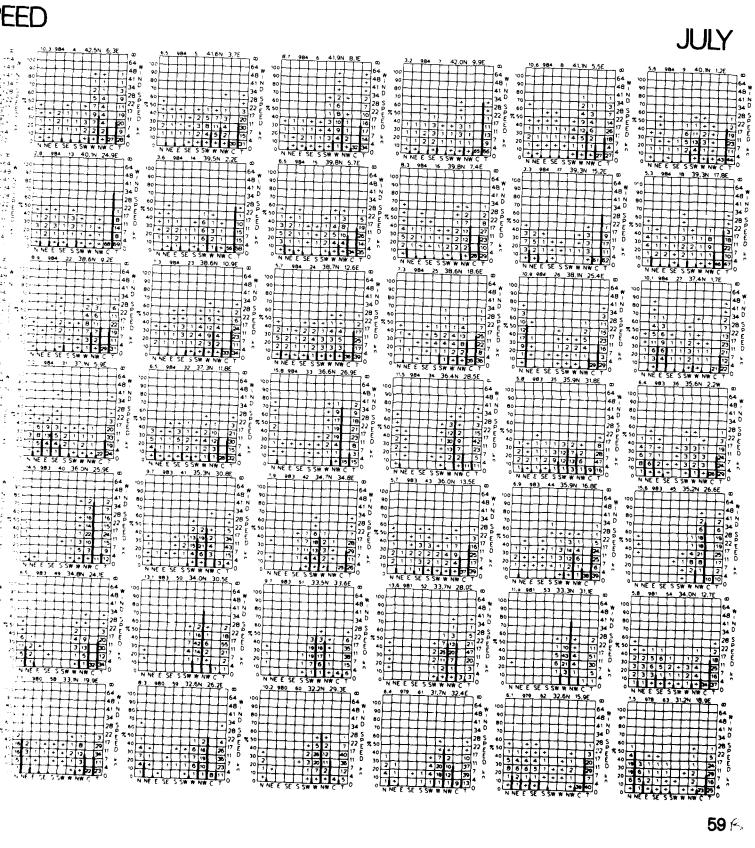


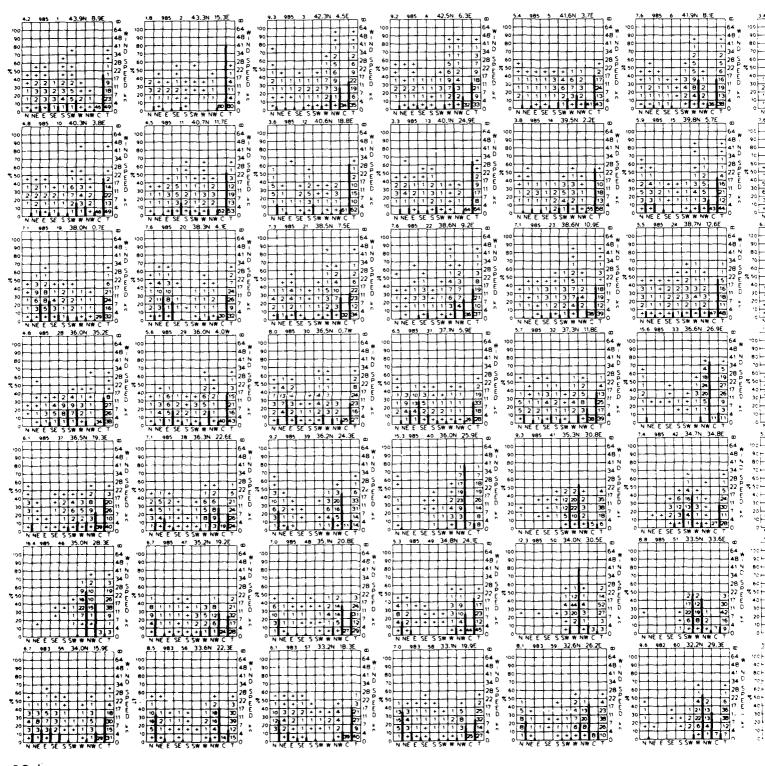
JUNE

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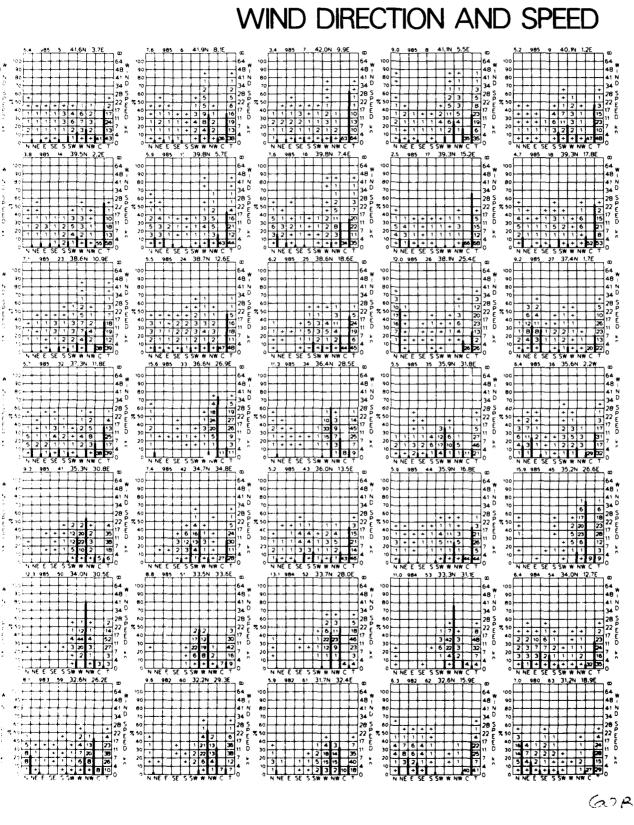




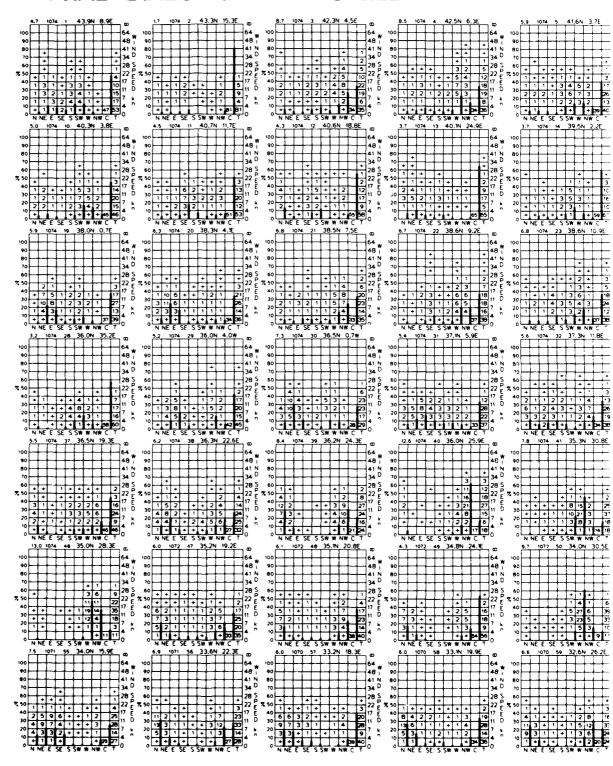




WIND DIRECTION AND SPEED



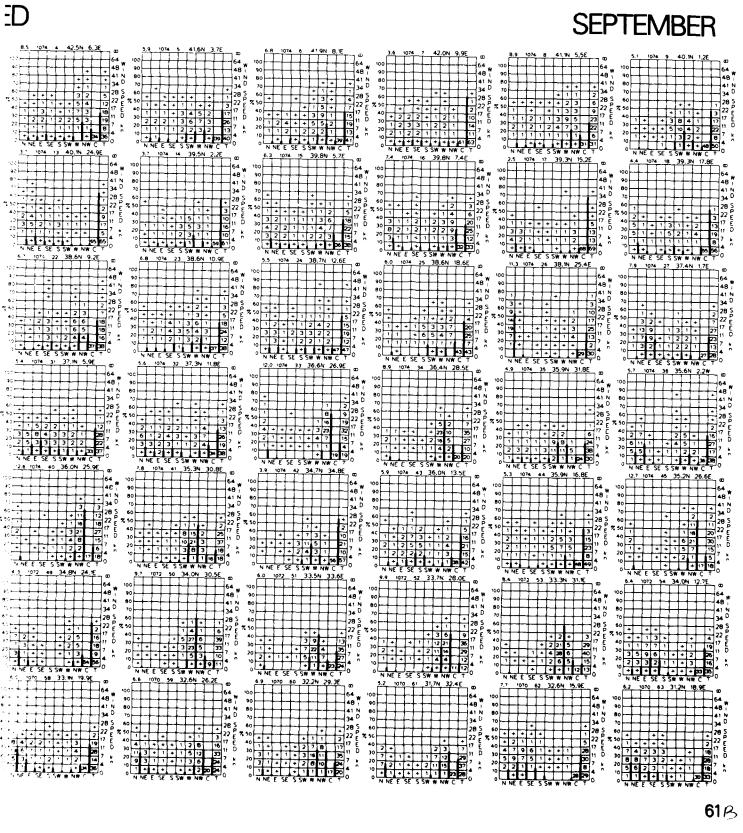
WIND DIRECTION AND SPEED



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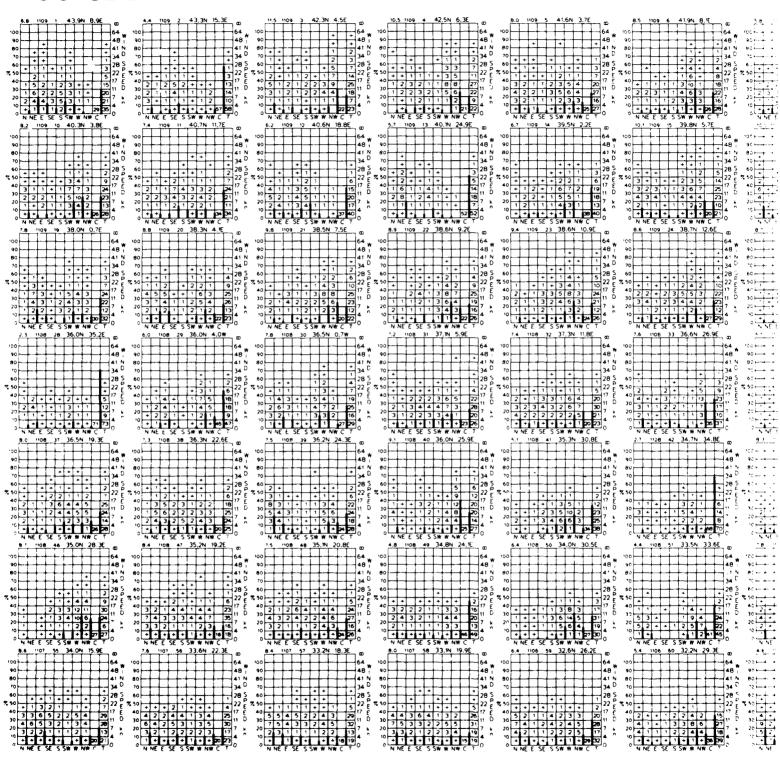
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SEPTEMBER

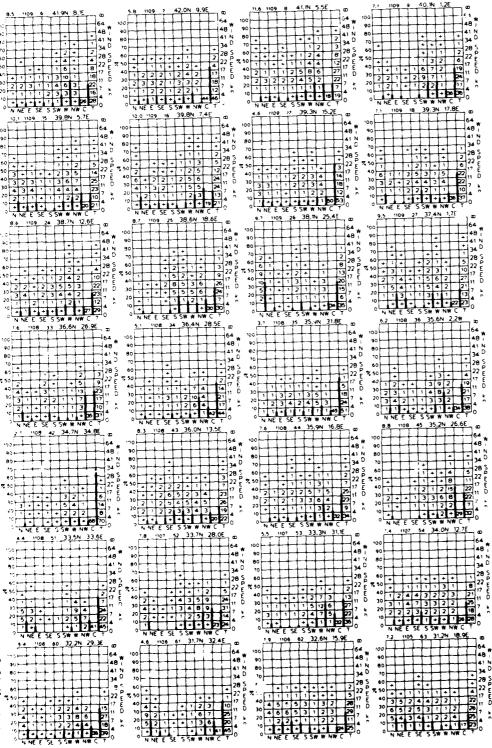


OCTOBER

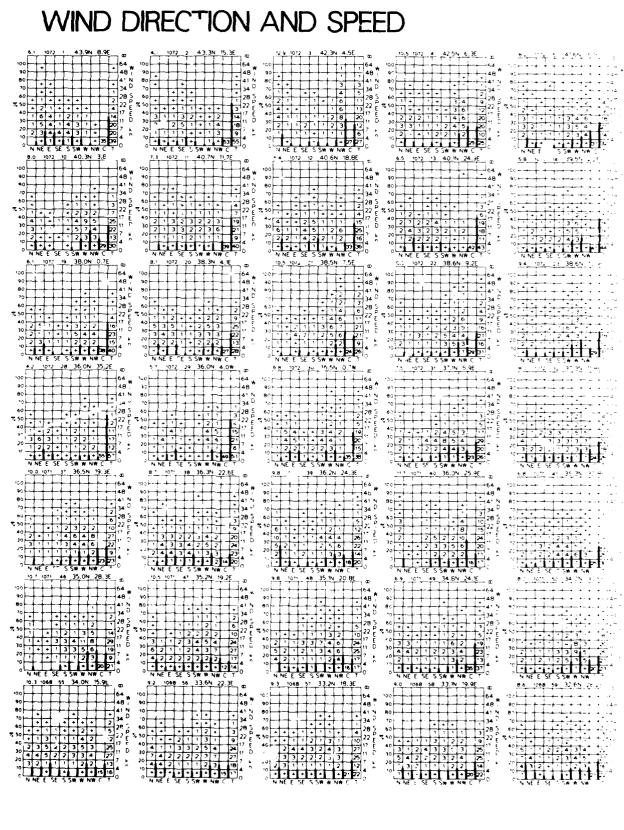
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WIND DIRECTION AND SPEED



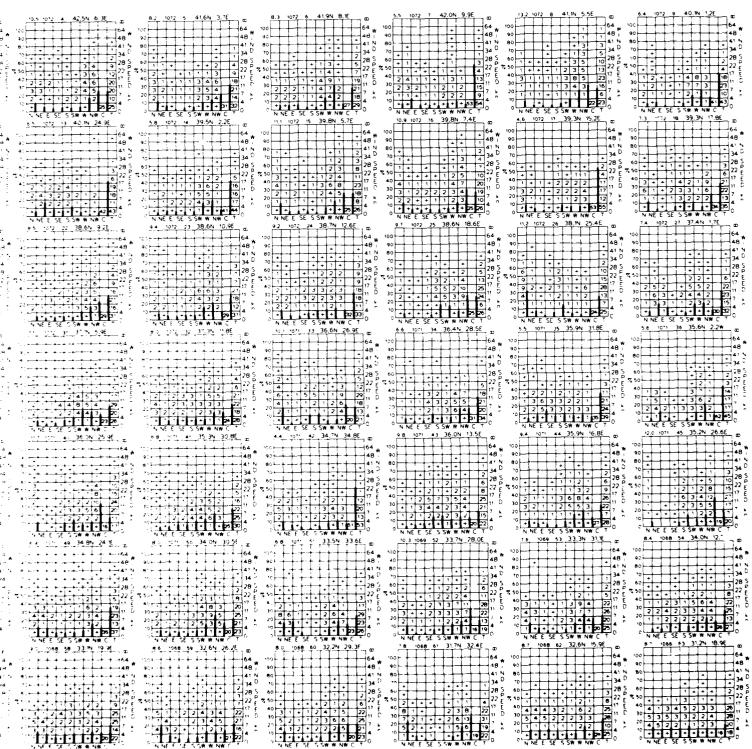
WIND DIRECTION AND SPEED



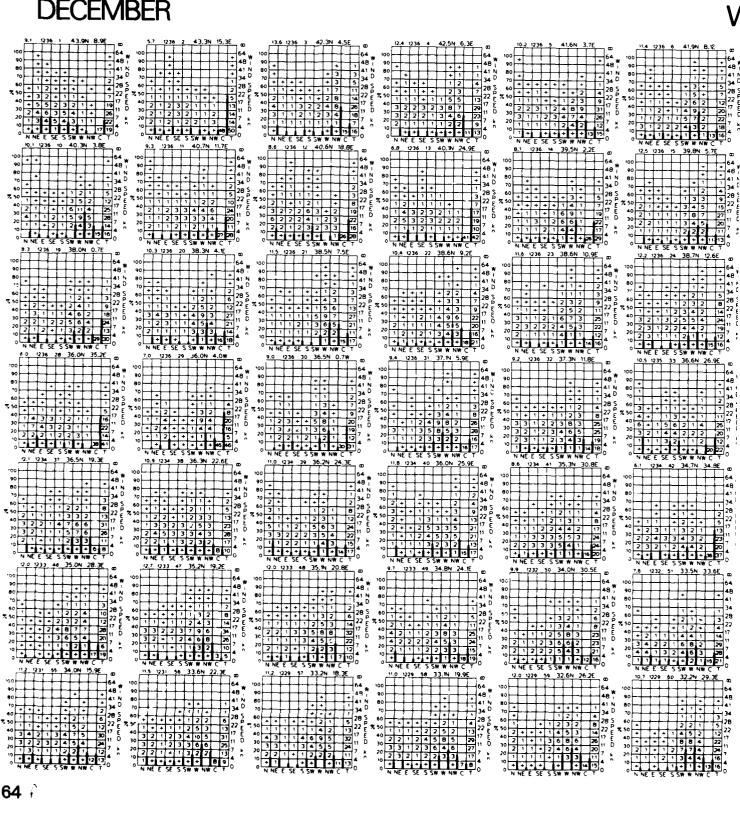
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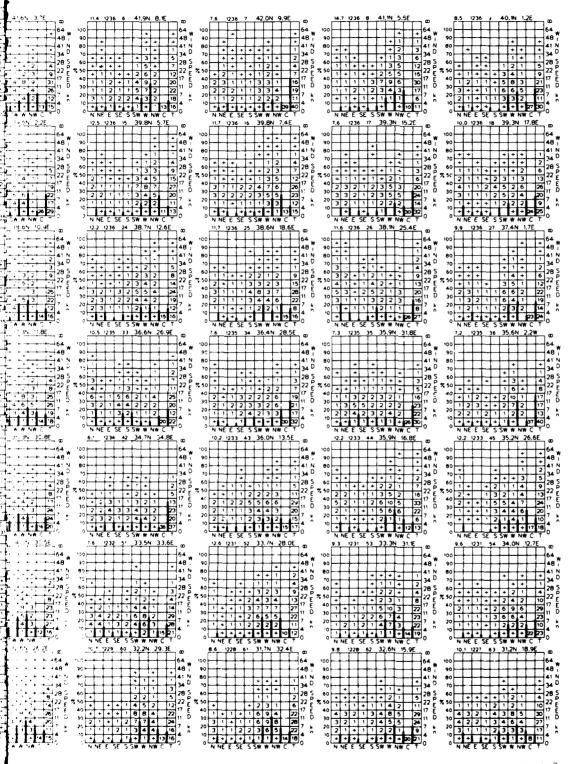
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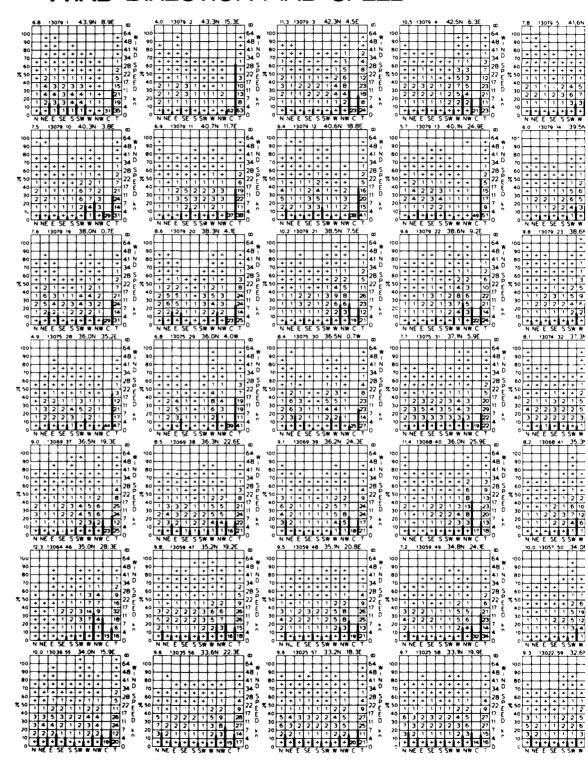
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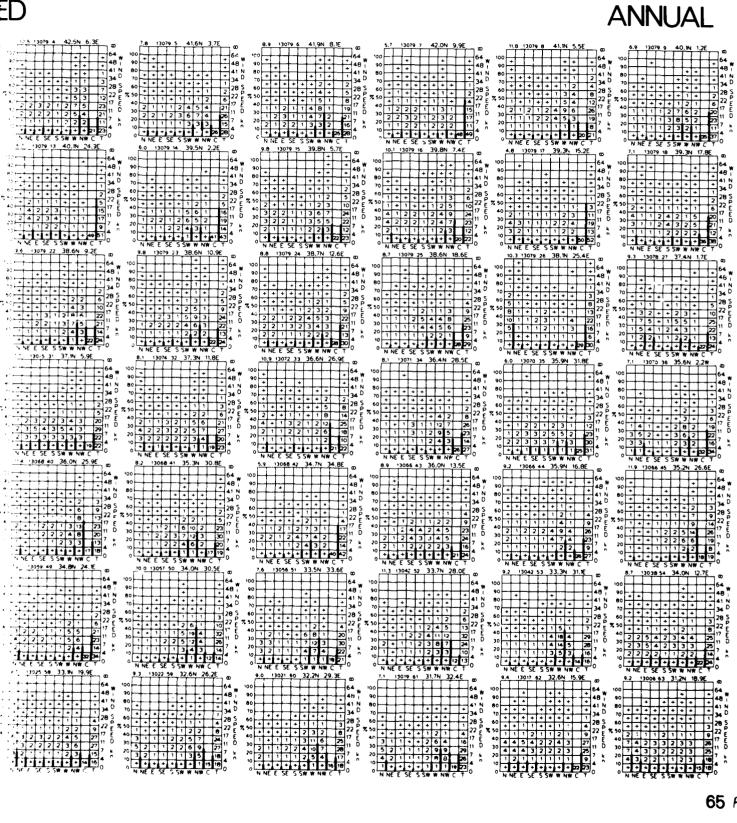
WIND DIRECTION AND SPEED



WIND DIRECTION AND SPEED

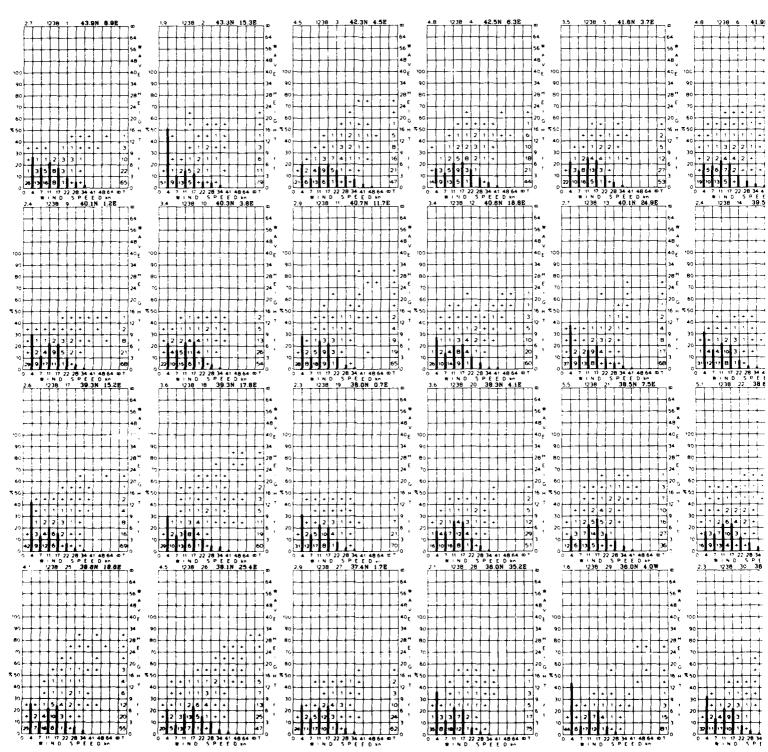


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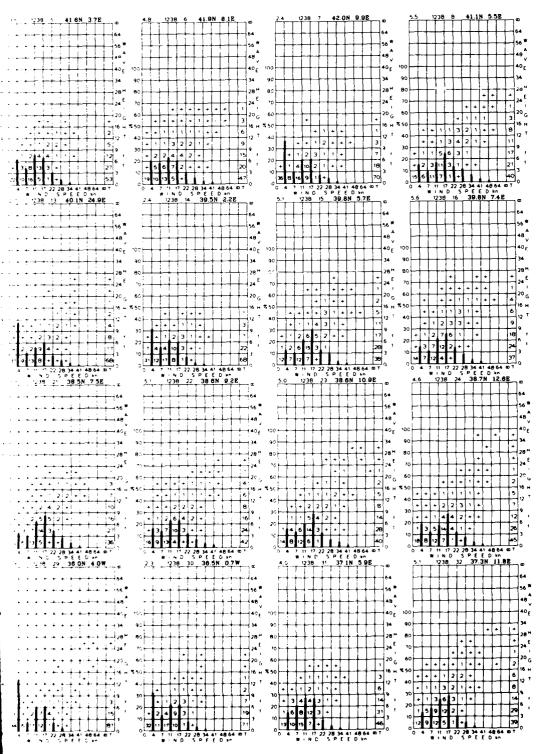


JANUARY

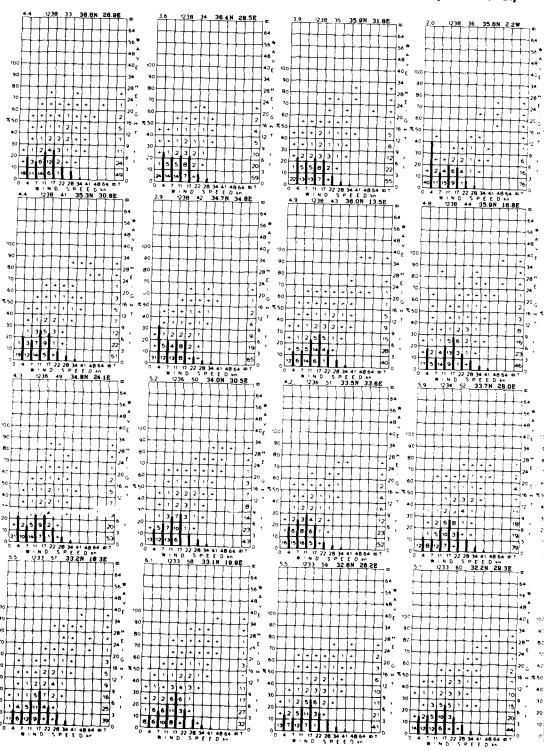
WAVE HE



WAVE HEIGHT AND WIND SPEED



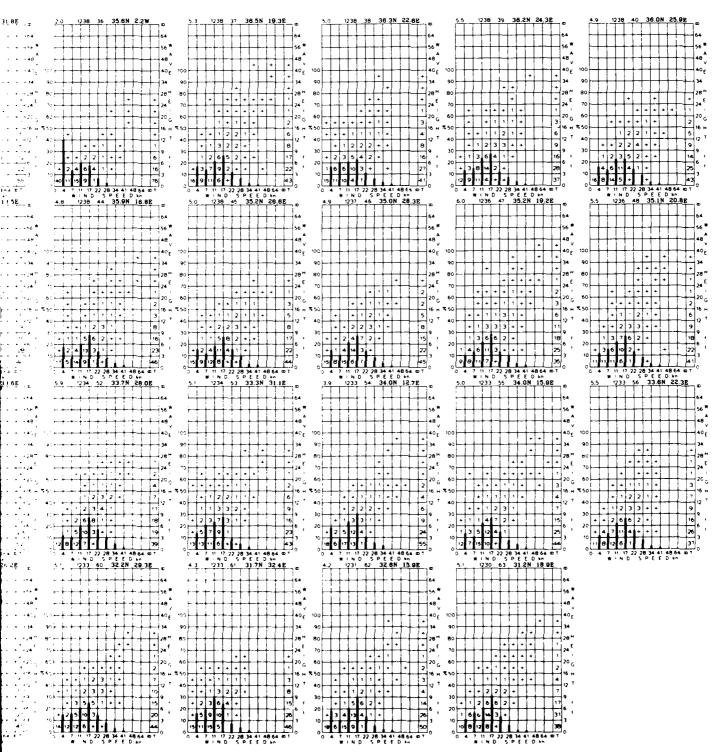
WAVE HEIGHT AND WIND SPEED (Cont'd)



67 A

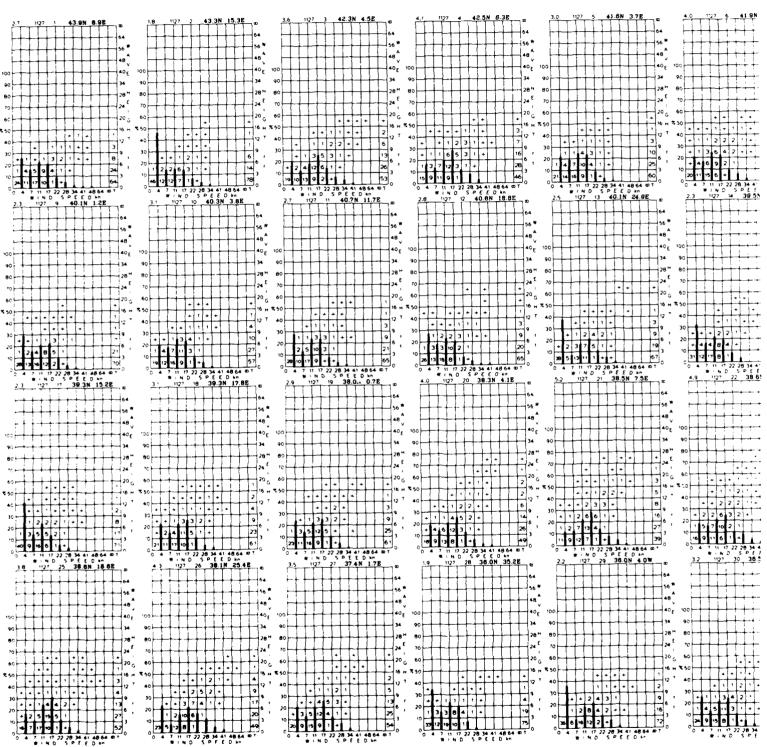
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JANUARY

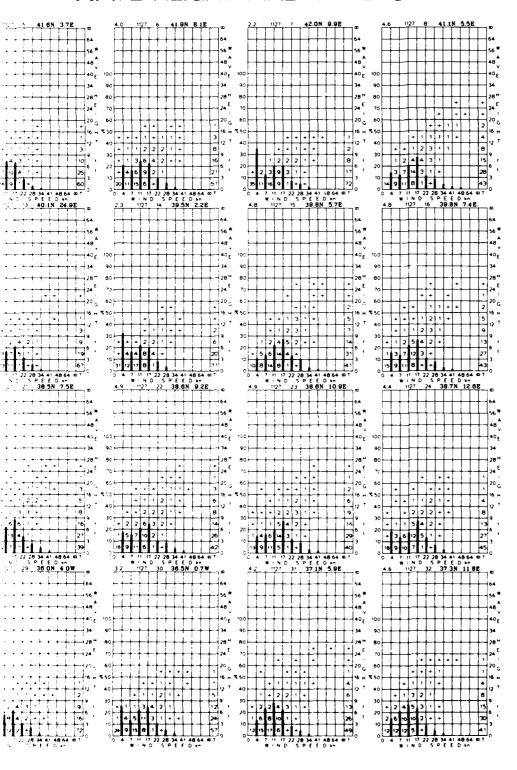


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WAVE HEI

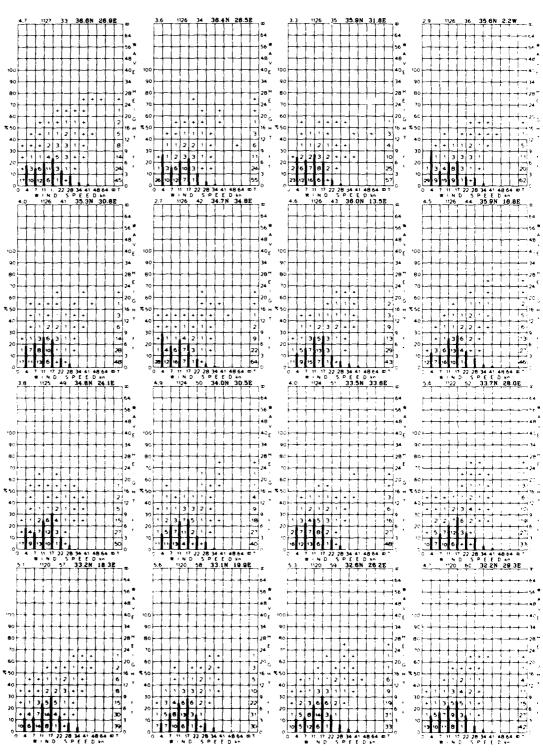


WAVE HEIGHT AND WIND SPEED



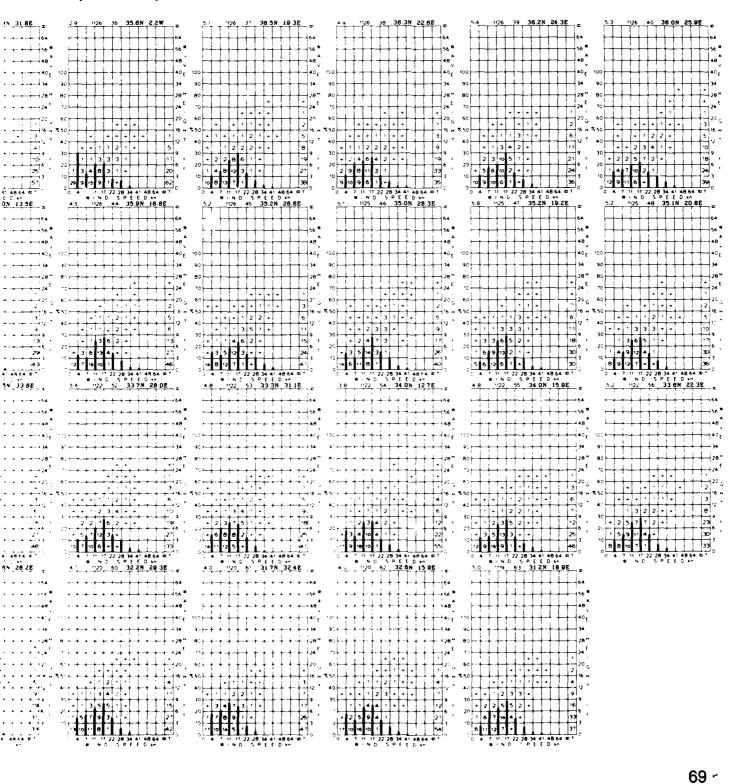
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WAVE HEIGHT AND WIND SPEED (Cont'd)



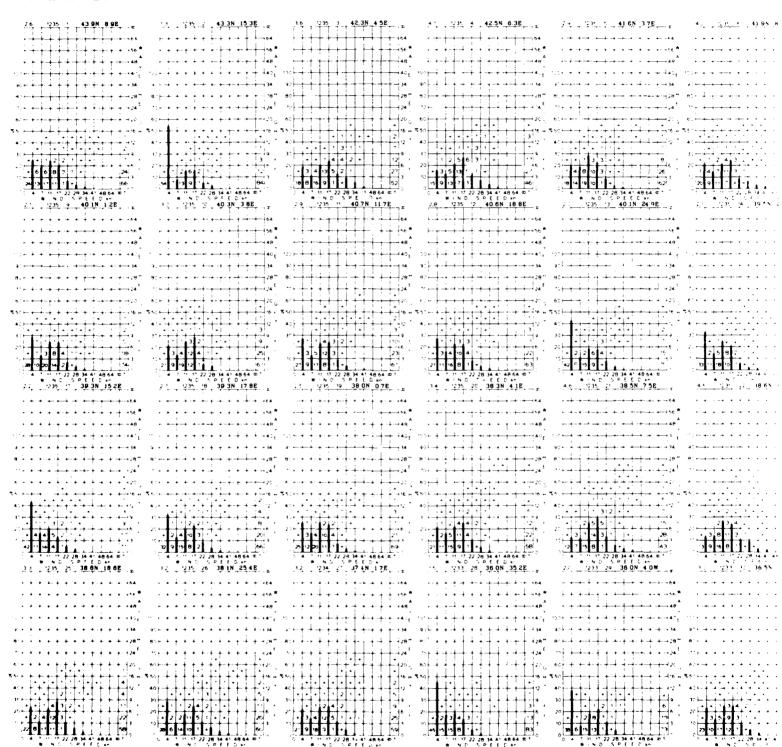
PEED (Cont'd)

FEBRUARY

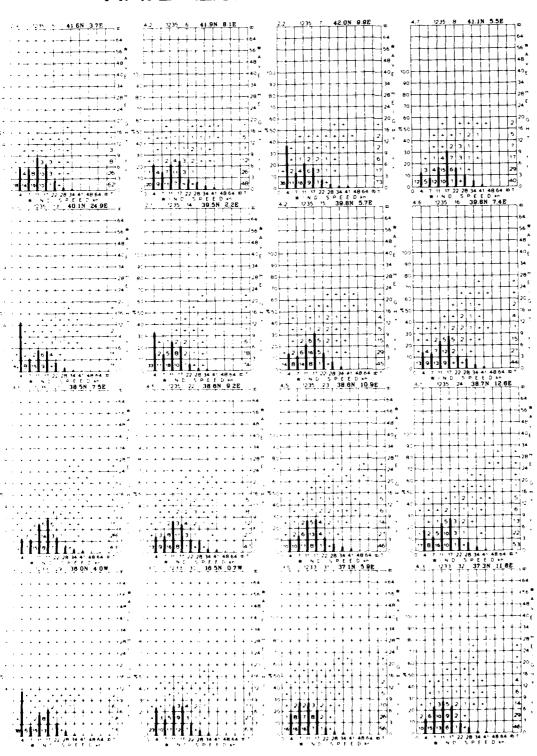


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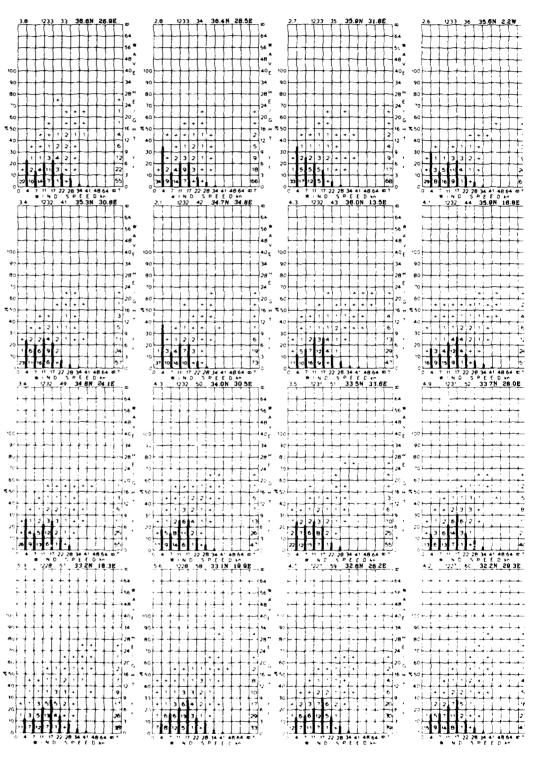
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WAVE HEIGHT AND WIND SPEED

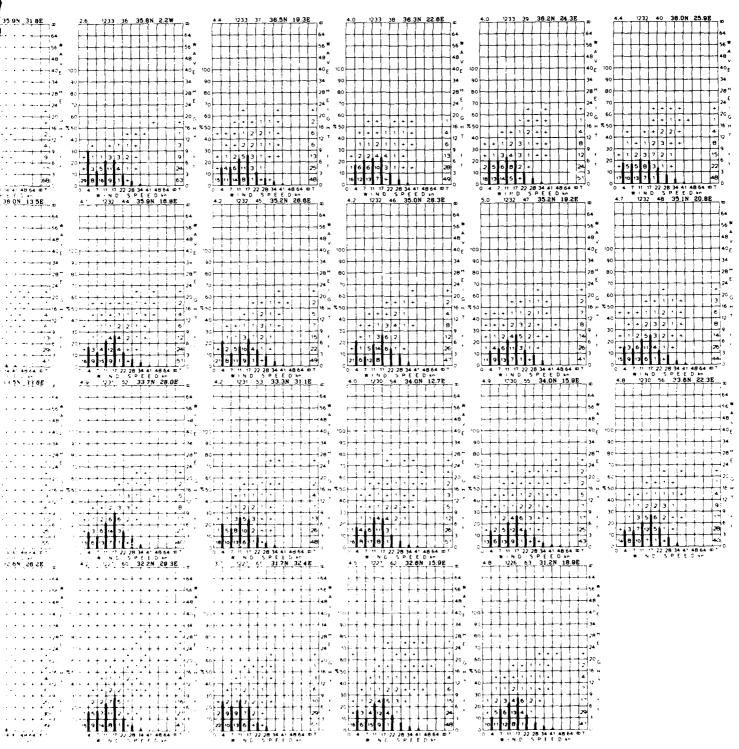


WAVE HEIGHT AND WIND SPEED (Cont'd)



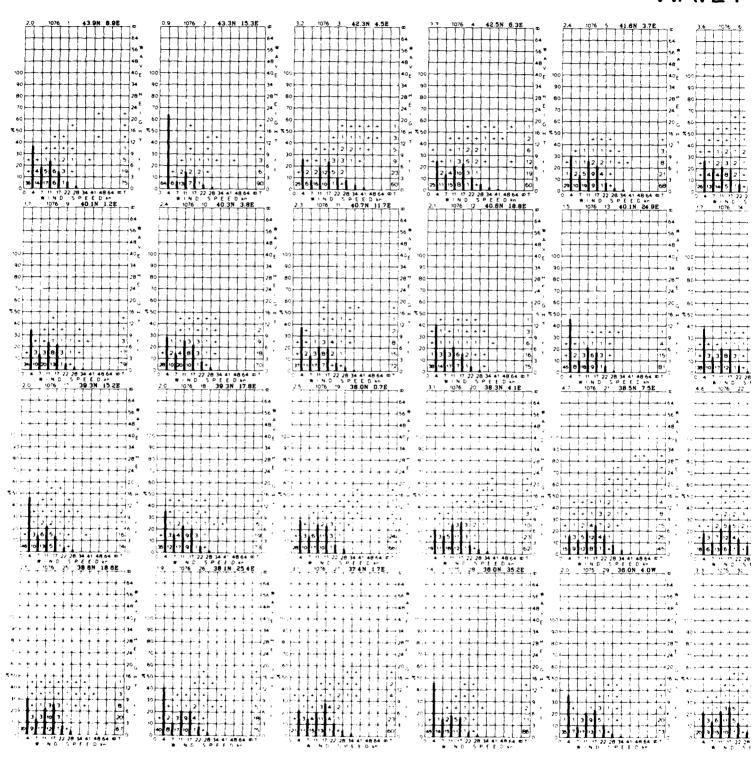
SPEED (Cont'd)

MARCH

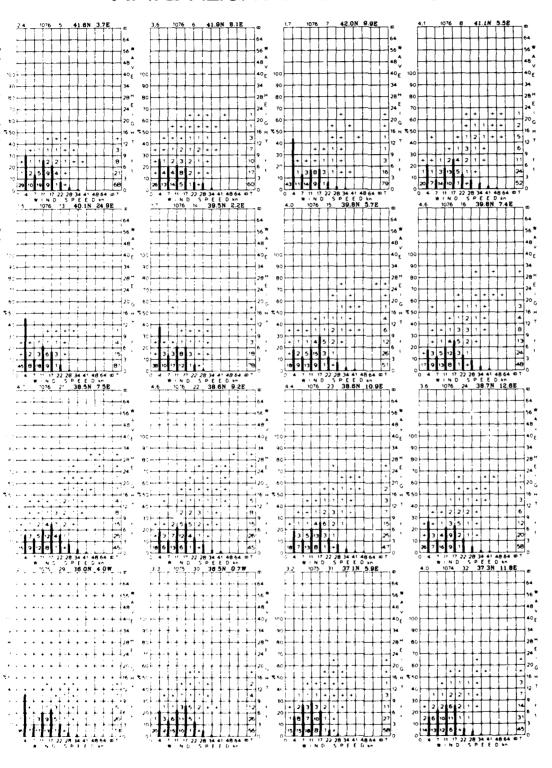


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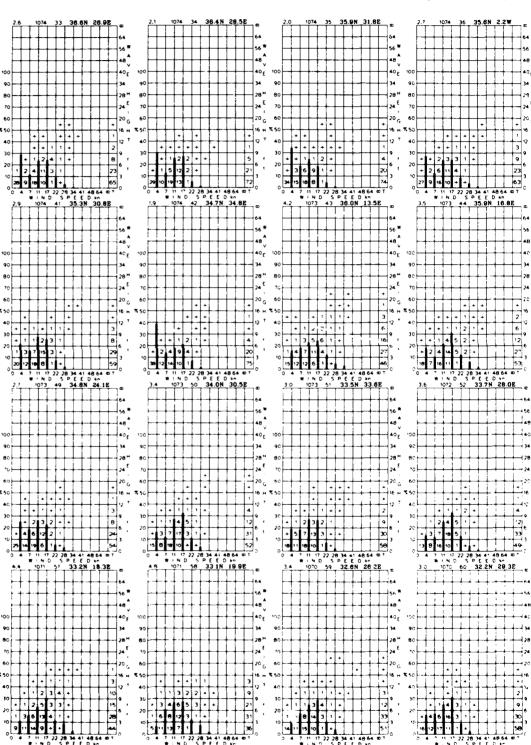
WAVE +

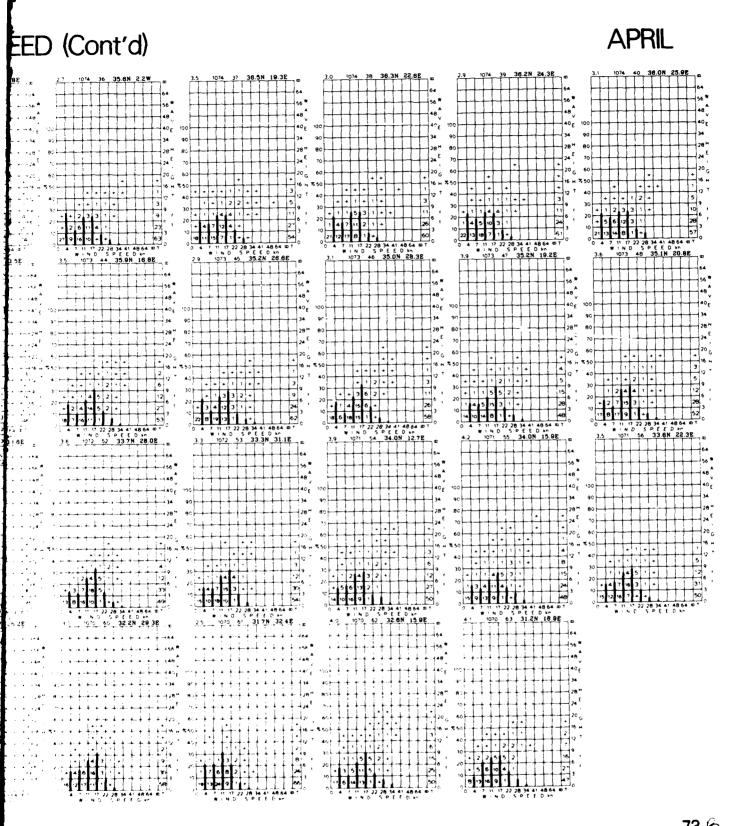


WAVE HEIGHT AND WIND SPEED



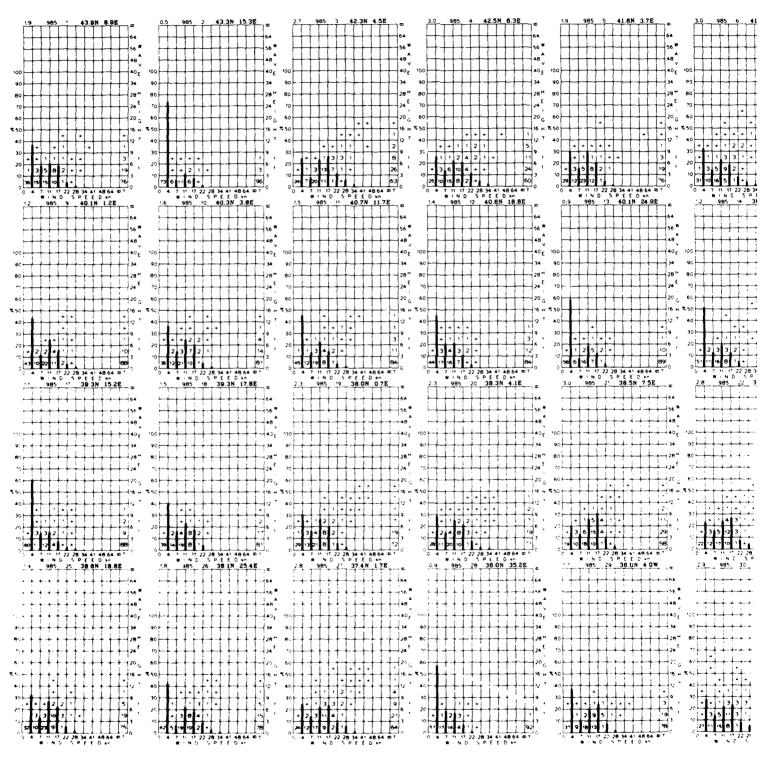
WAVE HEIGHT AND WIND SPEED (Cont'd)



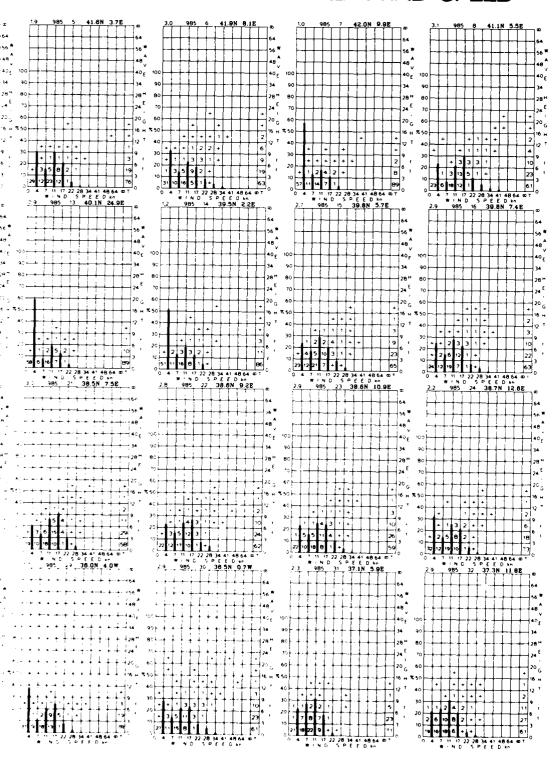


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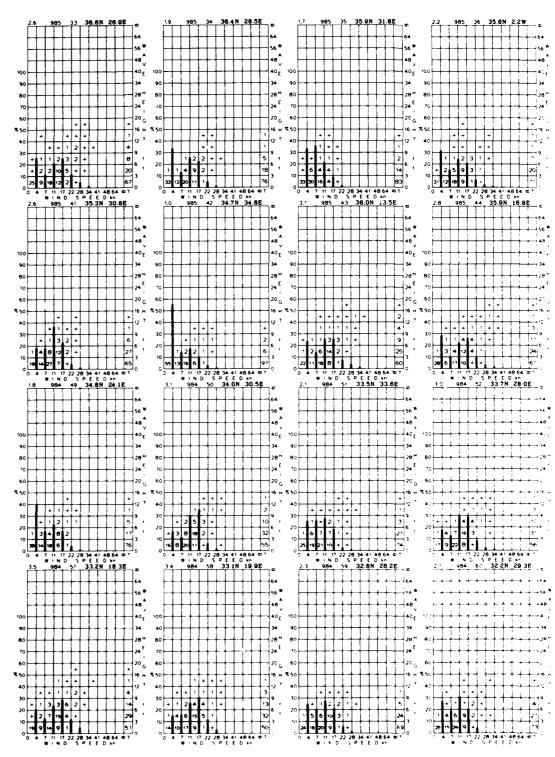
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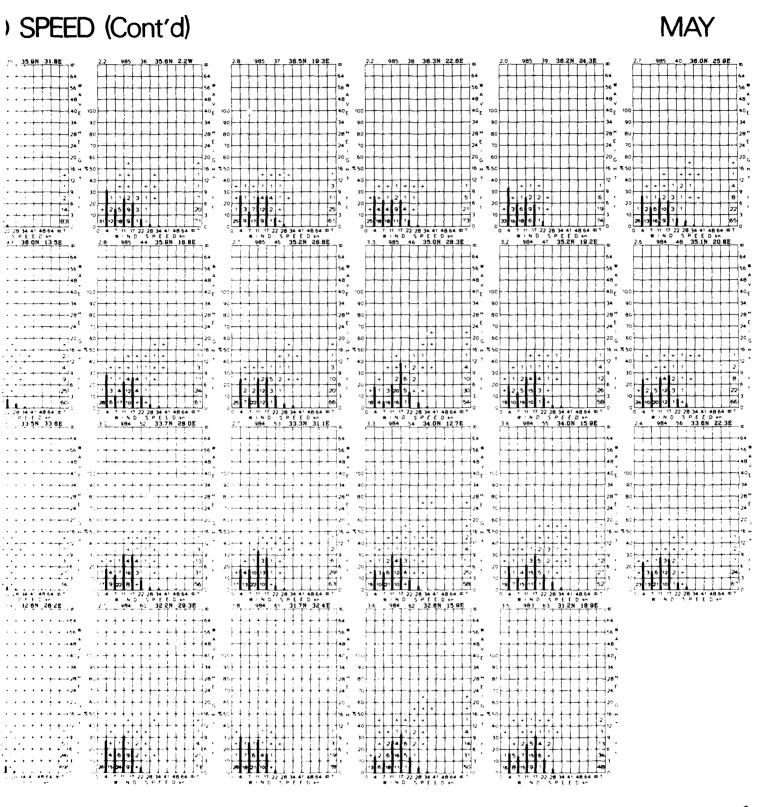


WAVE HEIGHT AND WIND SPEED



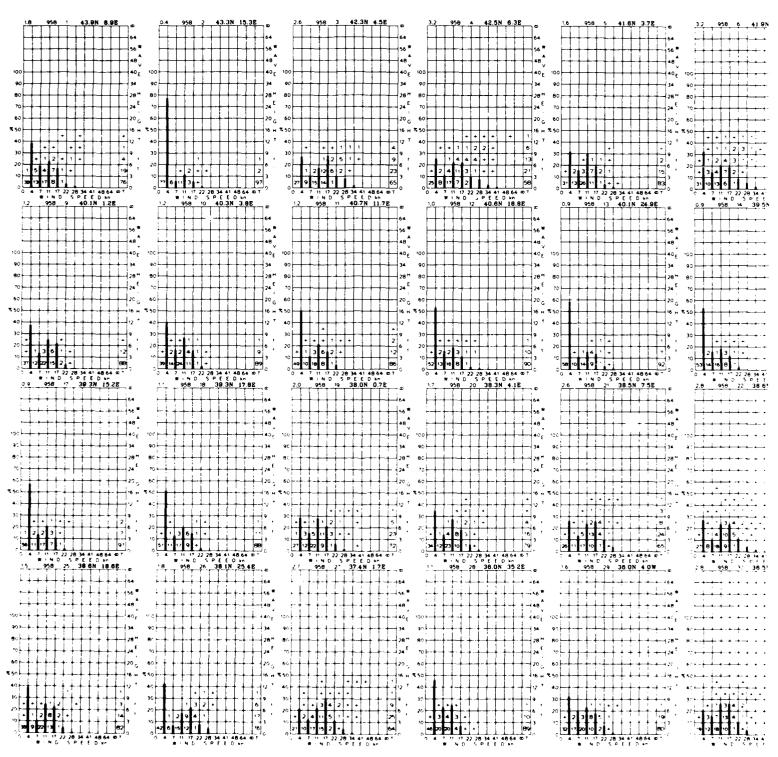
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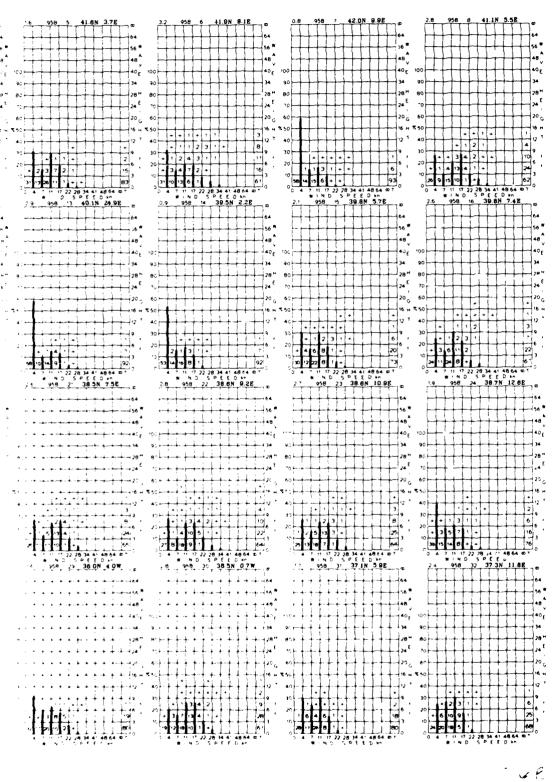


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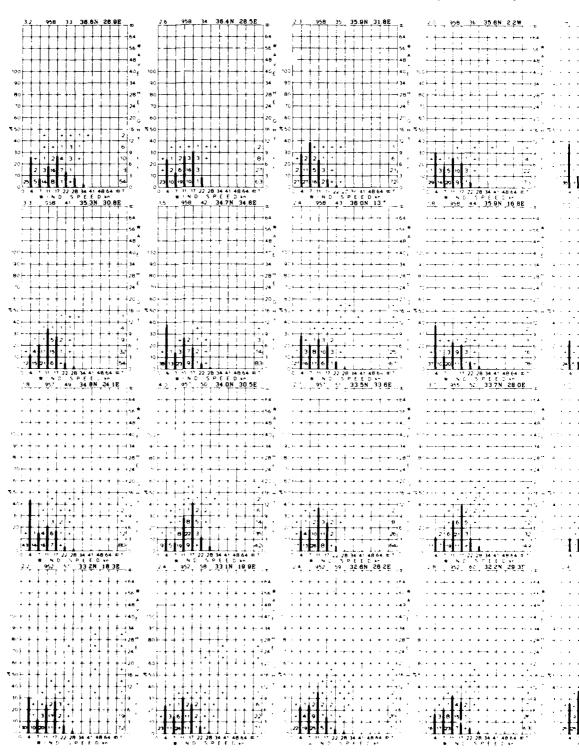
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WAVE HEIGHT AND WIND SPEED



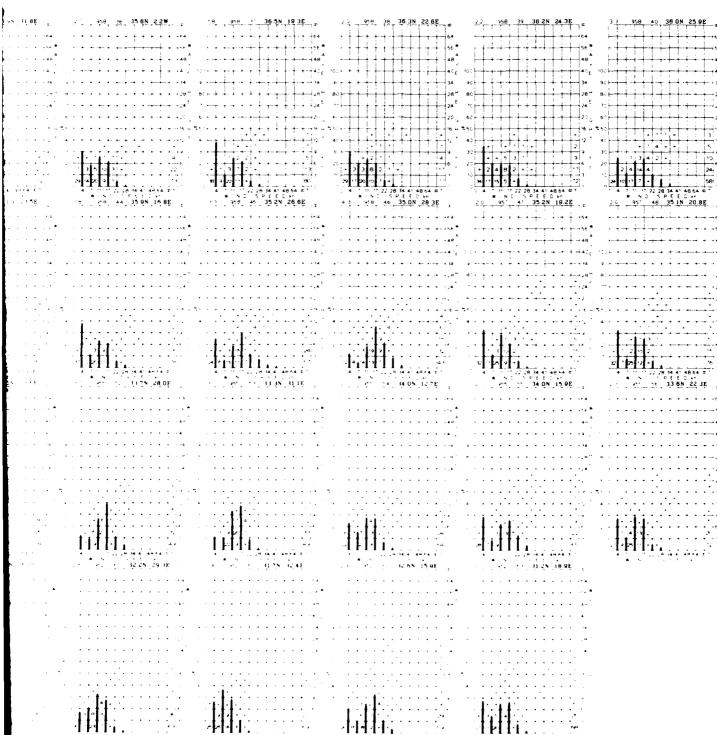
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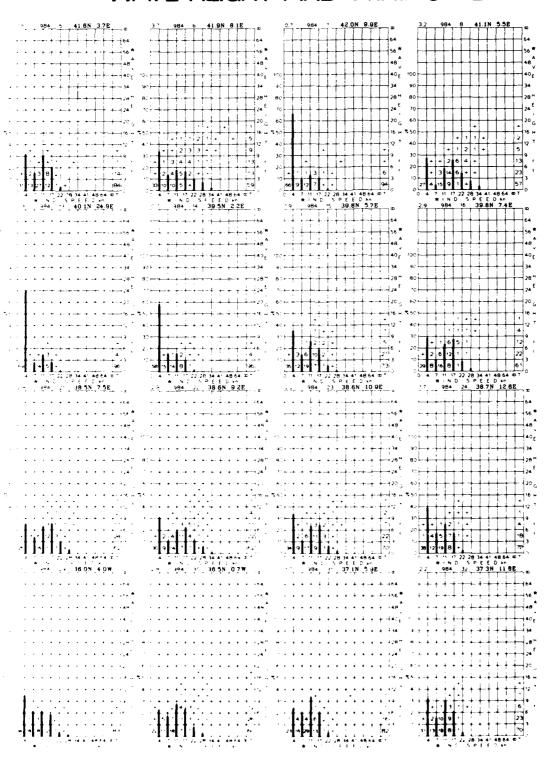
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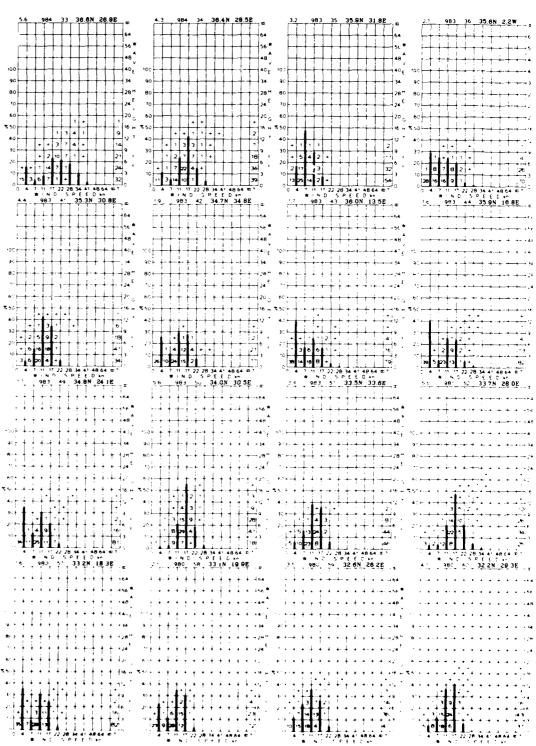
SPEED (Cont'd)

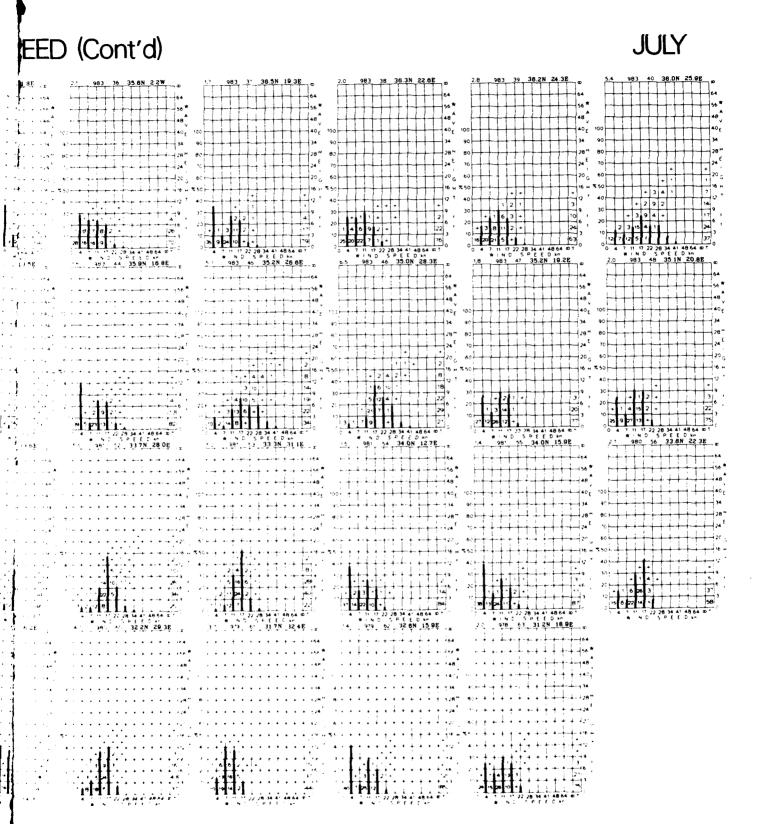
JUNE



WAVE HEIGHT AND WIND SPEED

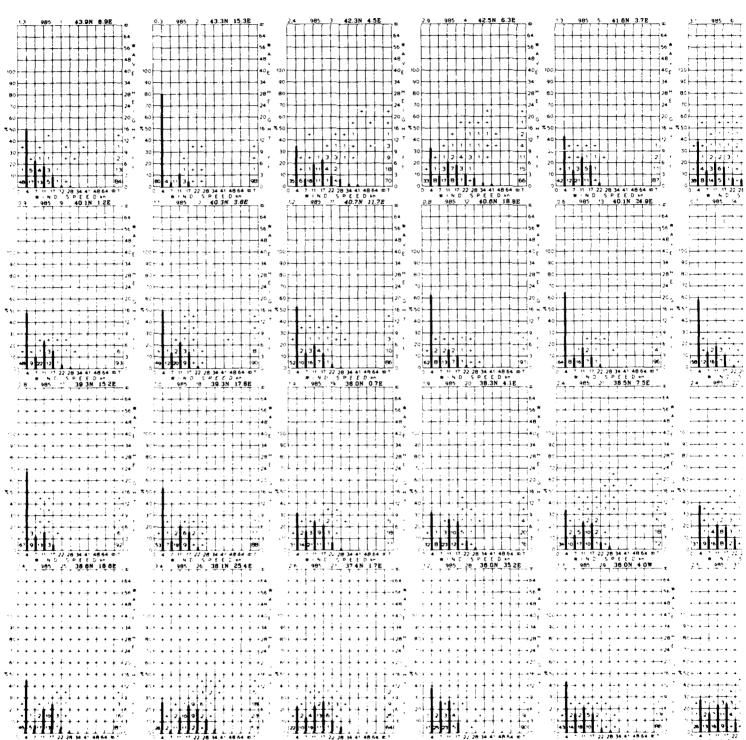




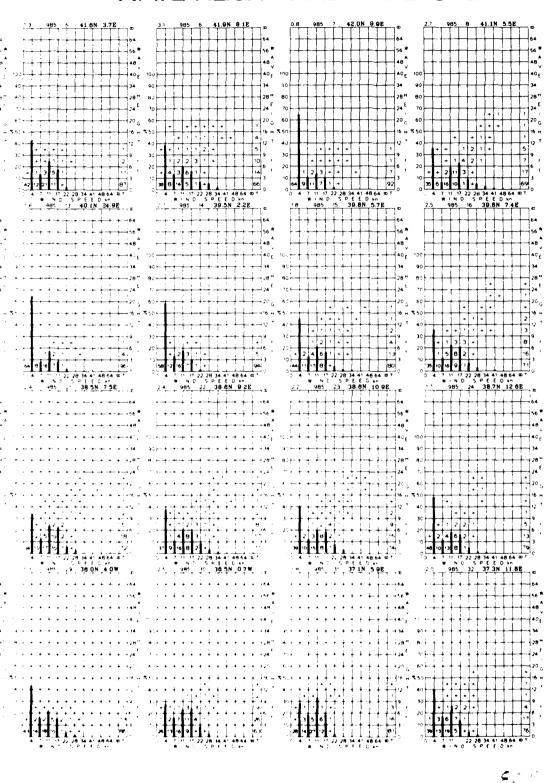


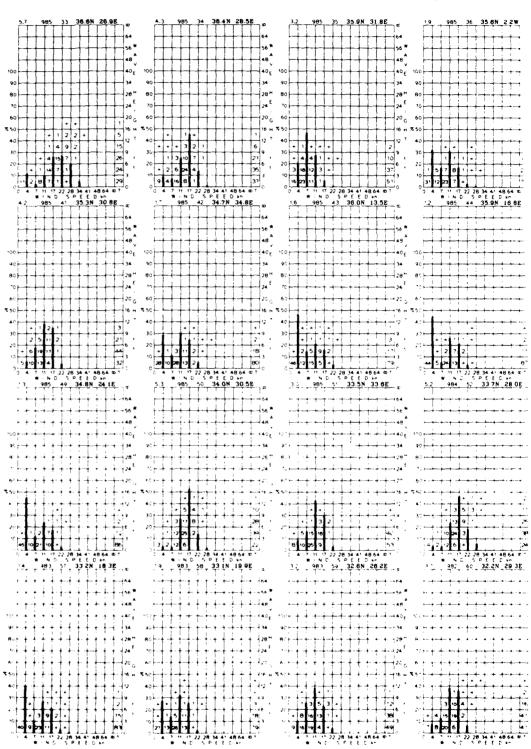
AUGUST

WAVE H



WAVE HEIGHT AND WIND SPEED

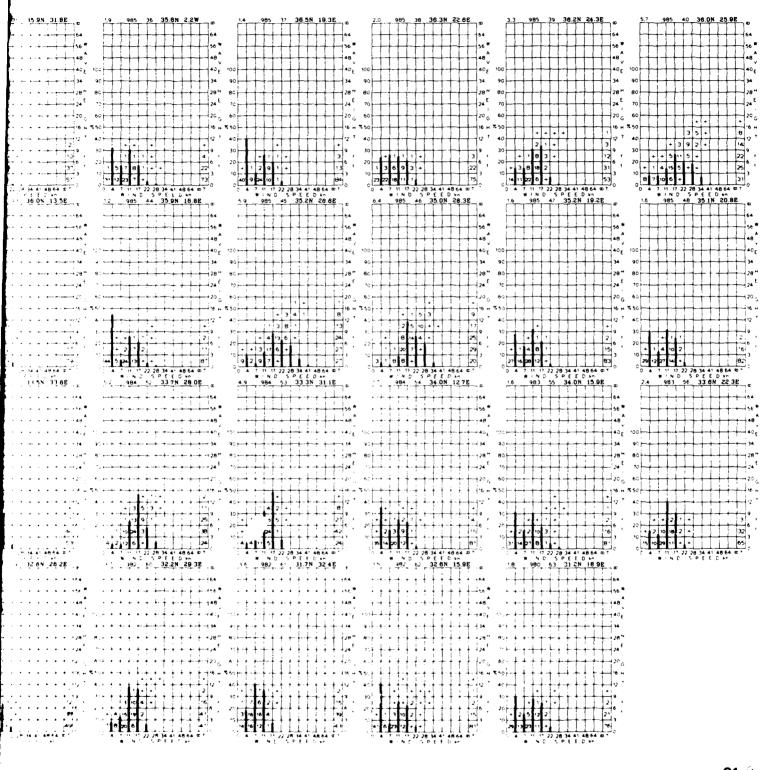




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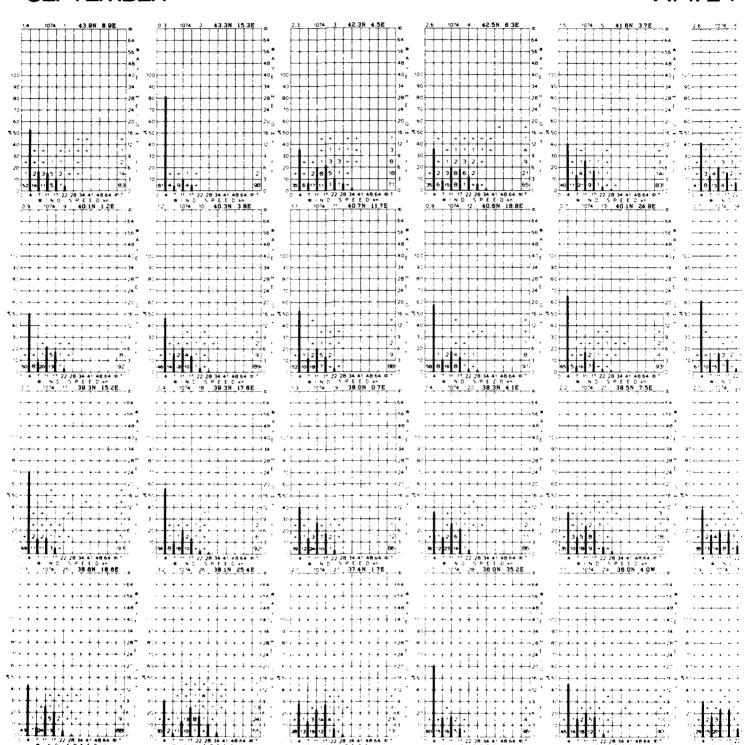
SPEED (Cont'd)

AUGUST

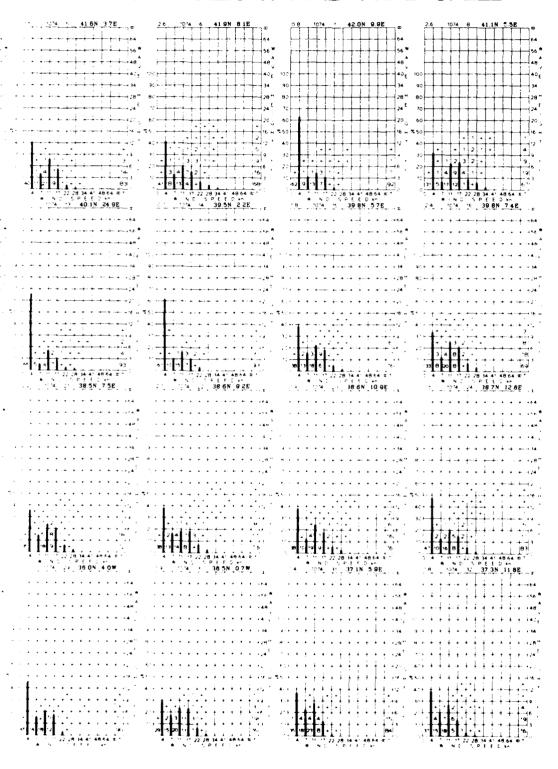


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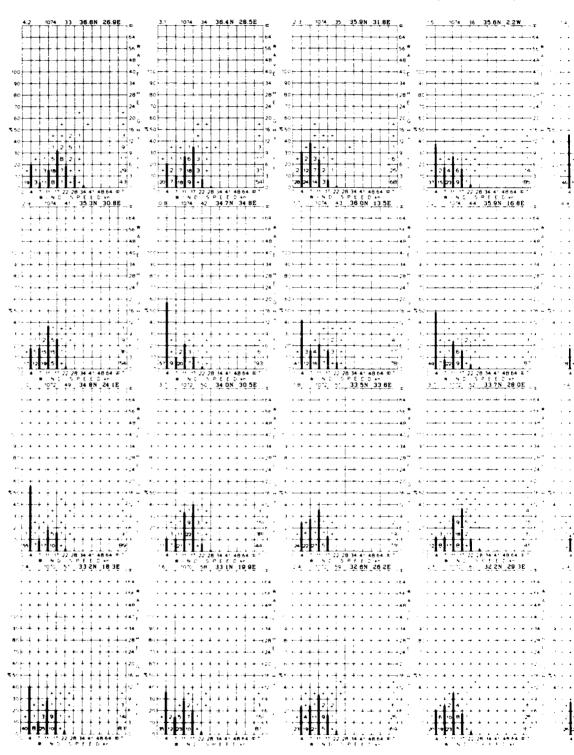
WAVE H



WAVE HEIGHT AND WIND SPEED



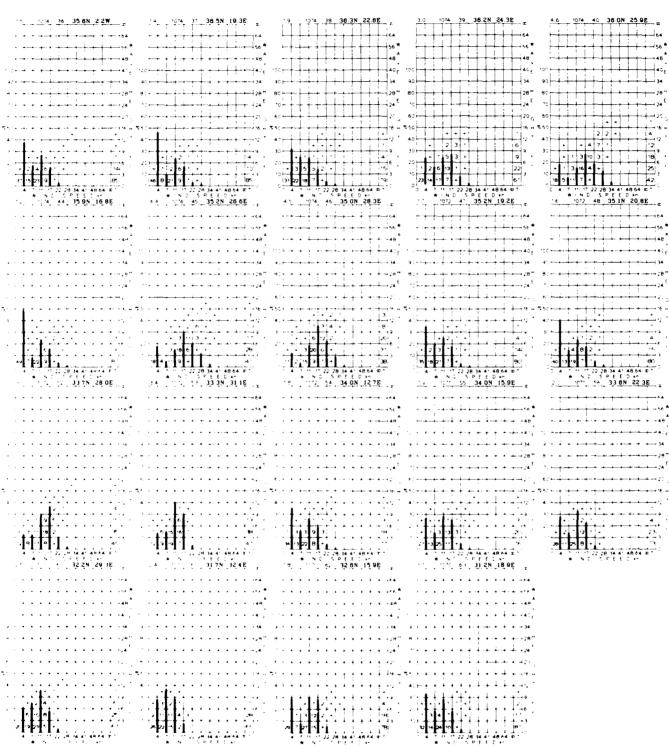
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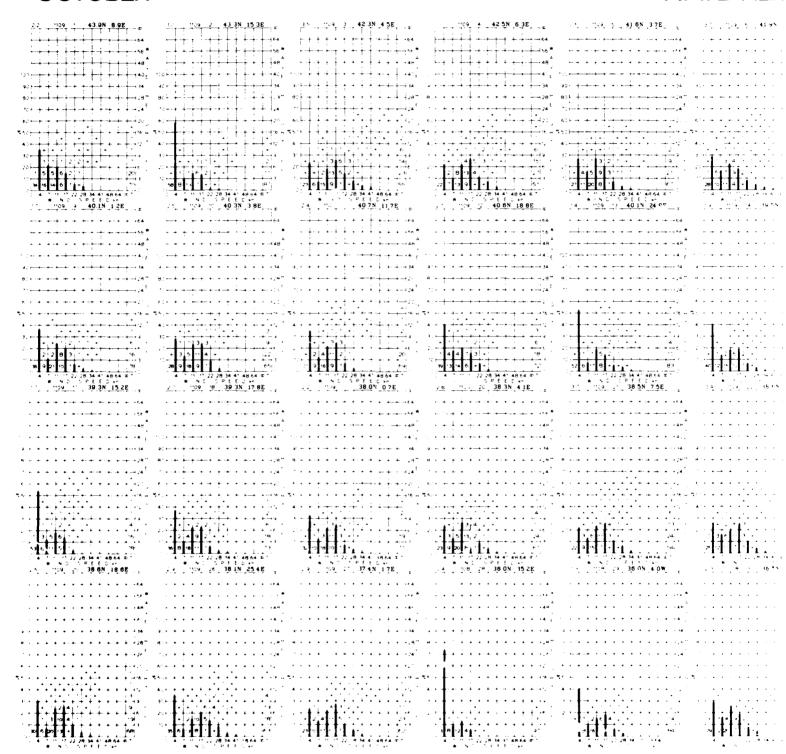
ED (Cont'd)

SEPTEMBER

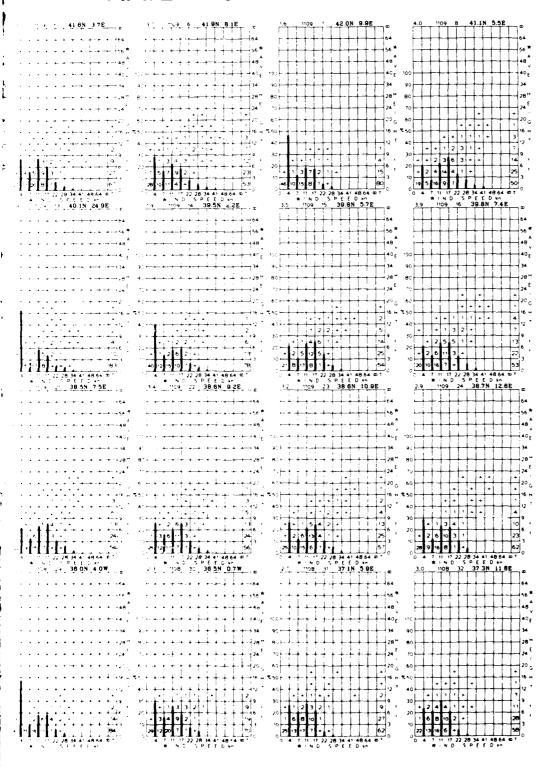


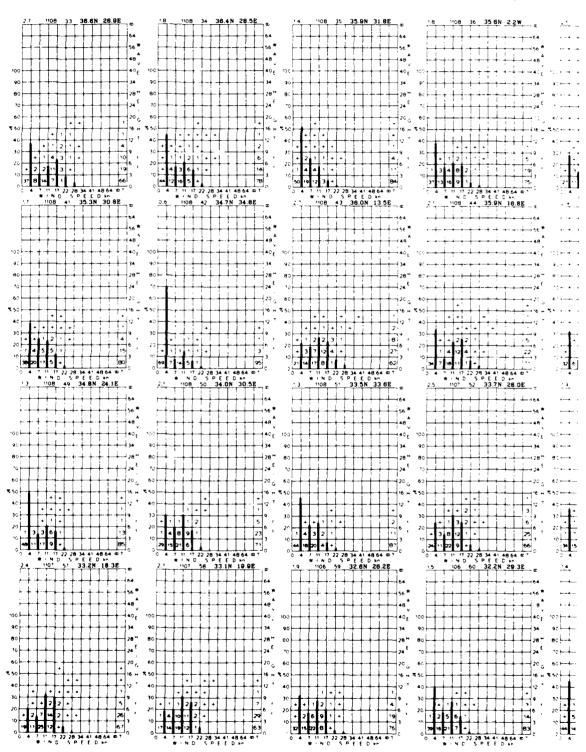
OCTOBER

WAVE HEIC



WAVE HEIGHT AND WIND SPEED

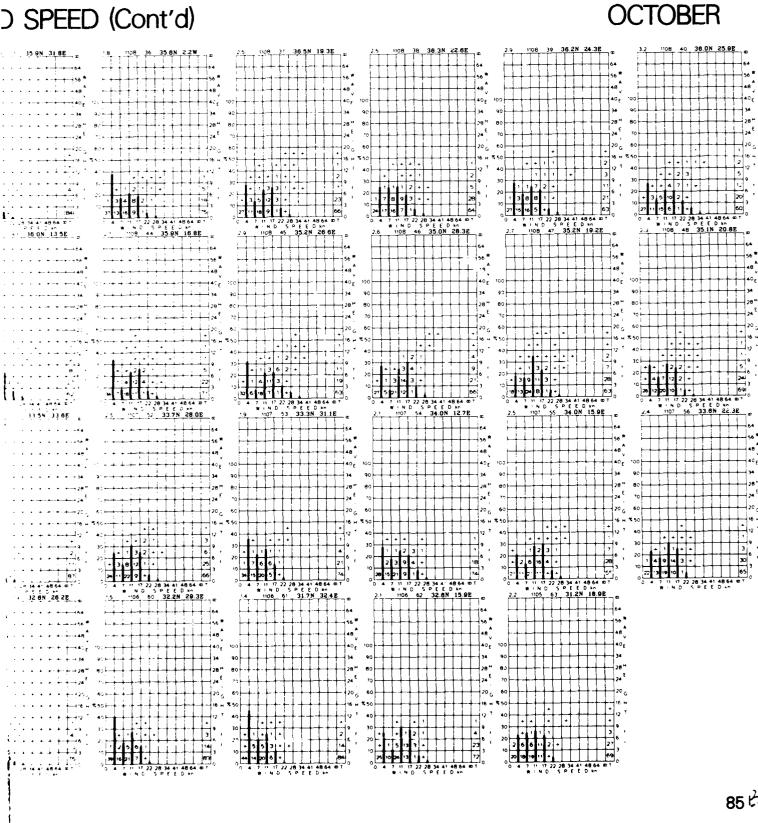






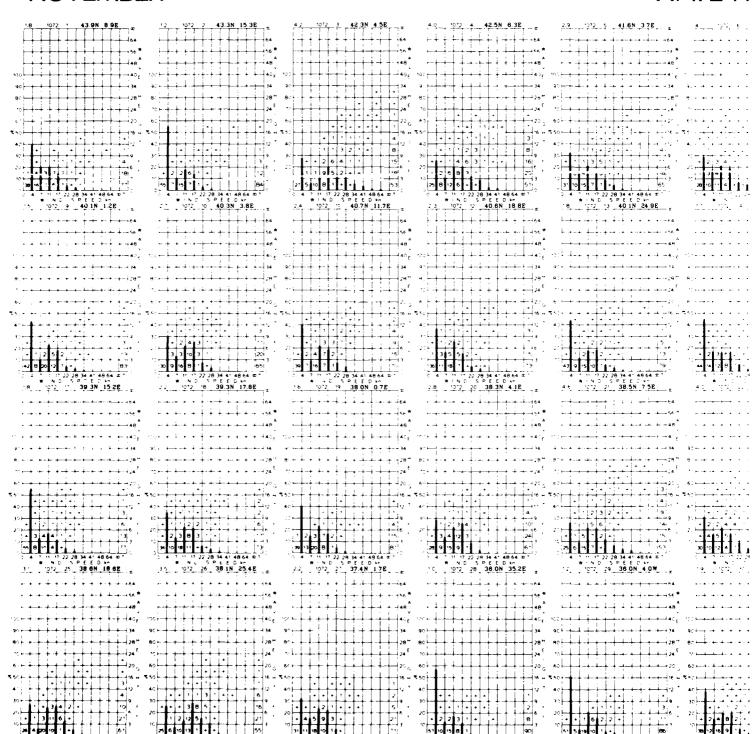
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OCTOBER

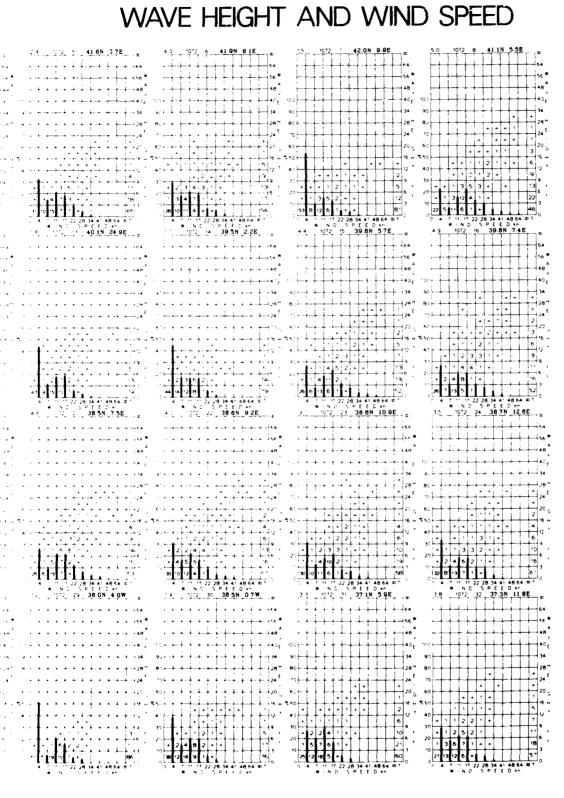


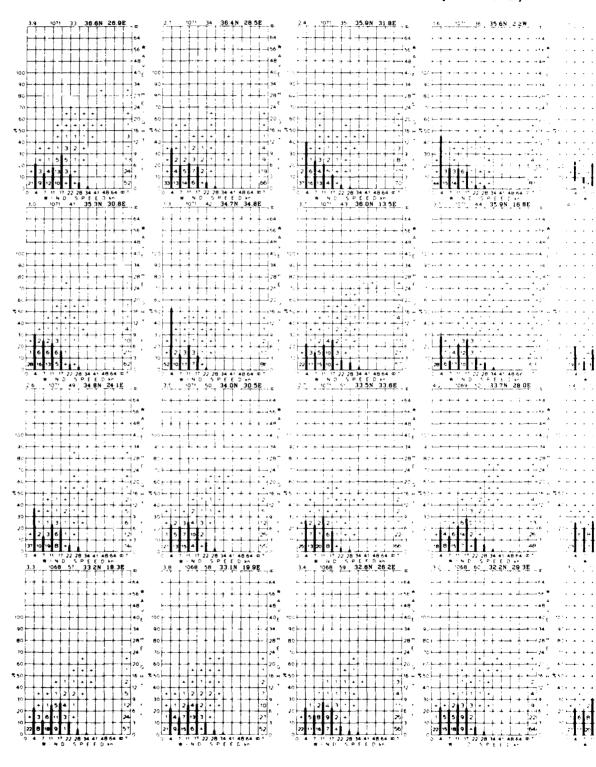
NOVEMBER

WAVE H



WAVE HEIGHT AND WIND SPEED

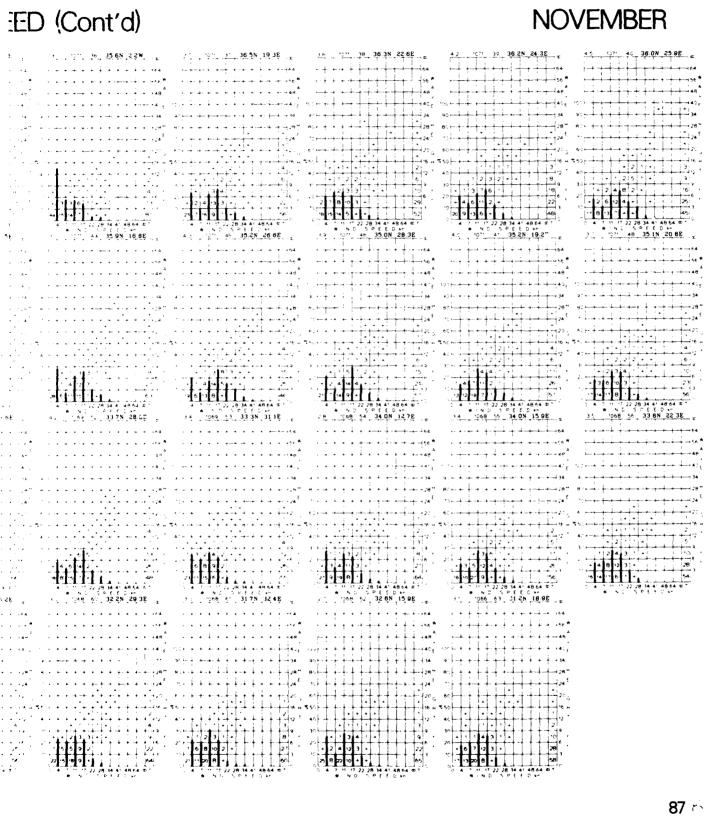




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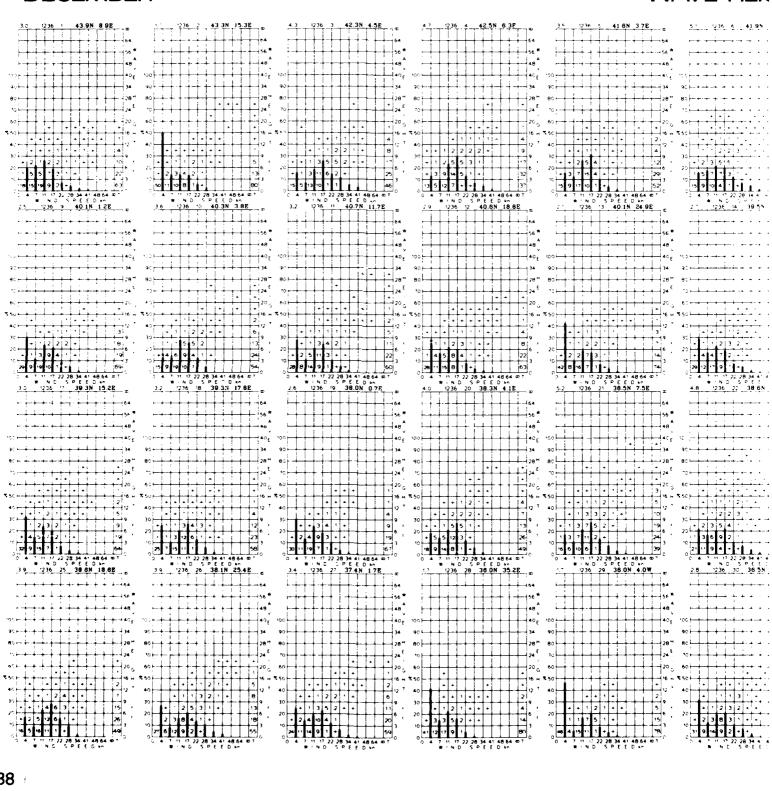
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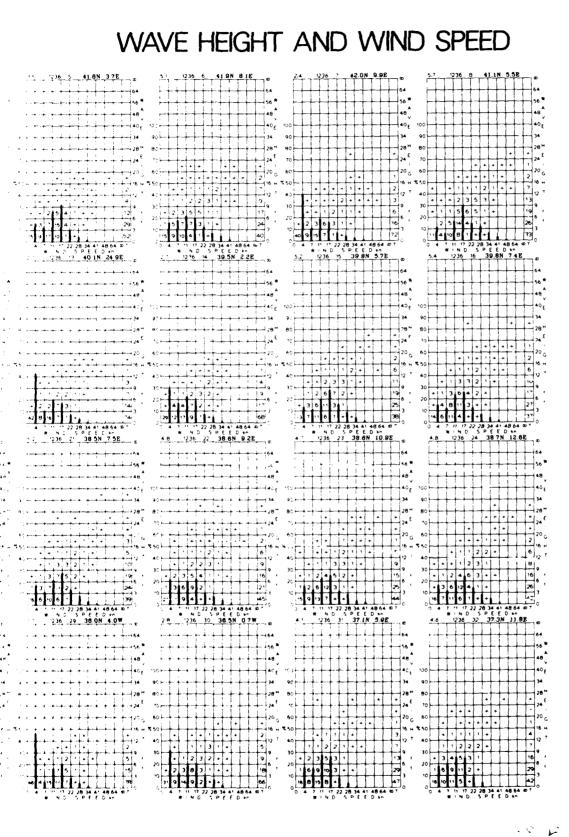
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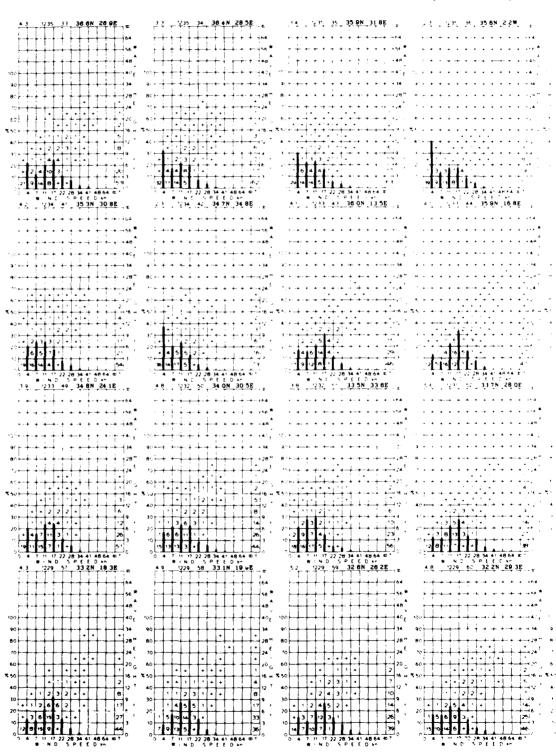


DECEMBER

WAVE HEI

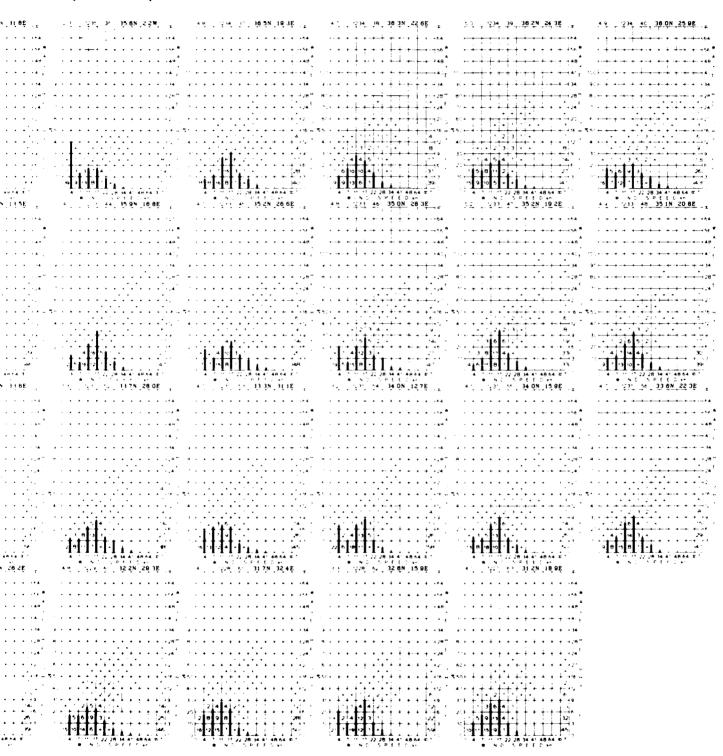






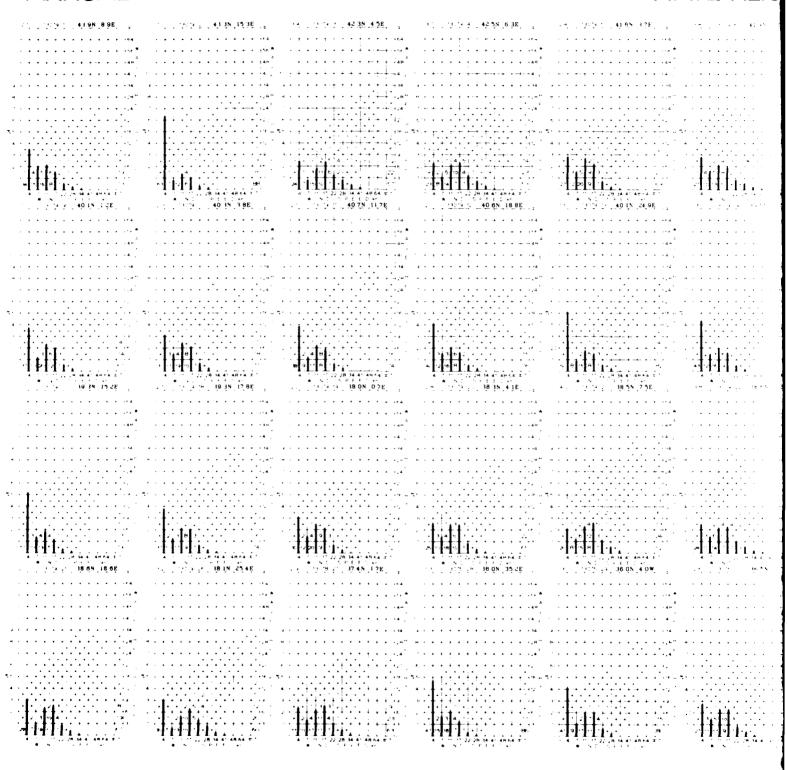
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DECEMBER

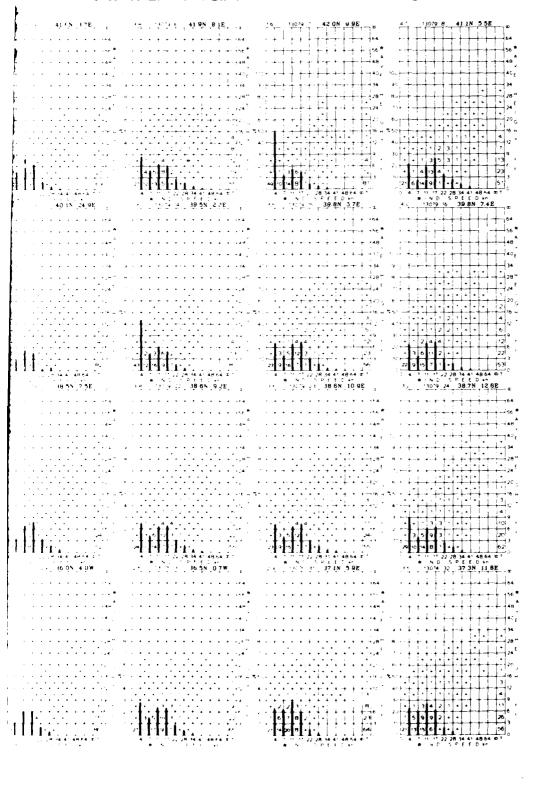


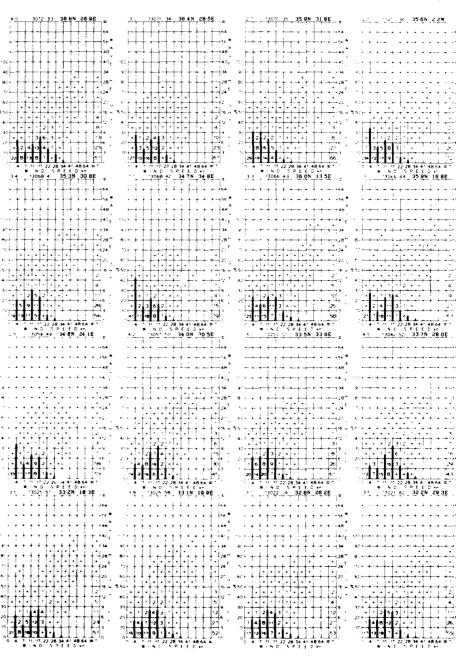
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WAVE HEIG



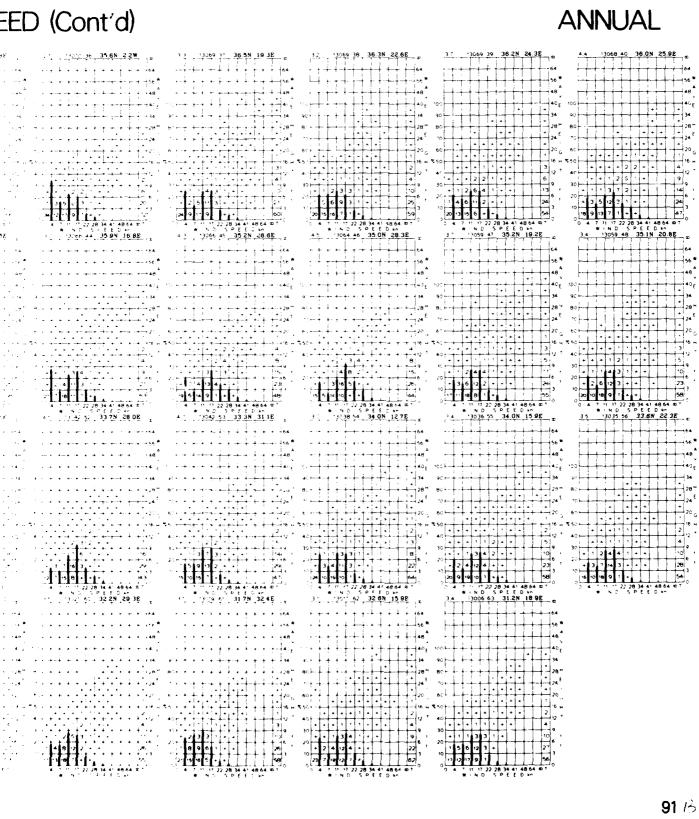
WAVE HEIGHT AND WIND SPEED





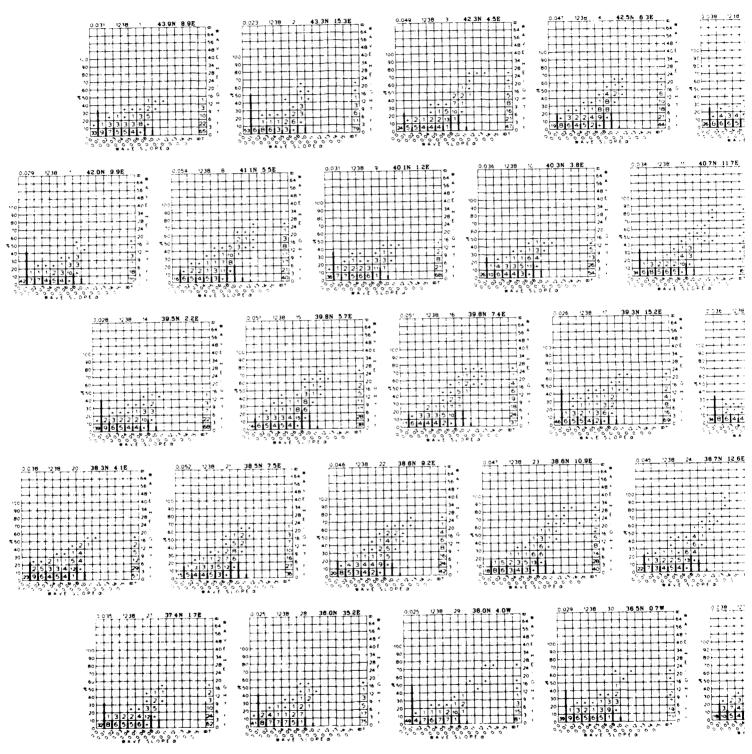
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ANNUAL

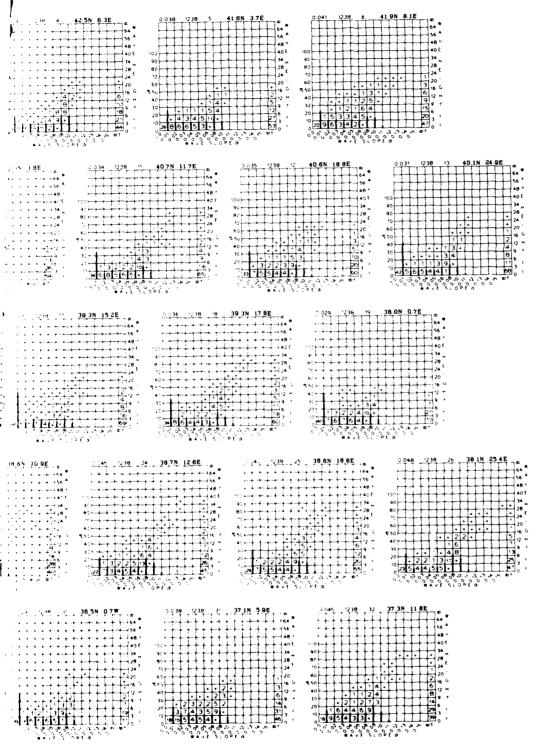


JANUARY

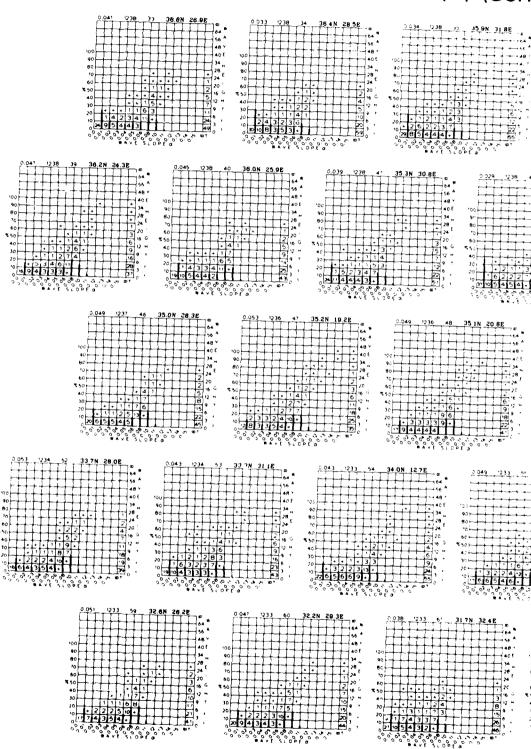
WAVE HEK



WAVE HEIGHT AND WAVE SLOPE (α)



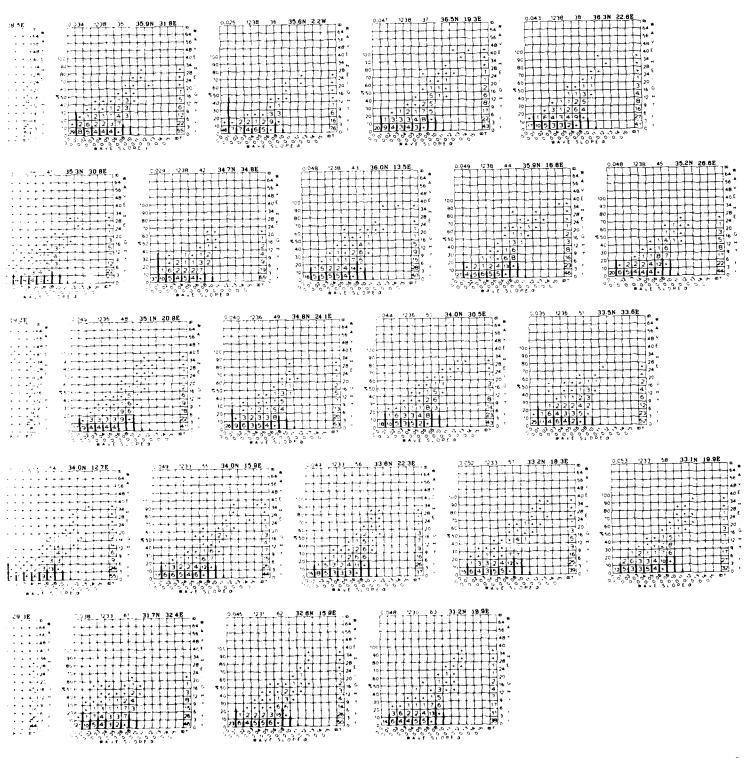
WAVE HEIGHT AND WAVE SLOPE (α) (Cont'



93 A

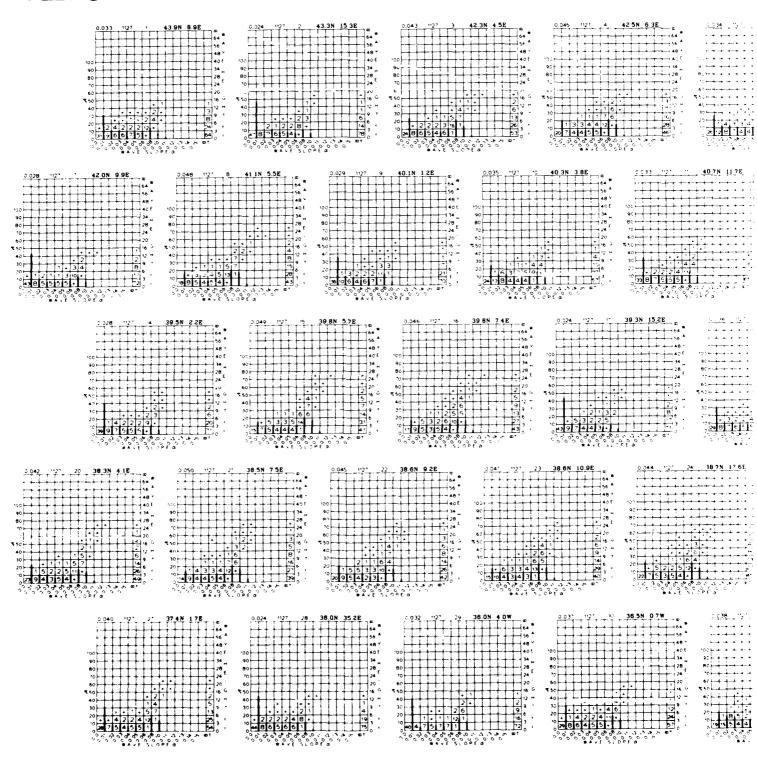
SLOPE (α) (Cont'd)

JANUARY

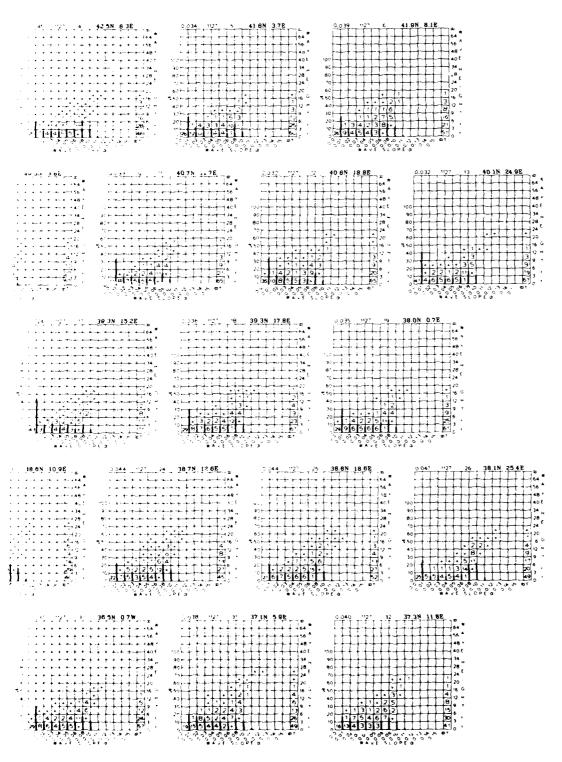


FEBRUARY

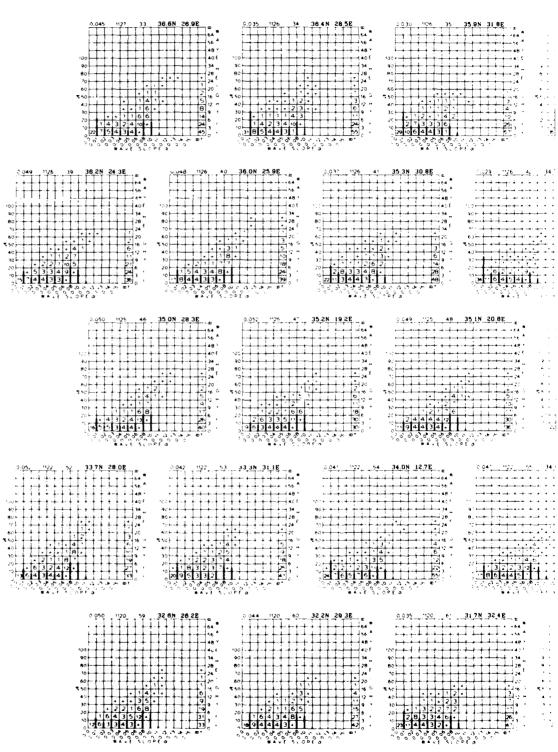
WAVE HEIC



WAVE HEIGHT AND WAVE SLOPE (α)

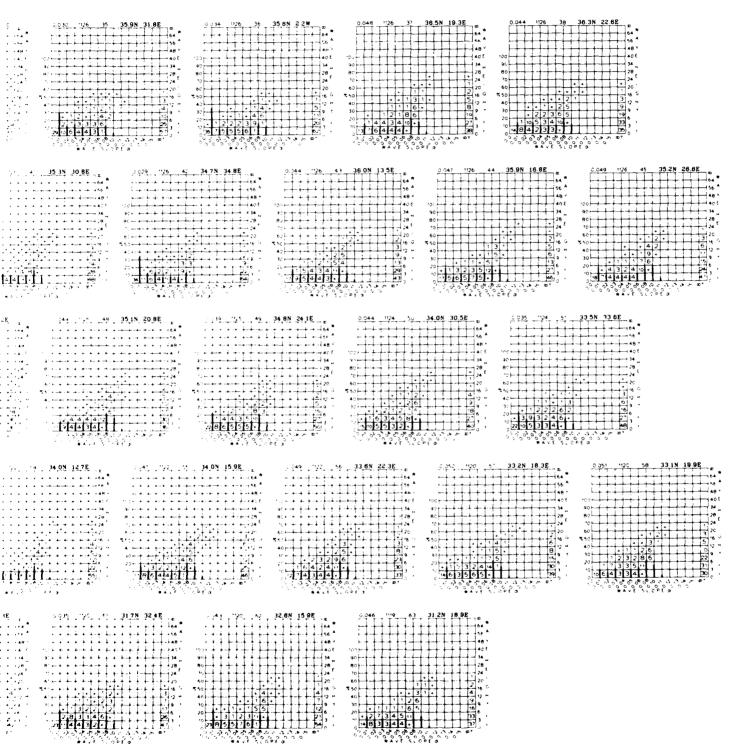


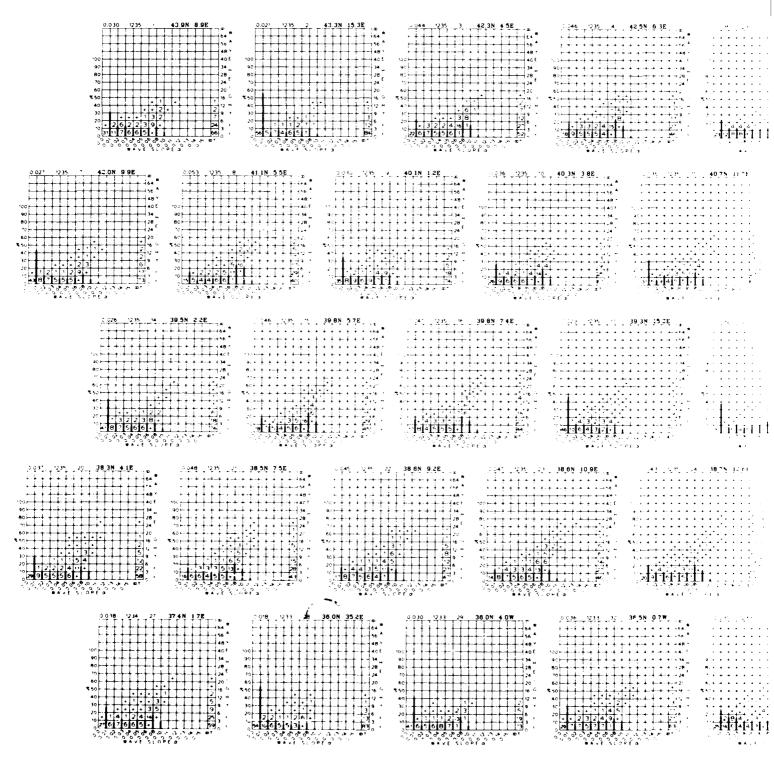
WAVE HEIGHT AND WAVE SLOPE (α) (Cont'd)

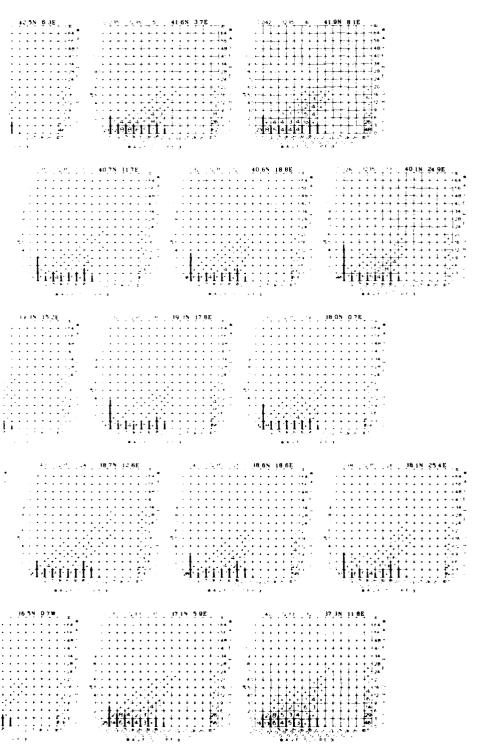


SLOPE (a) (Cont'd)

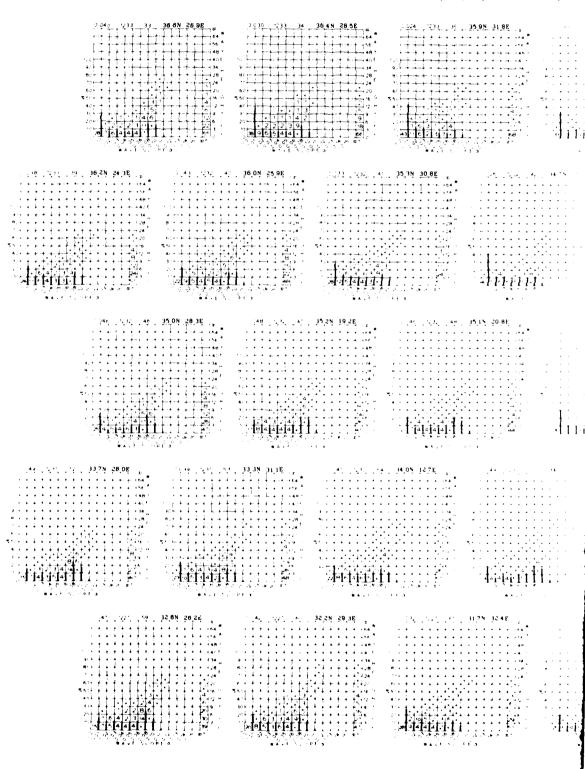
FEBRUARY





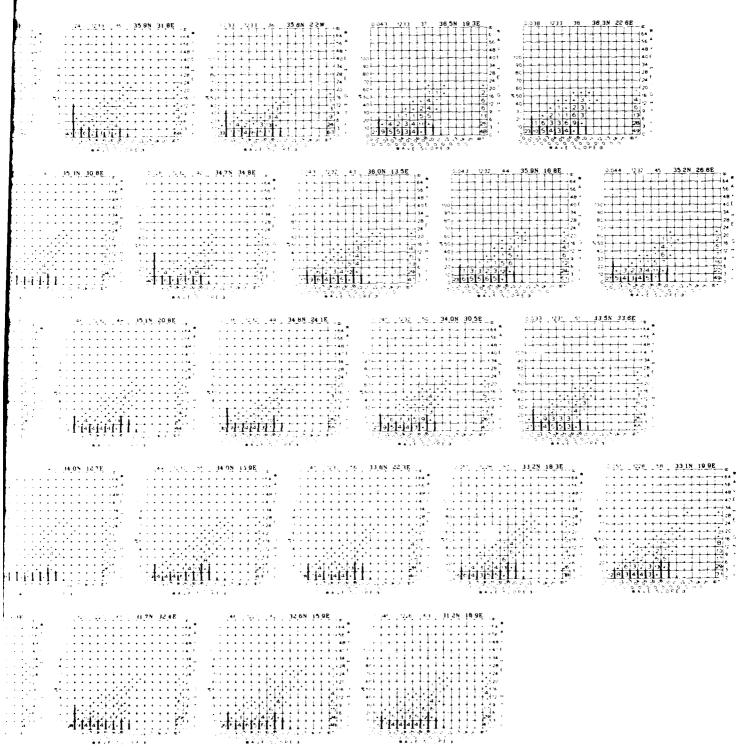


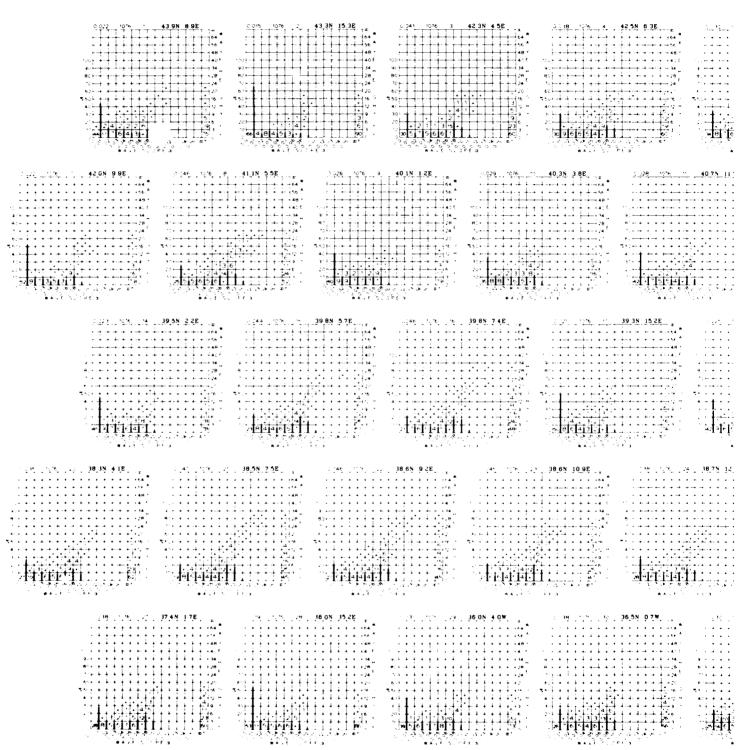
WAVE HEIGHT AND WAVE SLOPE (a) (Cont'd)

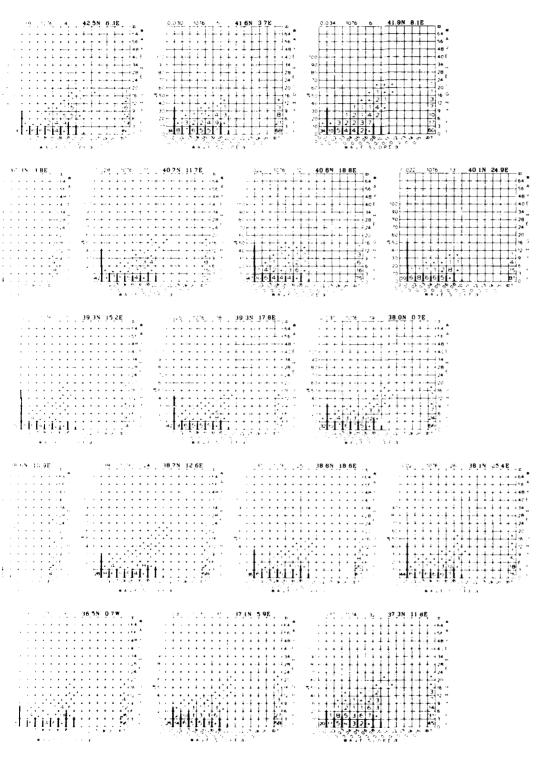


SLOPE (a) (Cont'd)

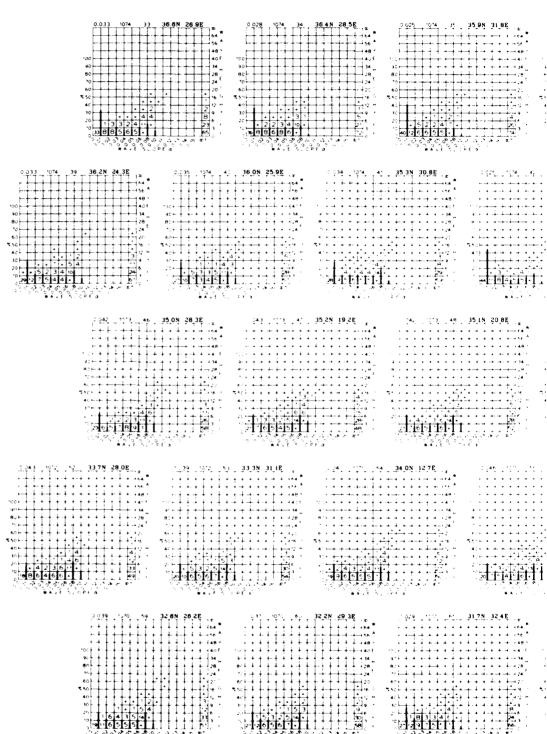
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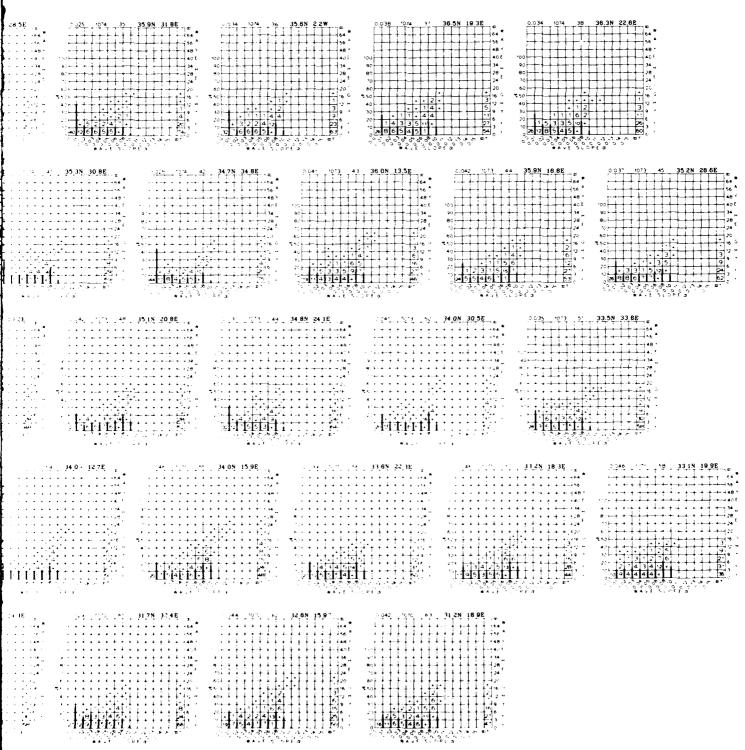
WAVE HEIGHT AND WAVE SLOPE (a) (Cont'o



79 A

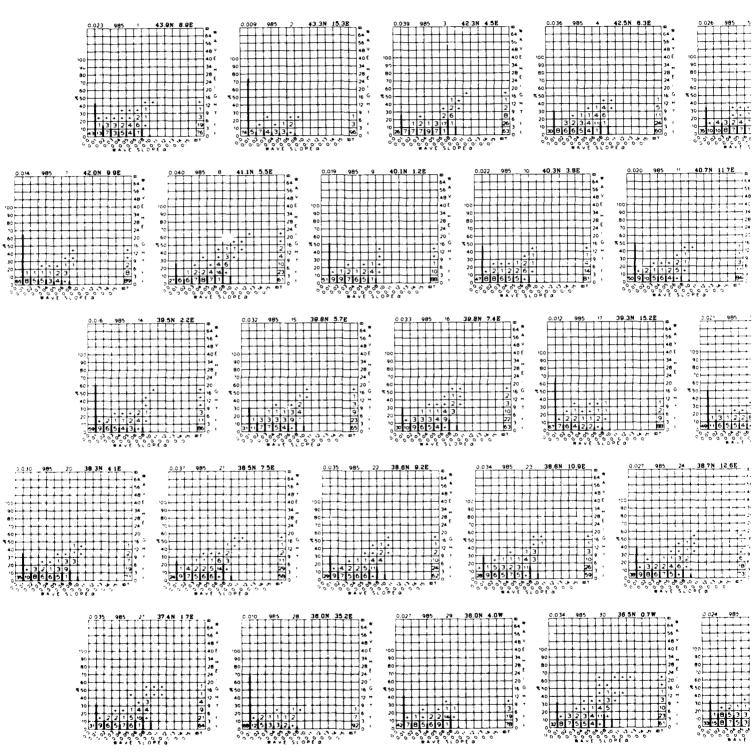
SLOPE (α) (Cont'd)

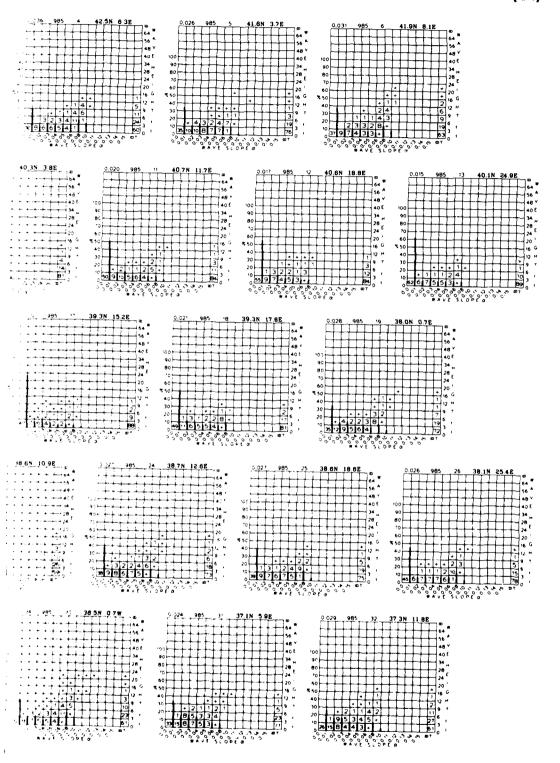
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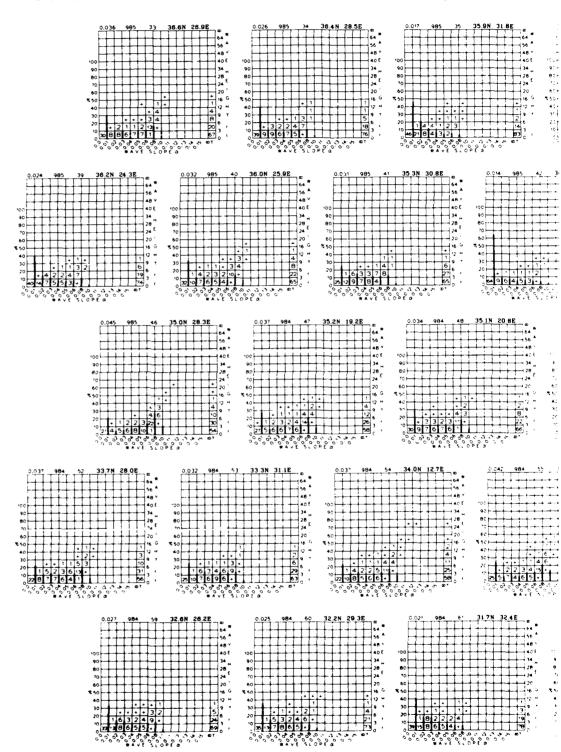
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WAVE HEIG



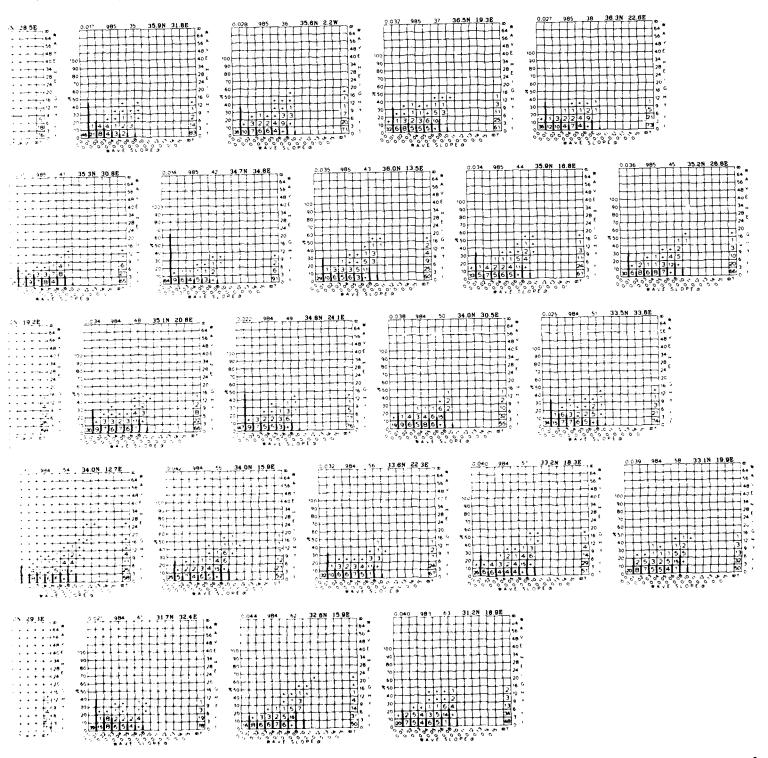


WAVE HEIGHT AND WAVE SLOPE (α) (Cont'd

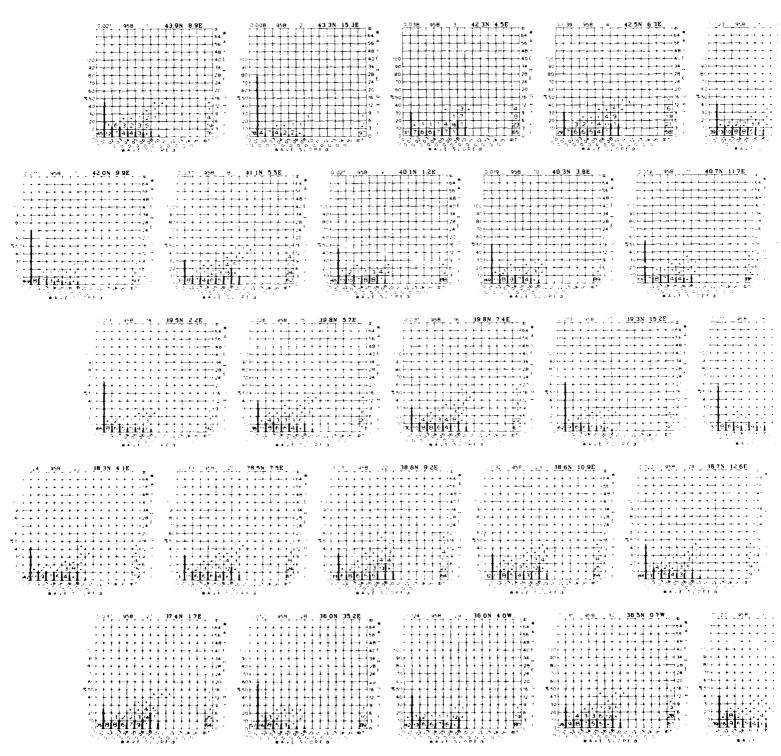


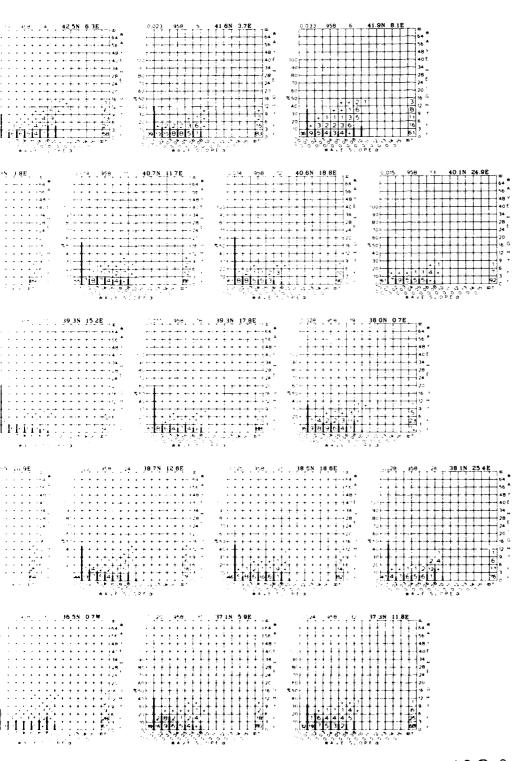
E SLOPE (α) (Cont'd)

MAY

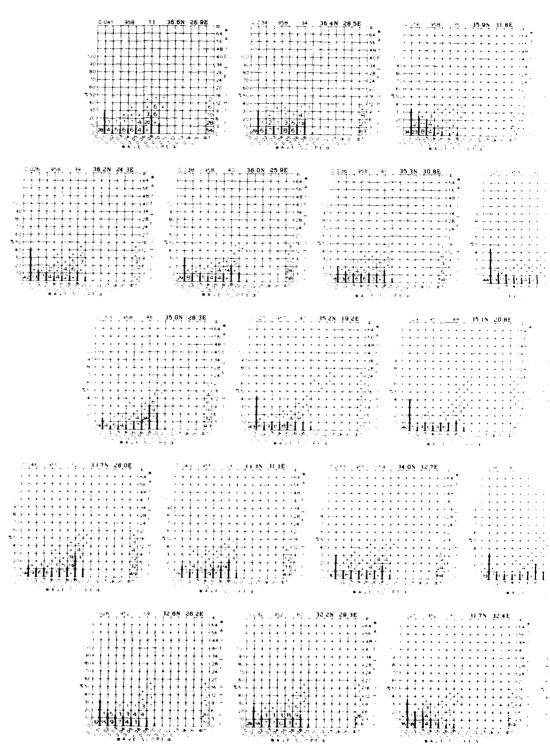


WAVE HEIGH



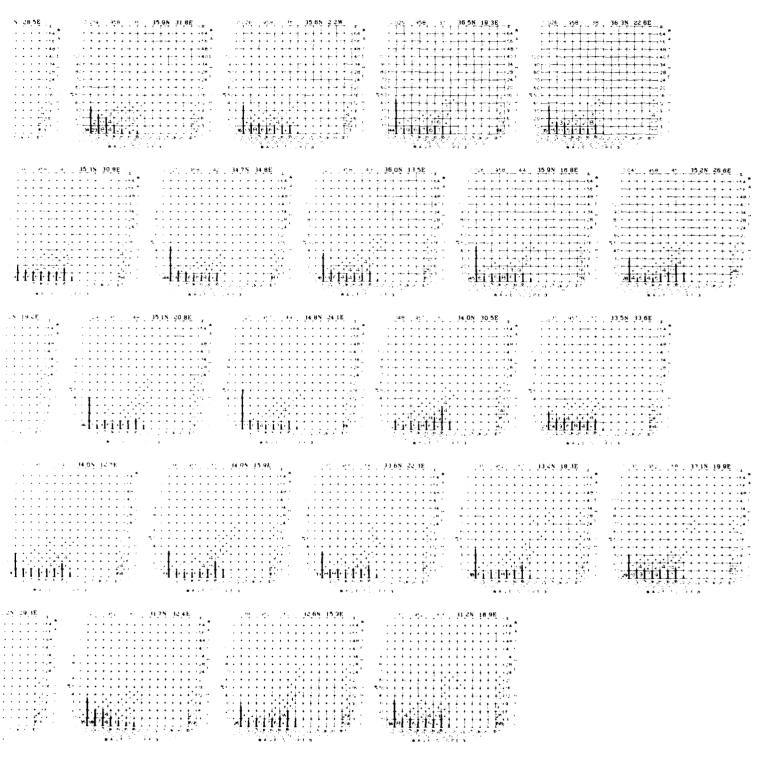


WAVE HEIGHT AND WAVE SLOPE (a) (Cont'

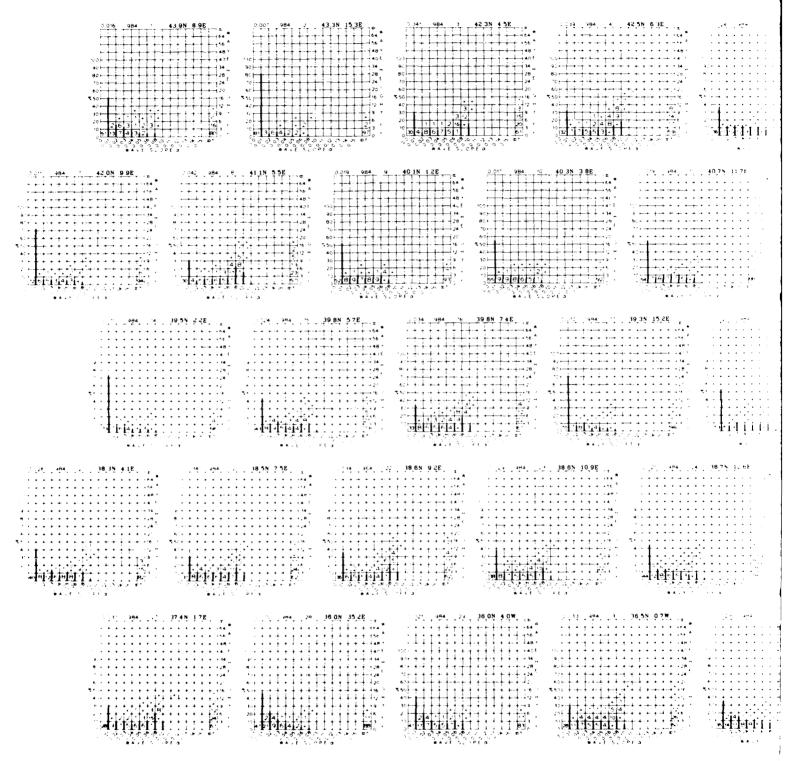


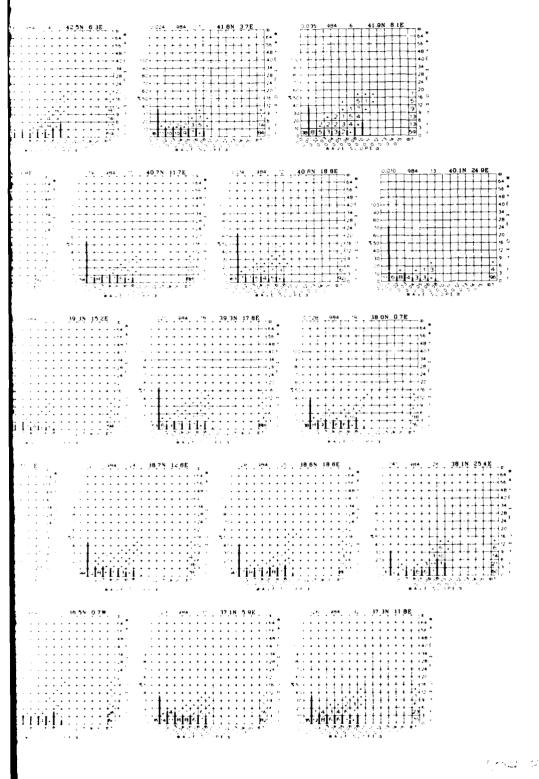
E SLOPE (a) (Cont'd)

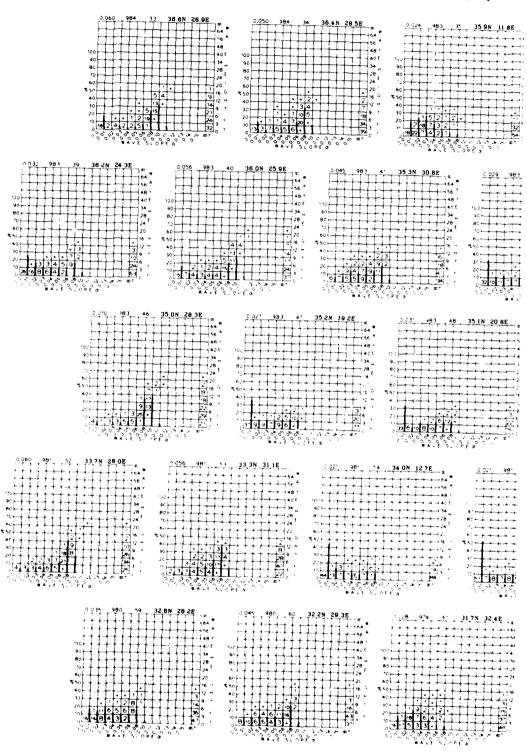
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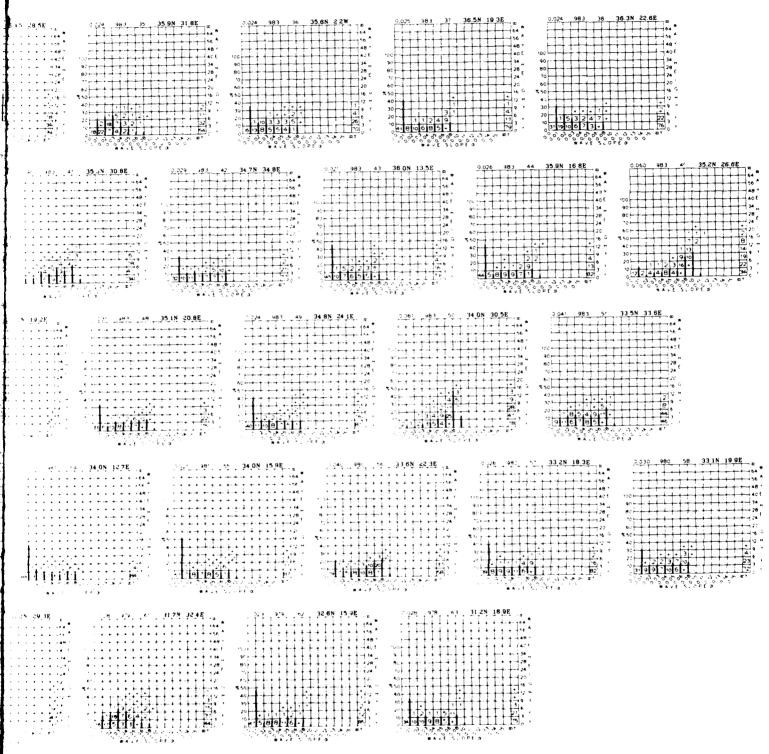


WAVE HEIGH



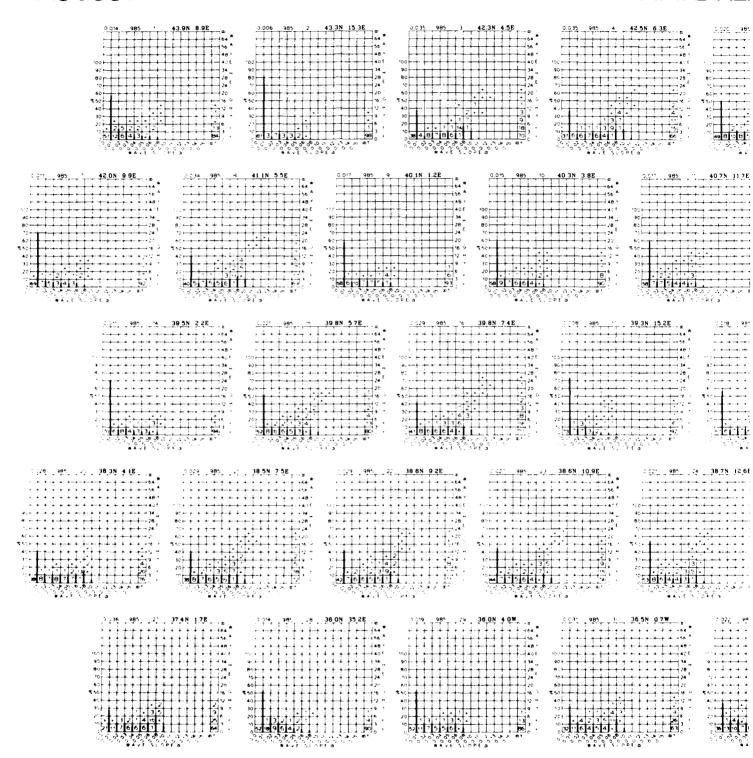


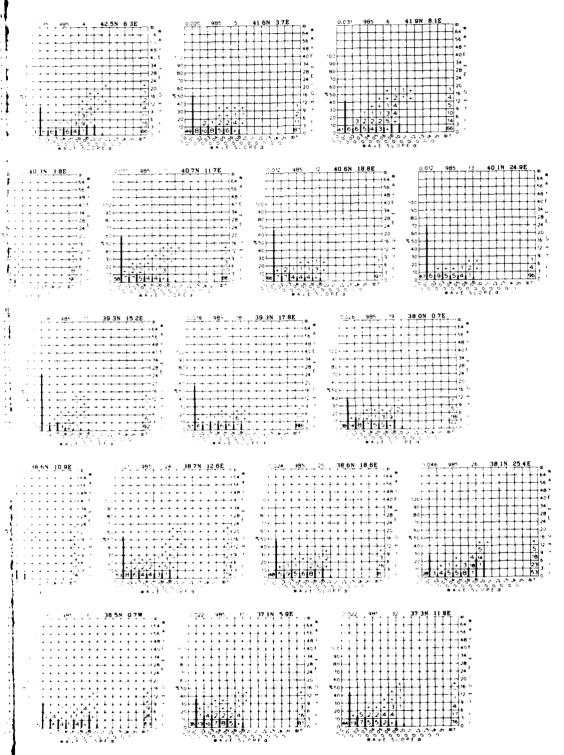




AUGUST

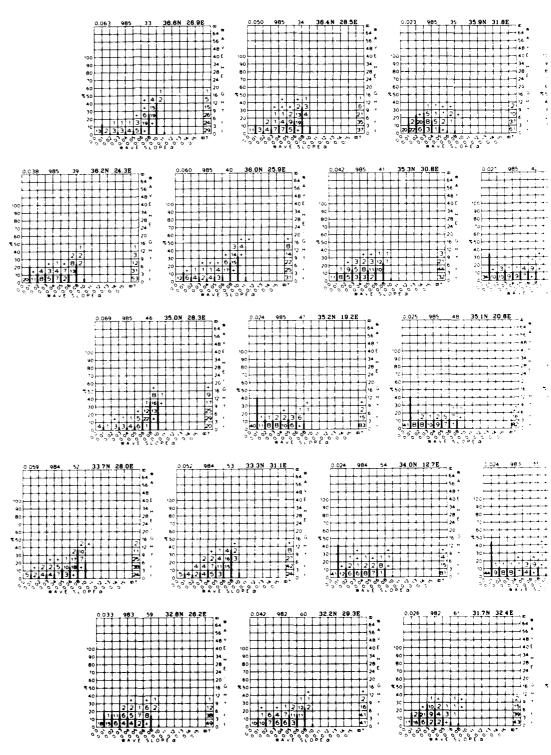
WAVE HEI





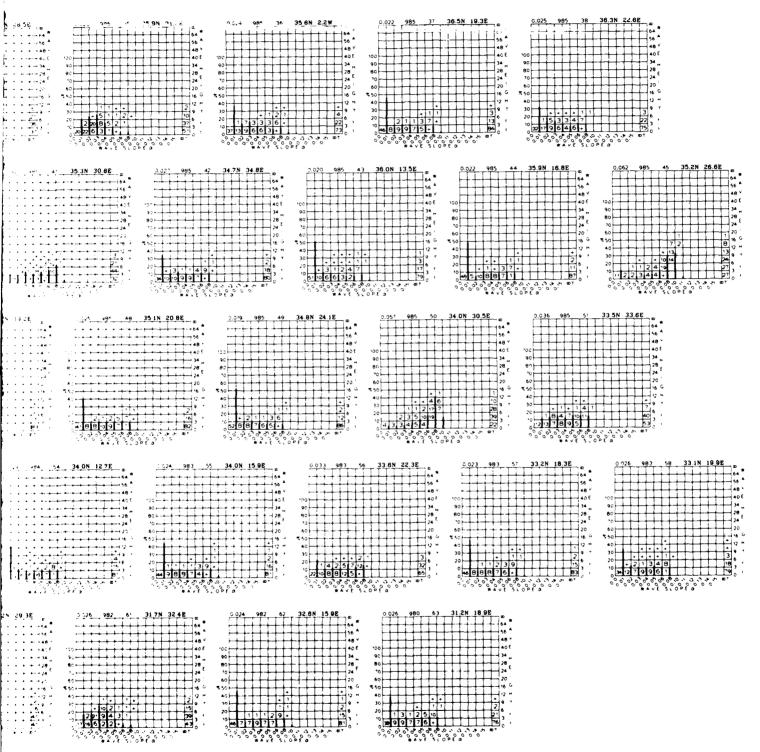
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WAVE HEIGHT AND WAVE SLOPE (α) (Cont'c



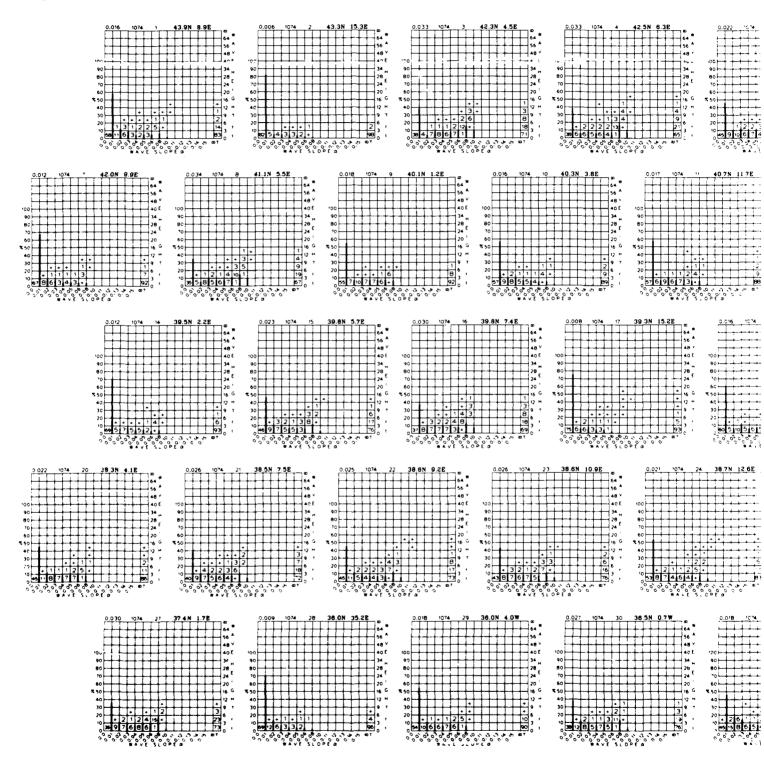
E SLOPE (α) (Cont'd)

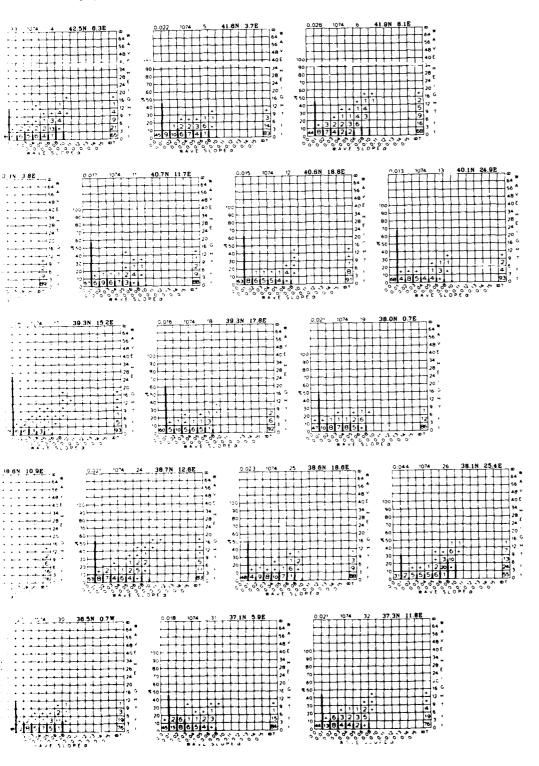
AUGUST



SEPTEMBER

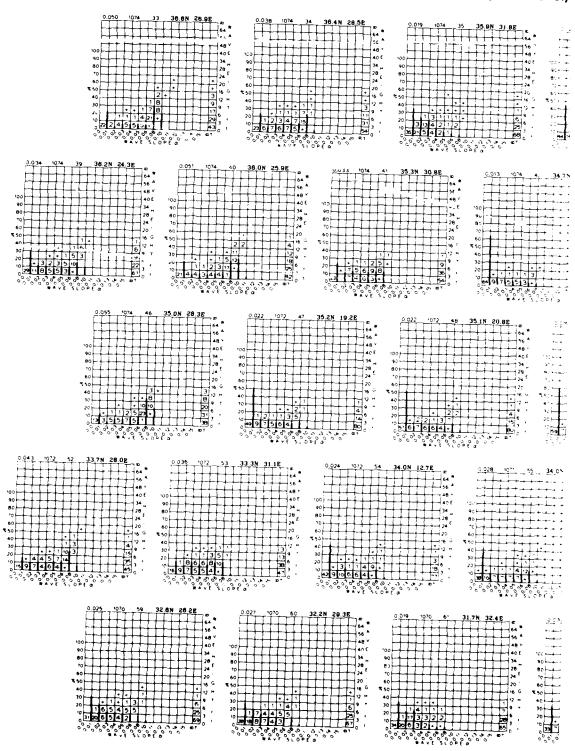
WAVE HEK





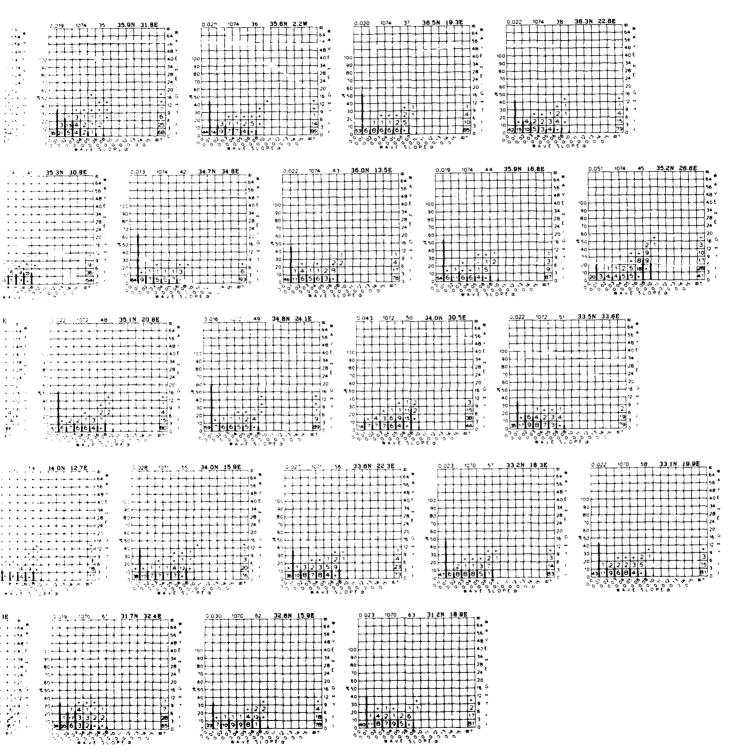
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WAVE HEIGHT AND WAVE SLOPE (α) (Cont'd)



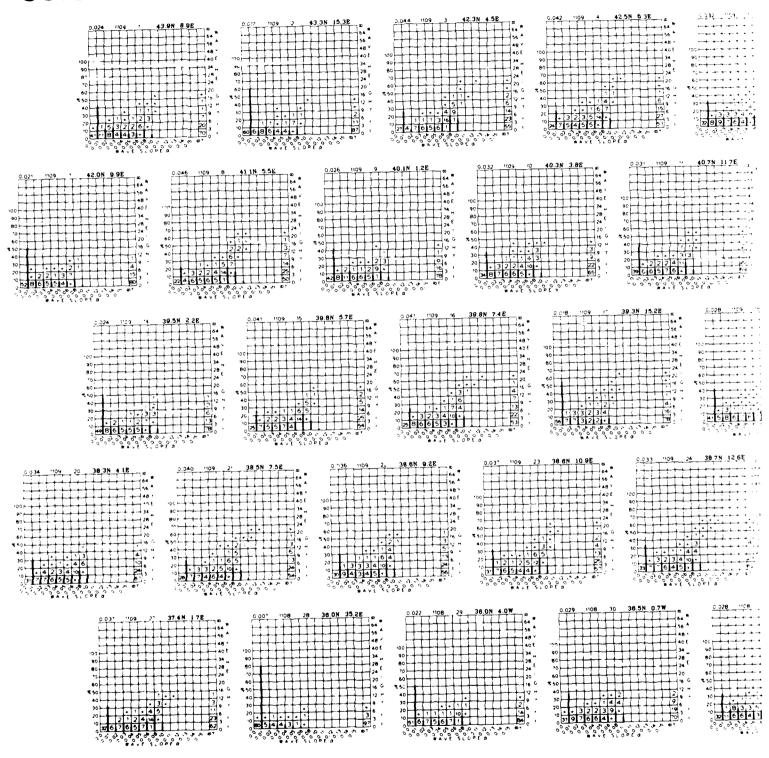
SLOPE (α) (Cont'd)

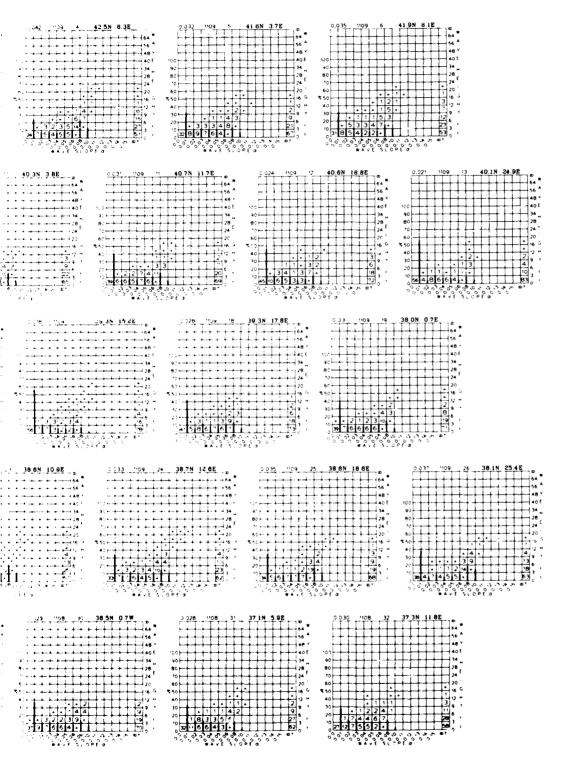
SEPTEMBER



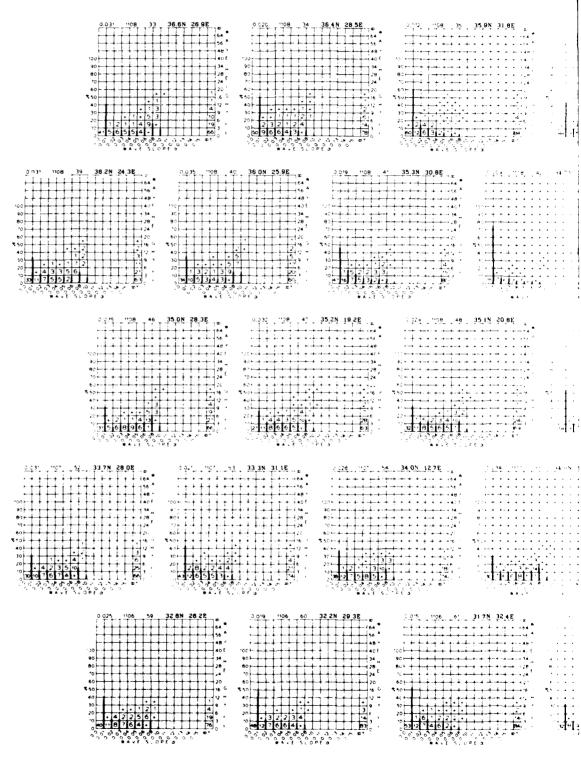
OCTOBER

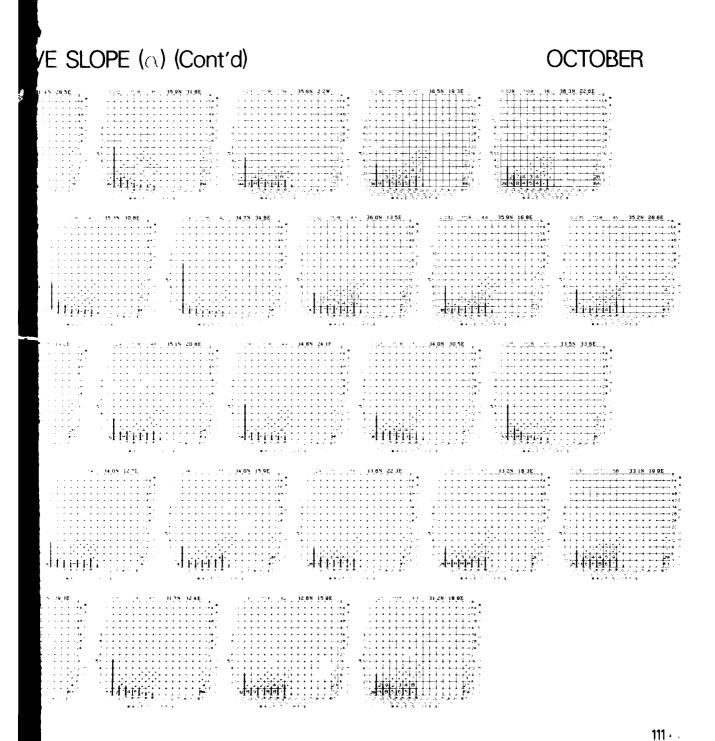
WAVE HEIG





WAVE HEIGHT AND WAVE SLOPE (a) (Cont'd)



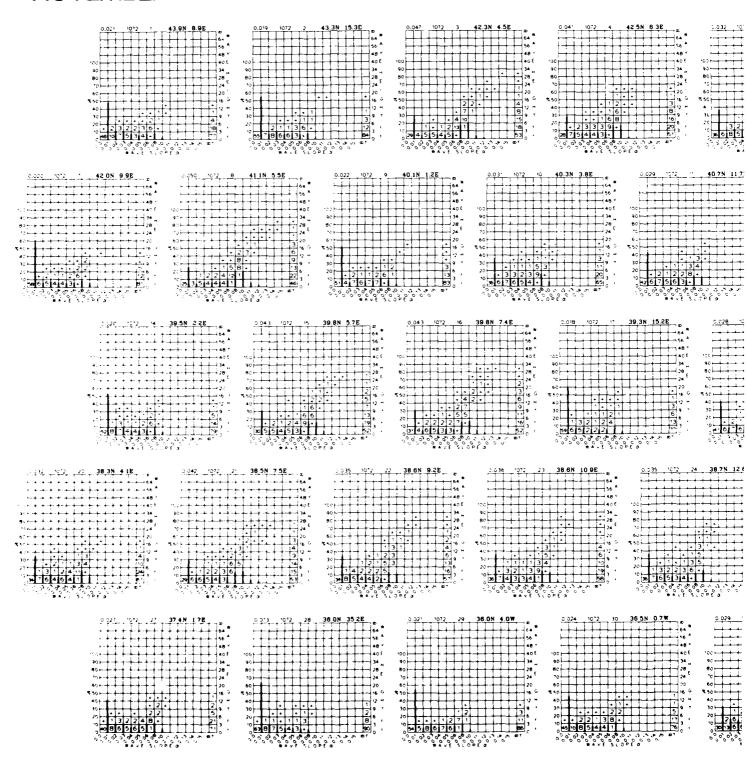


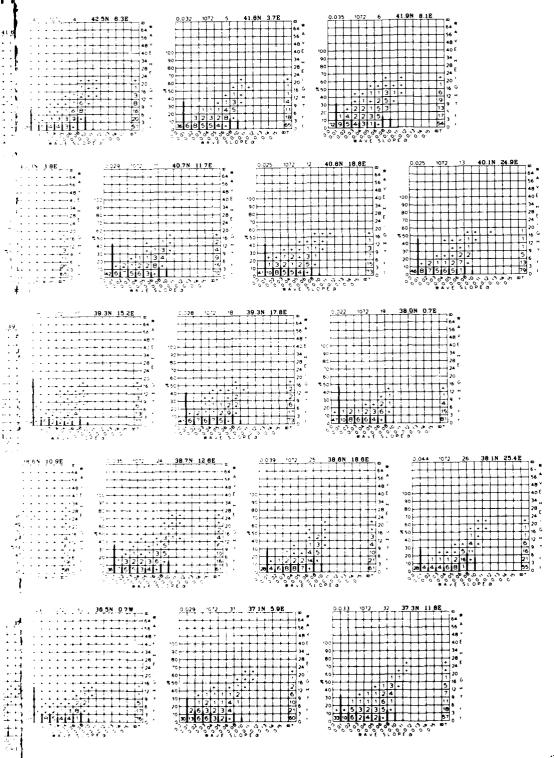
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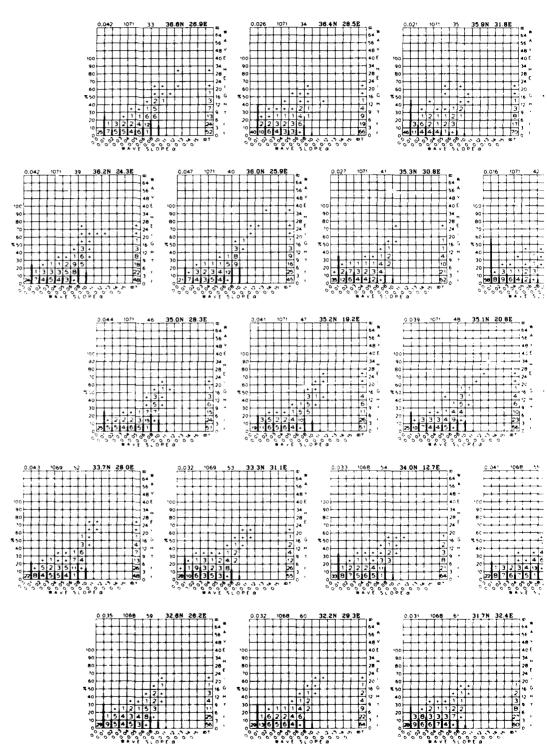
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NOVEMBER

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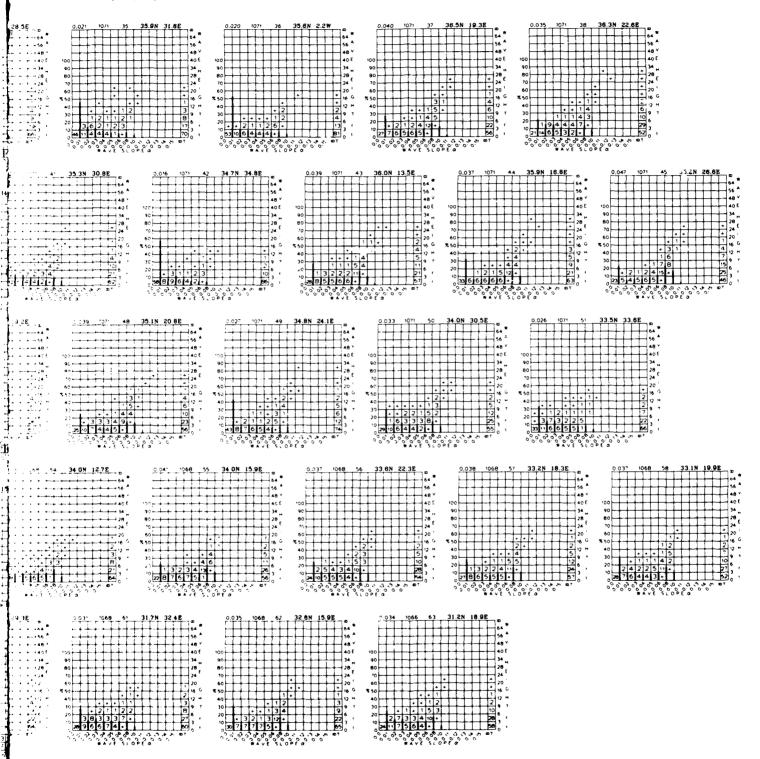






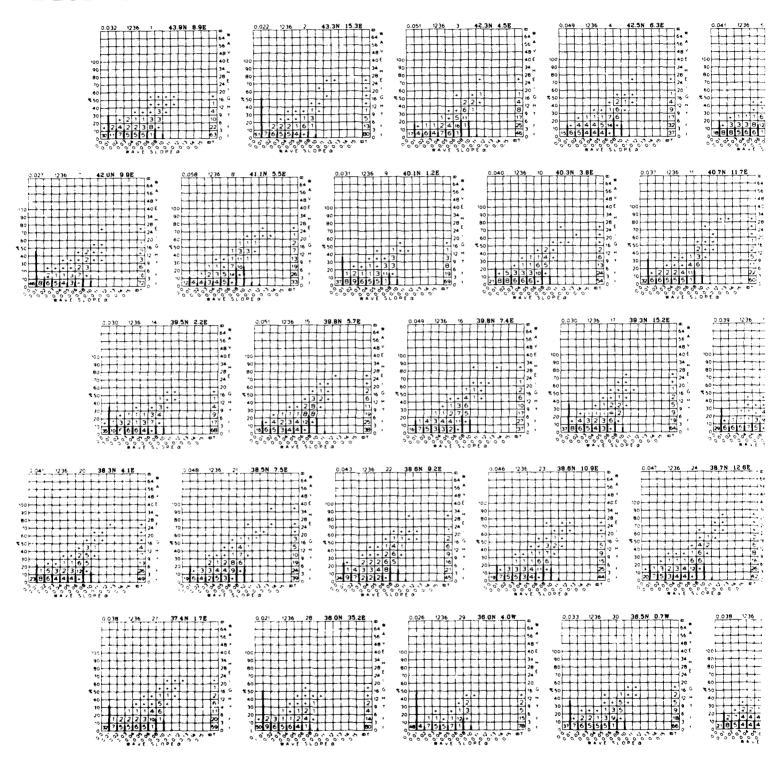
SLOPE (α) (Cont'd)

NOVEMBER

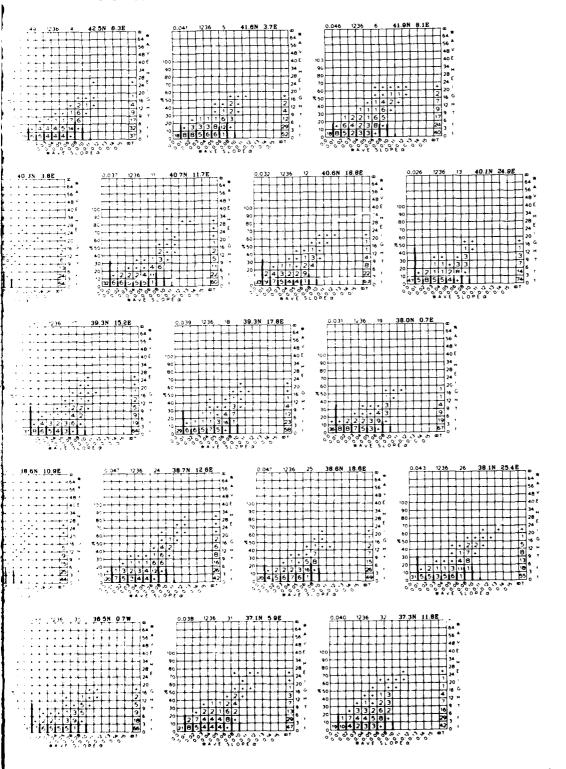


DECEMBER

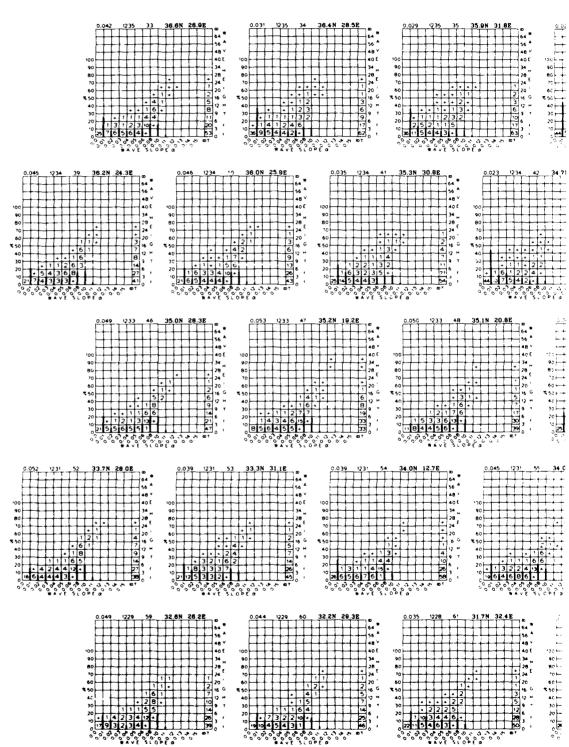
WAVE HEIG



WAVE HEIGHT AND WAVE SLOPE (α)

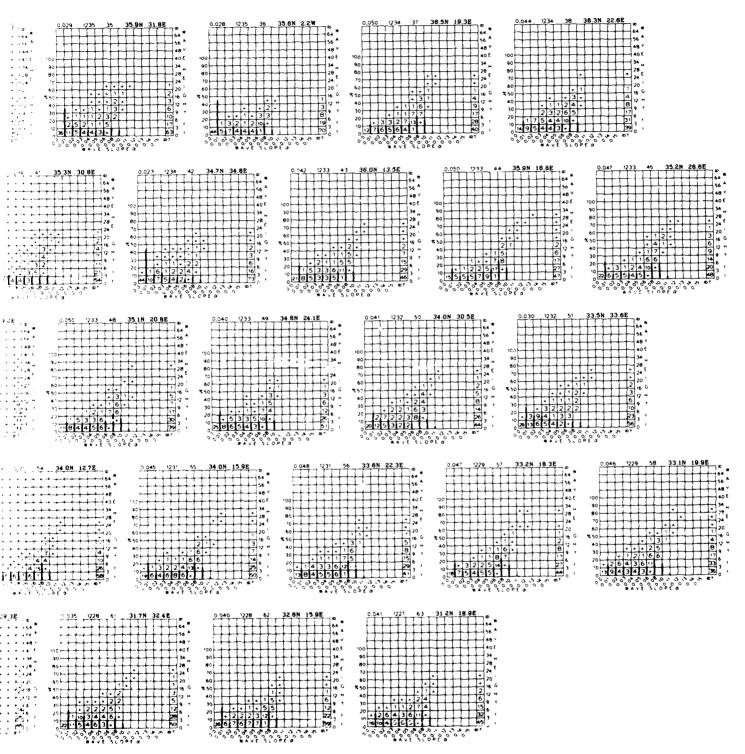


WAVE HEIGHT AND WAVE SLOPE (α) (Cont'd)



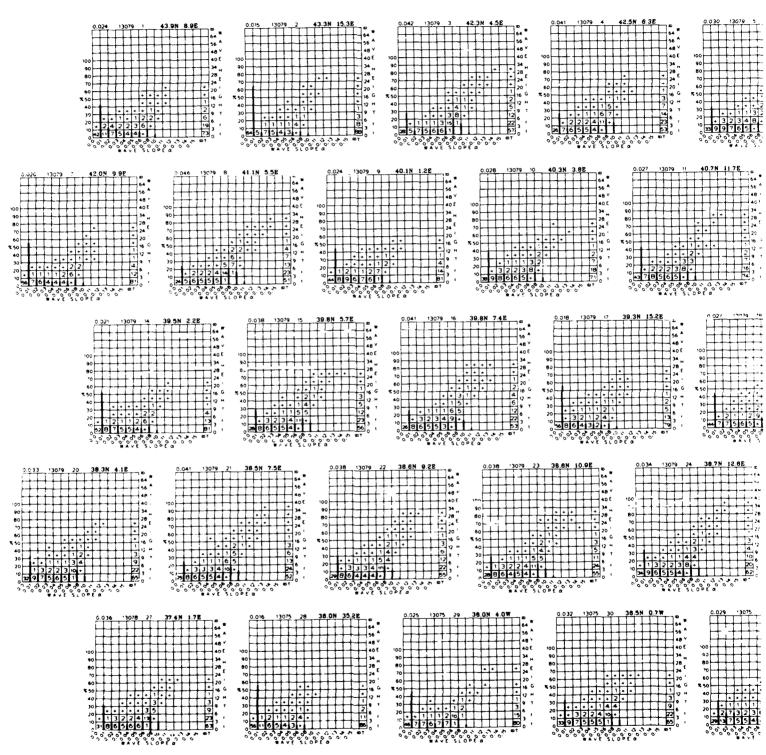
SLOPE (α) (Cont'd)

DECEMBER

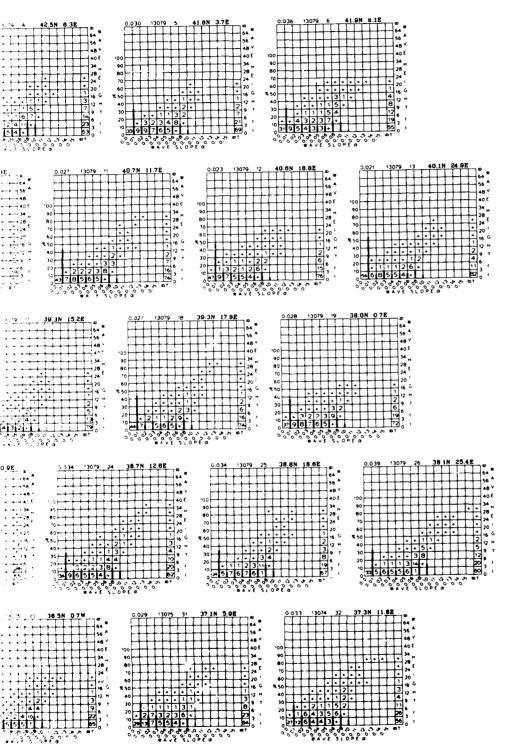


ANNUAL

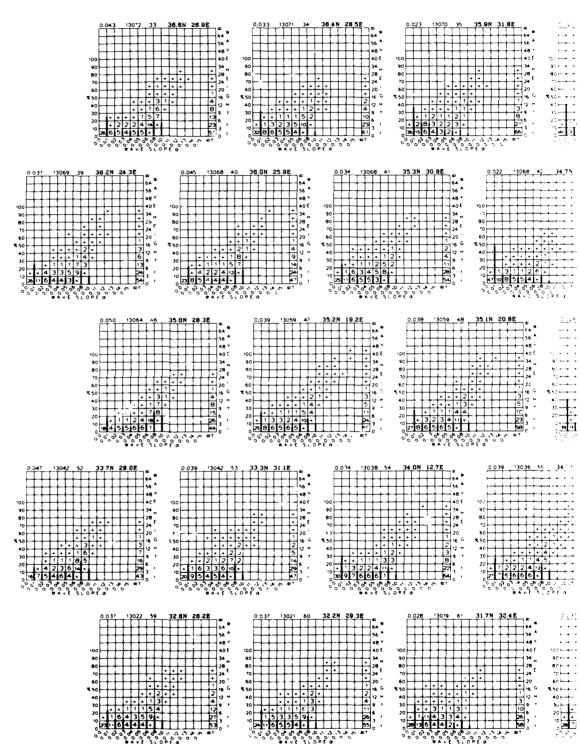
WAVE HEIGH



WAVE HEIGHT AND WAVE SLOPE (lpha)



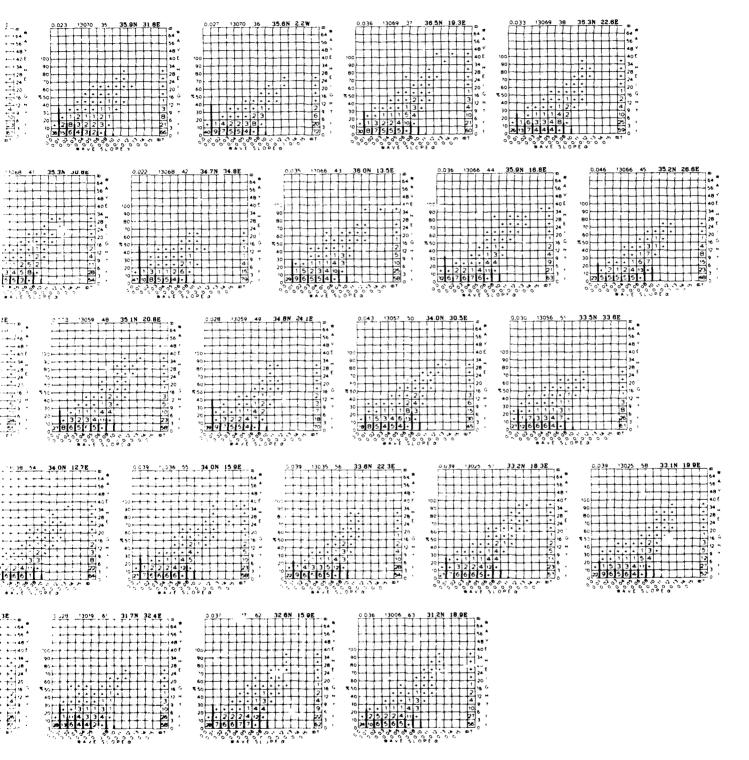
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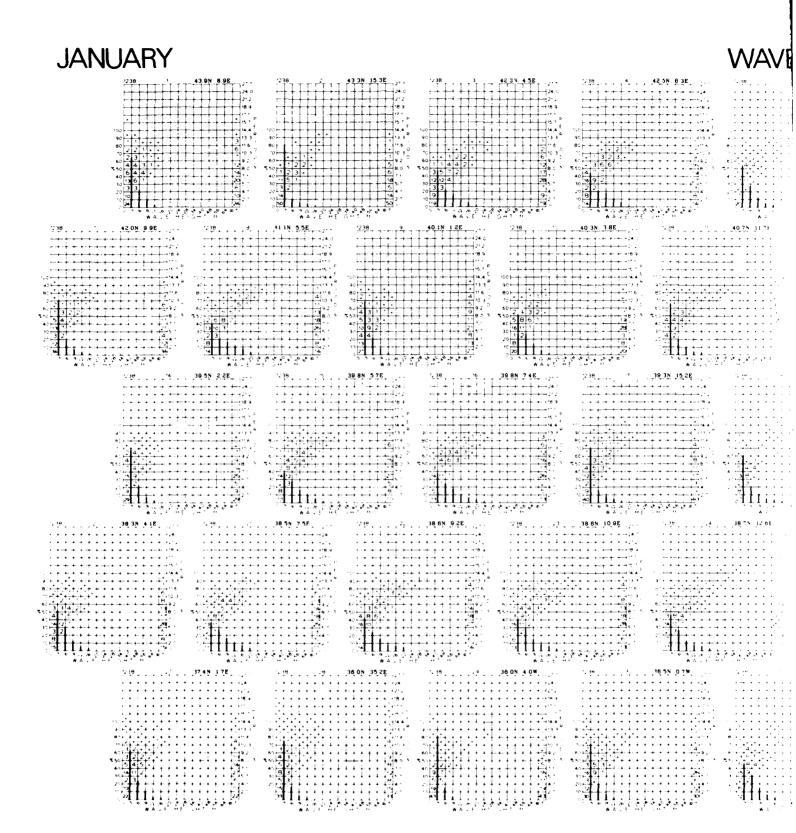


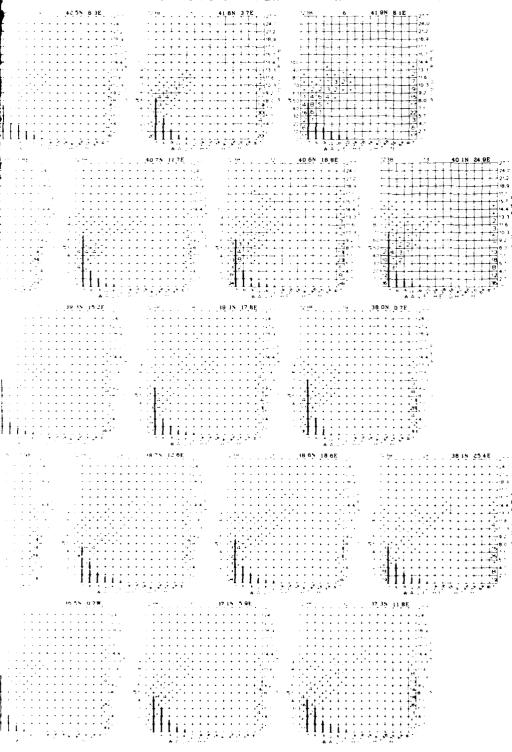
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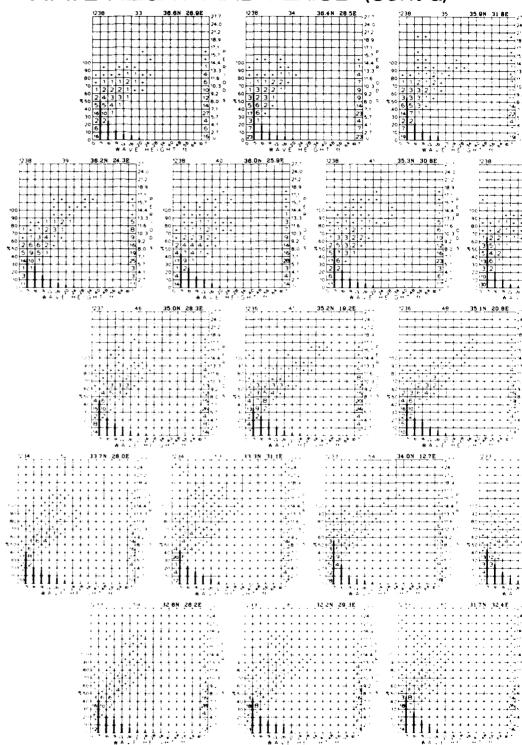
SLOPE (α) (Cont'd)

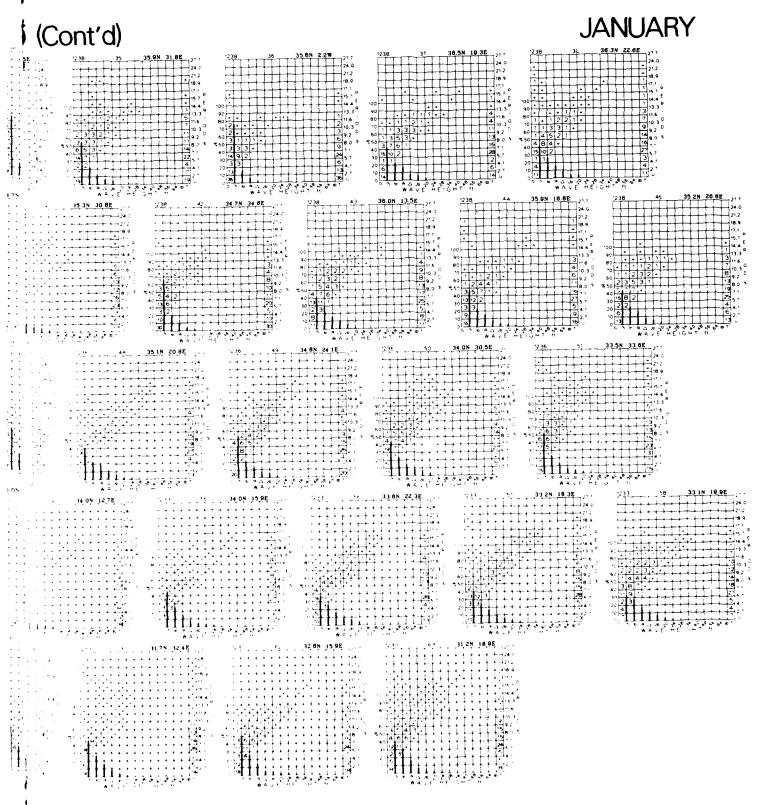
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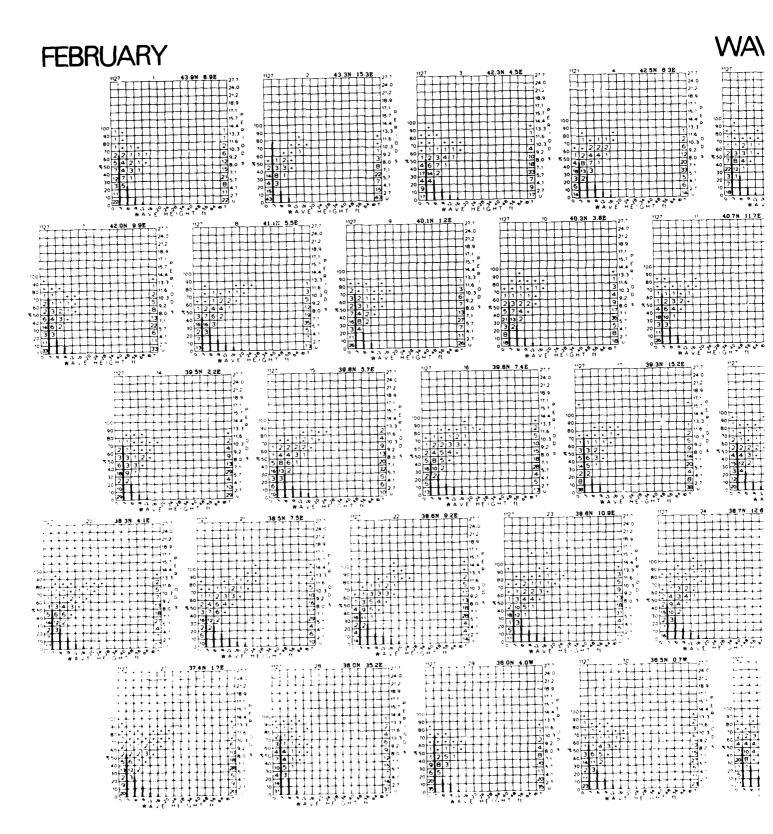


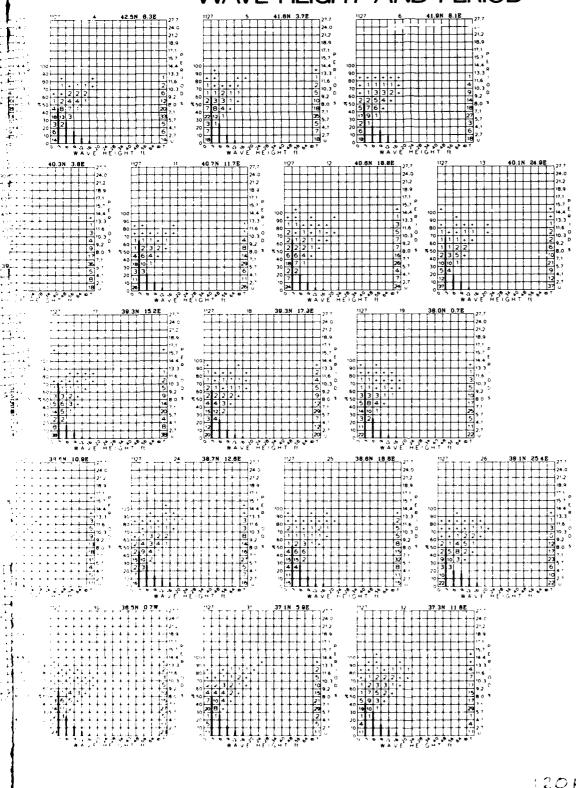


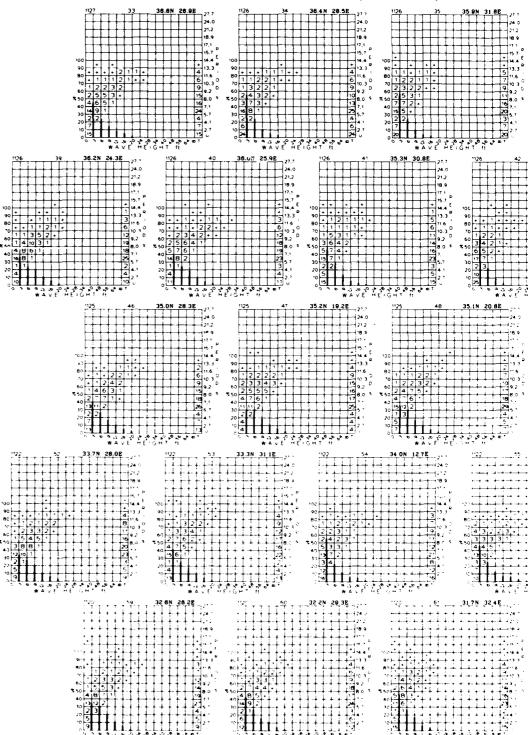


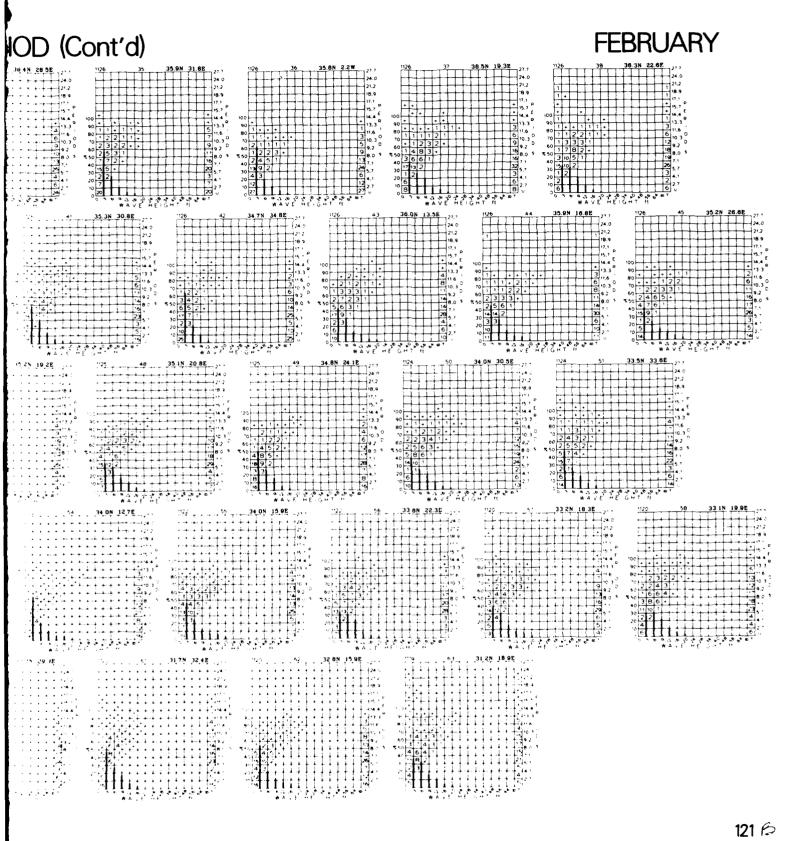


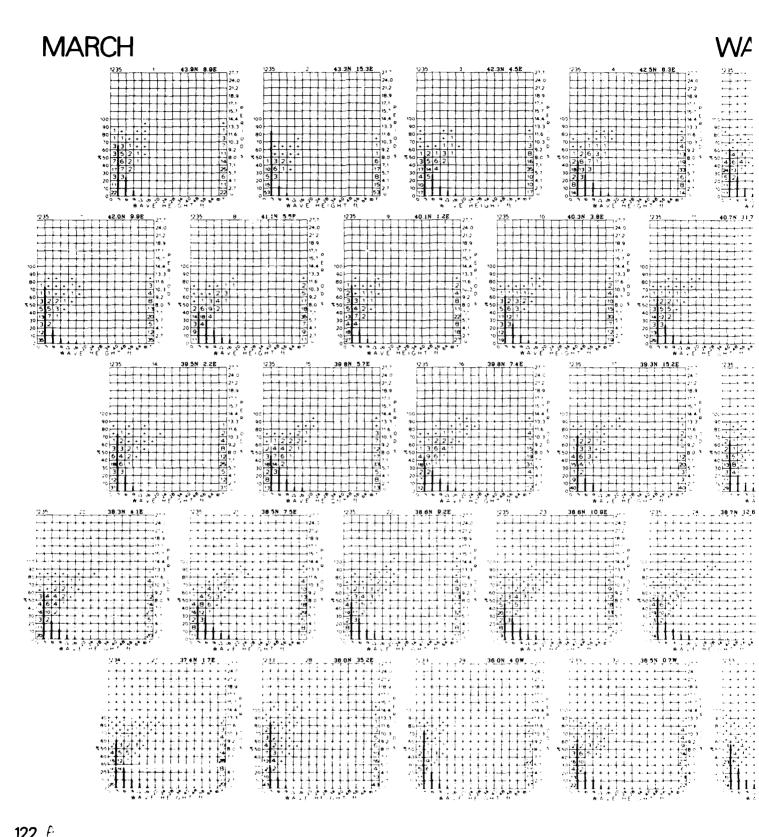


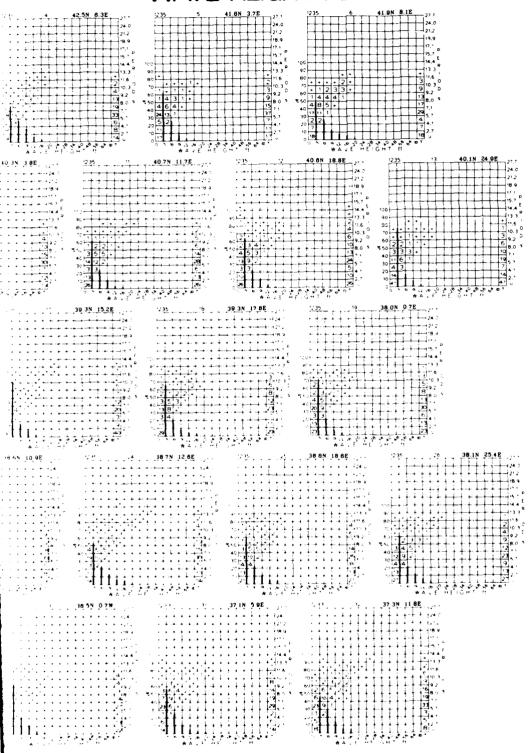


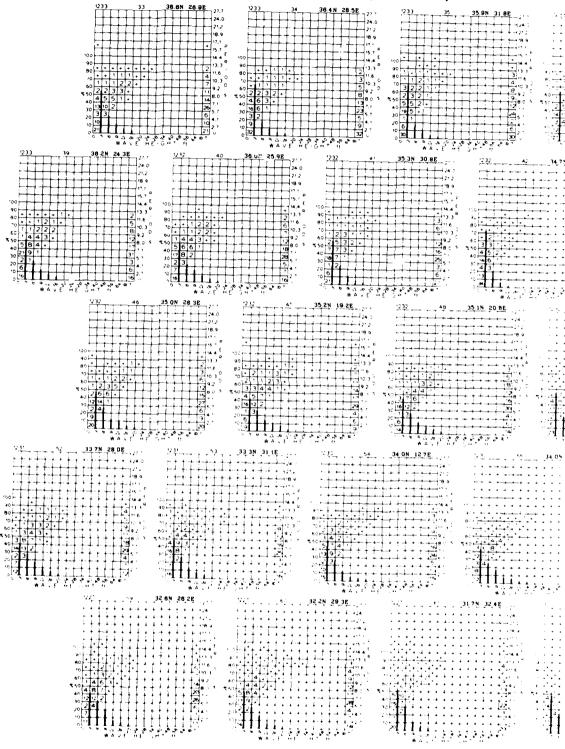


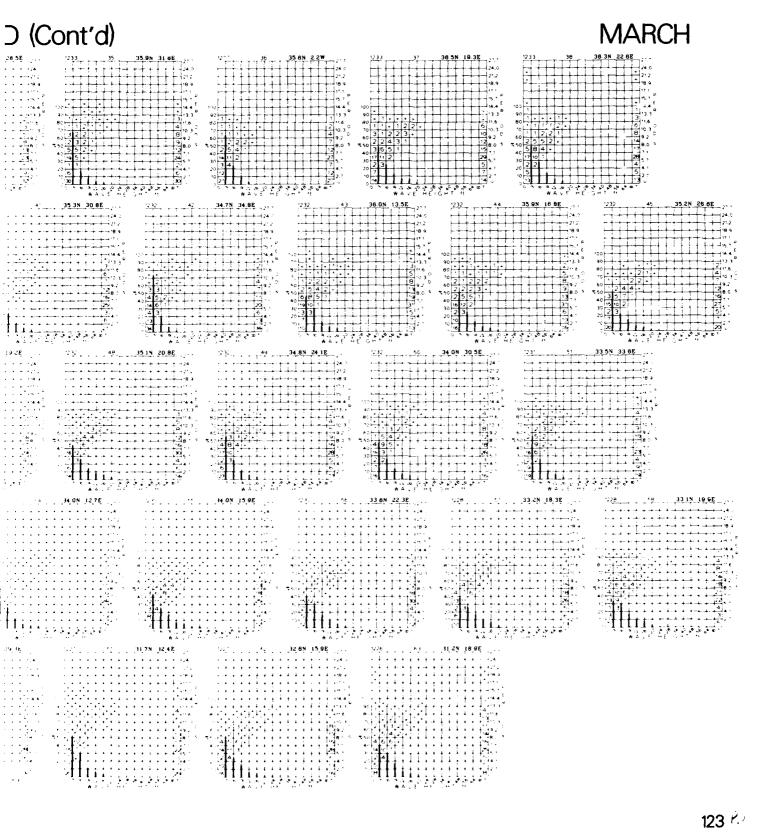


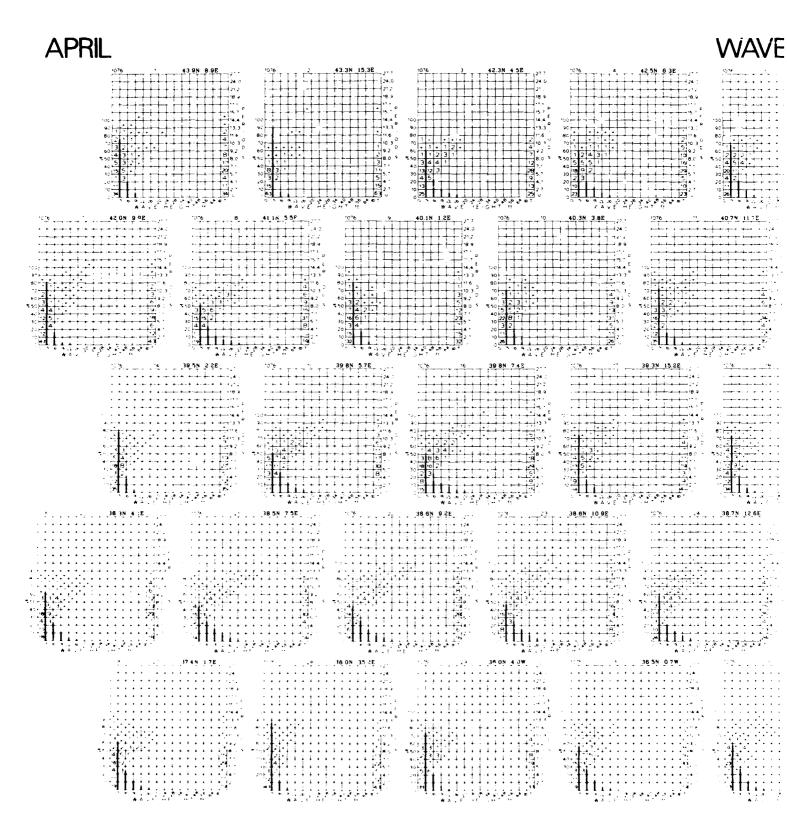


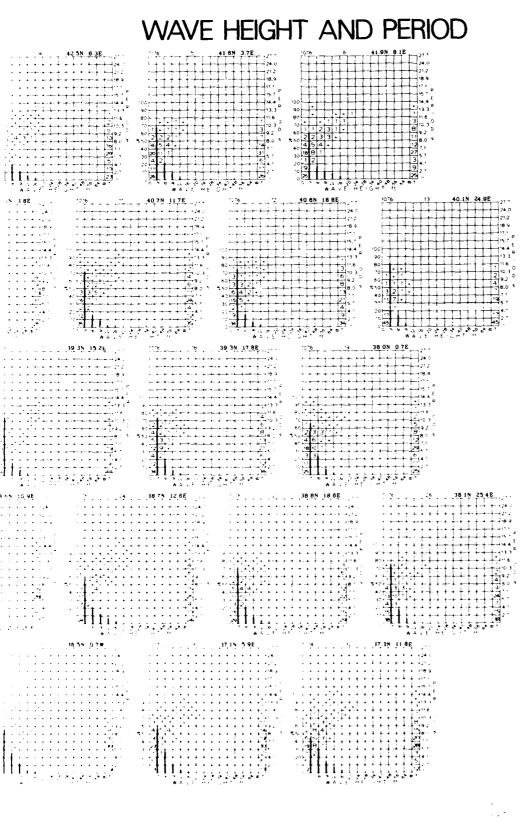


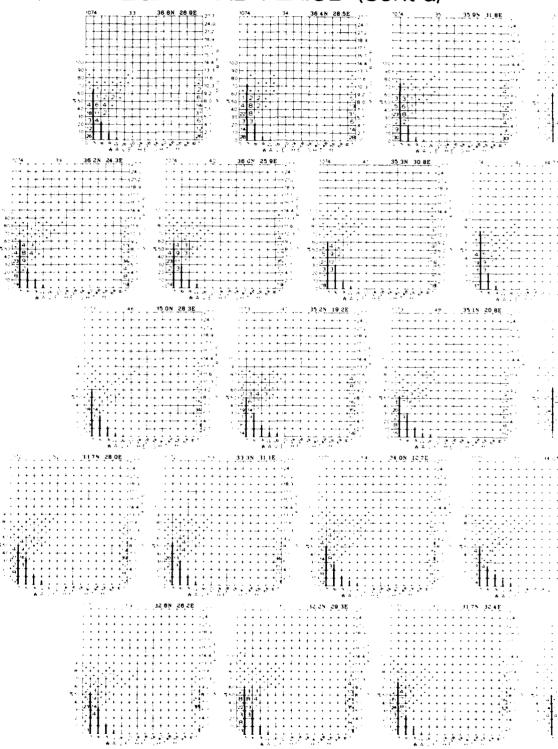


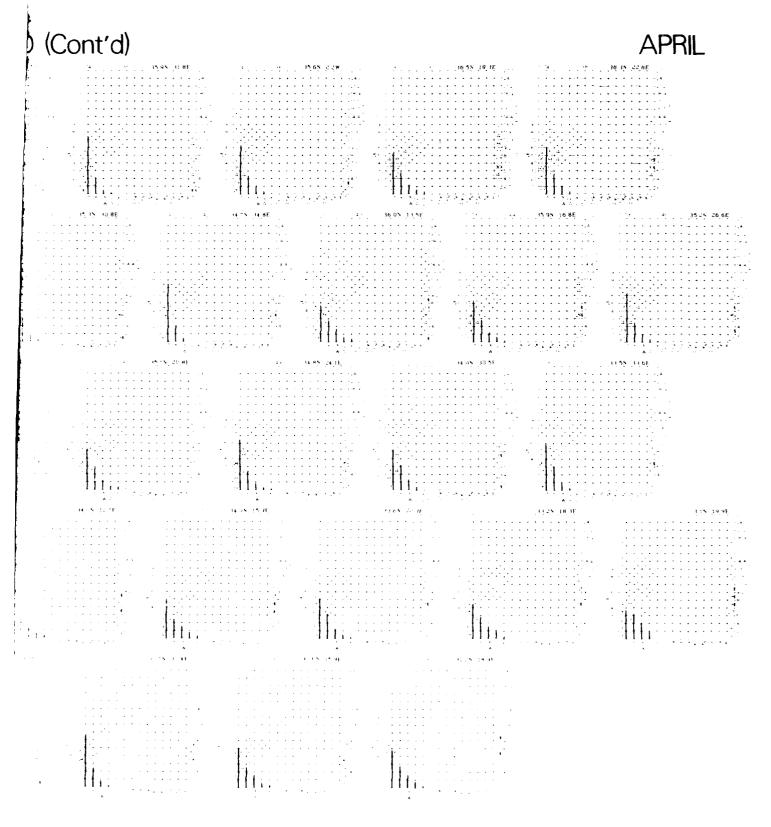


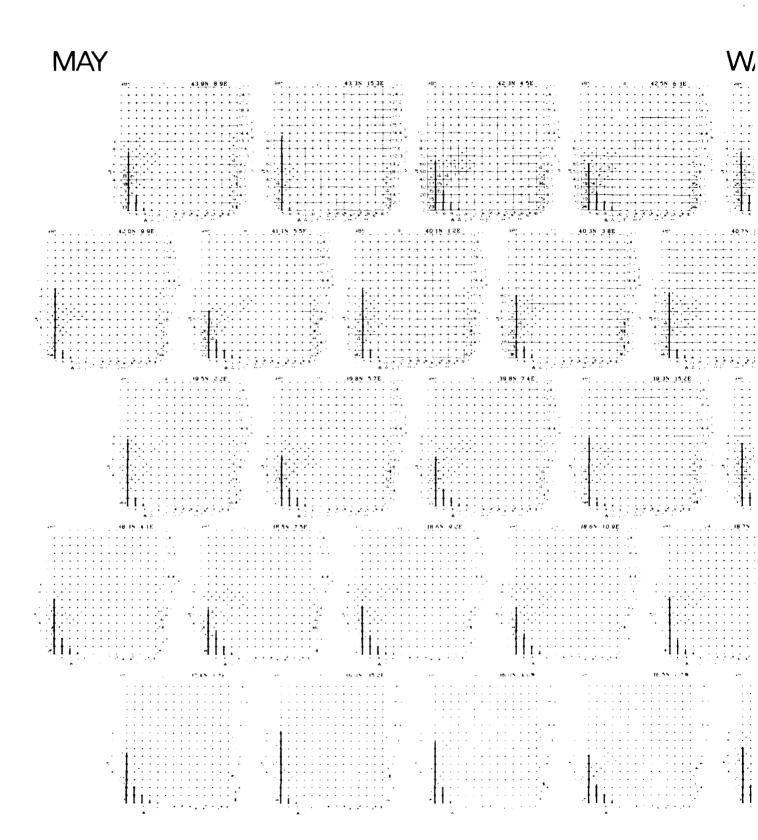


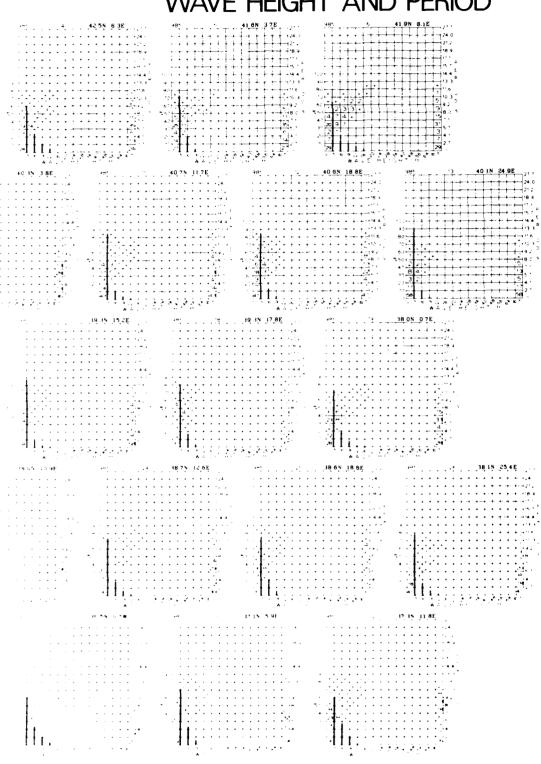


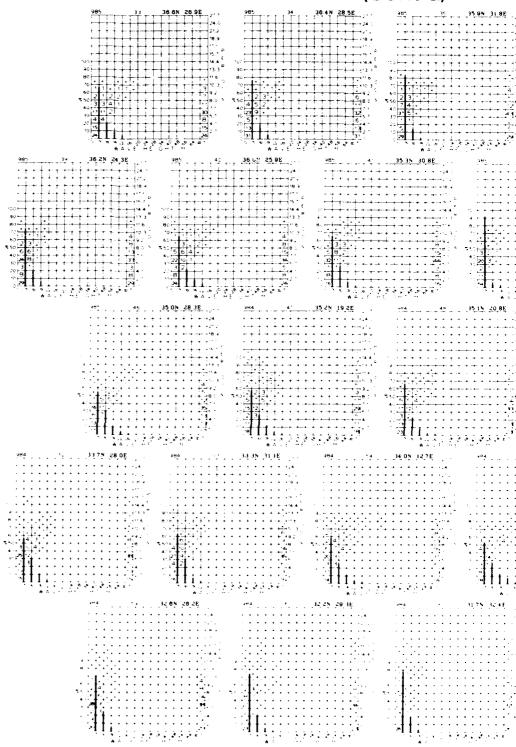


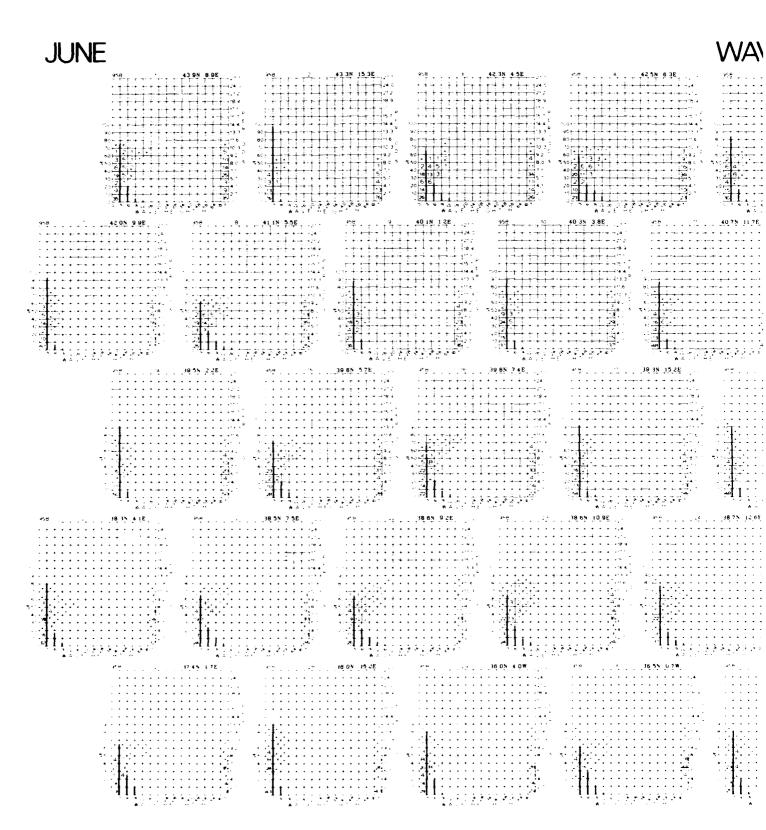


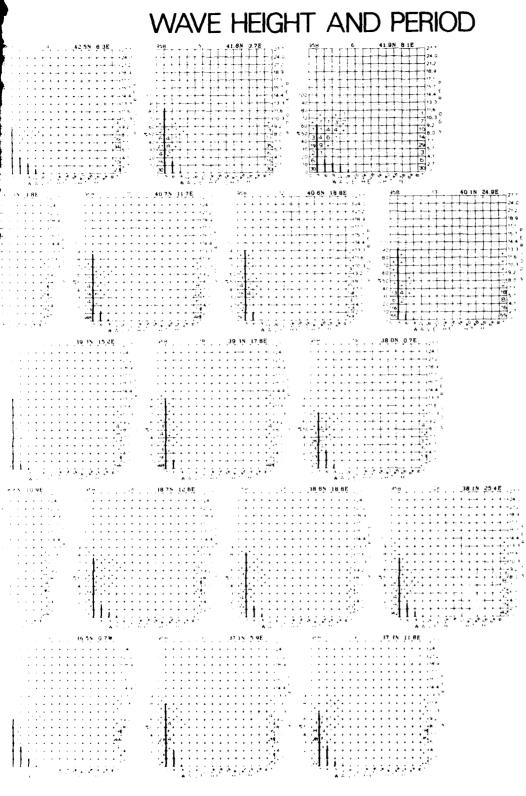


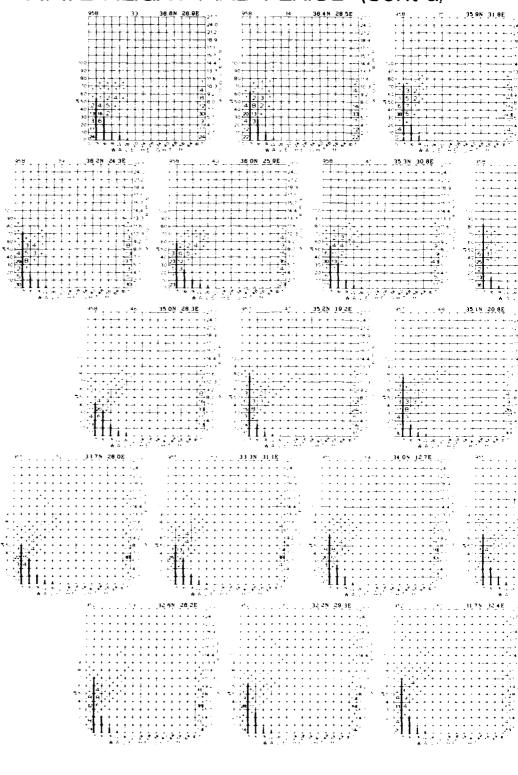


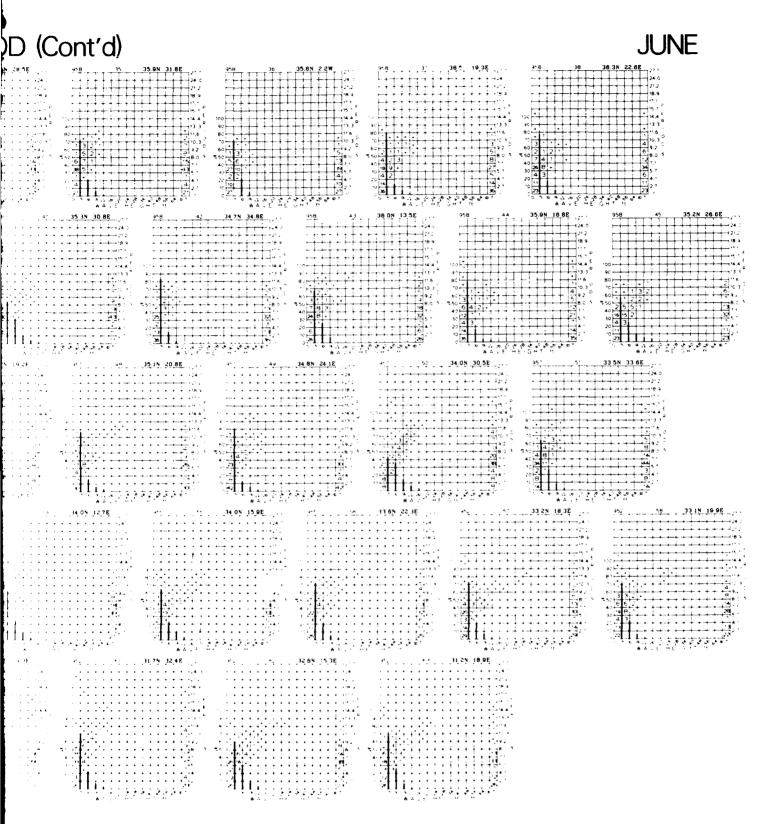


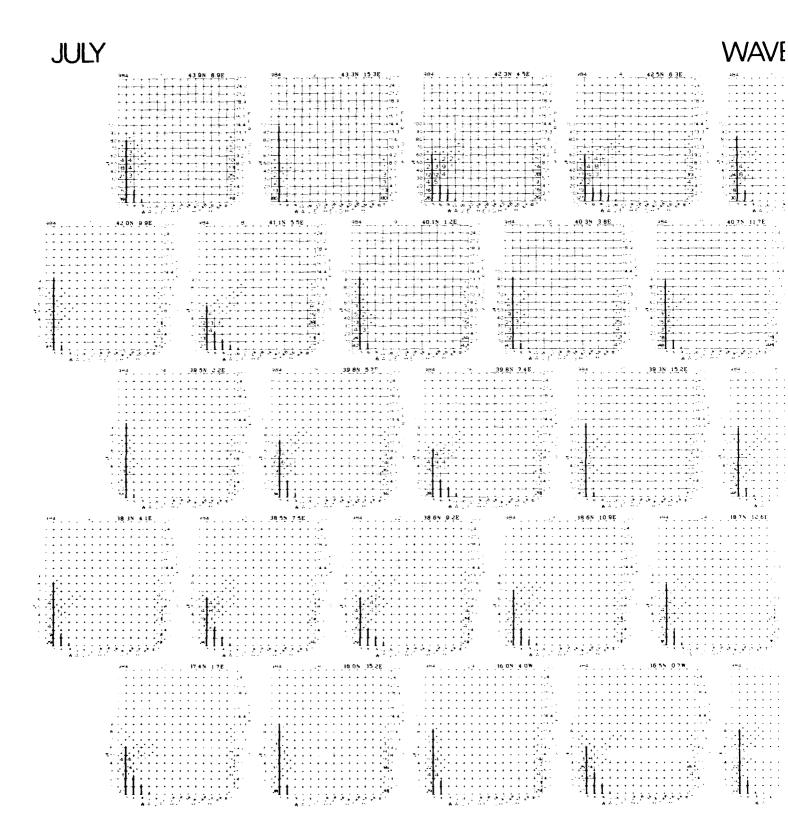


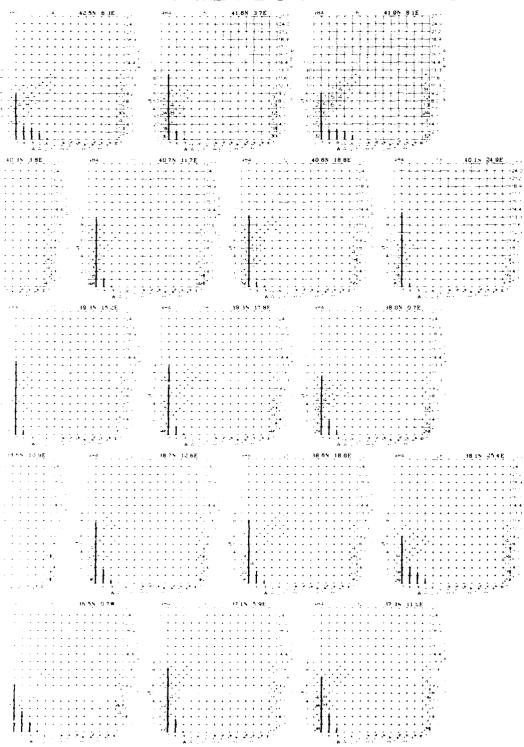


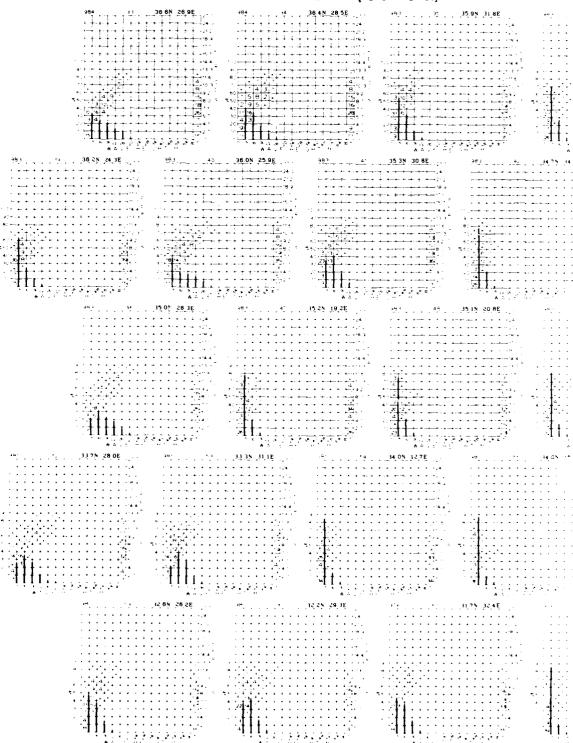


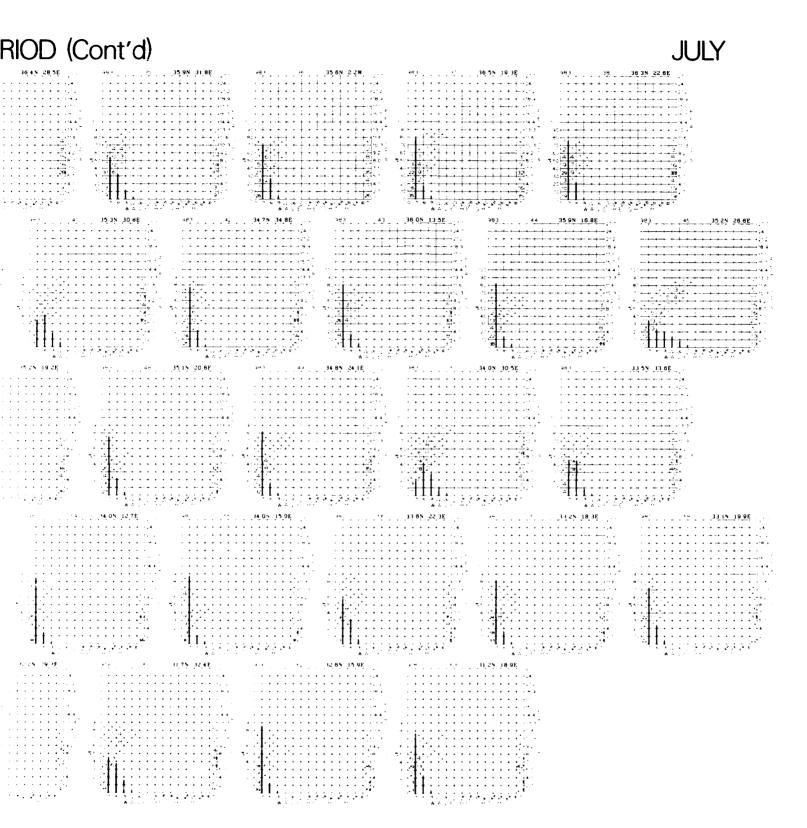


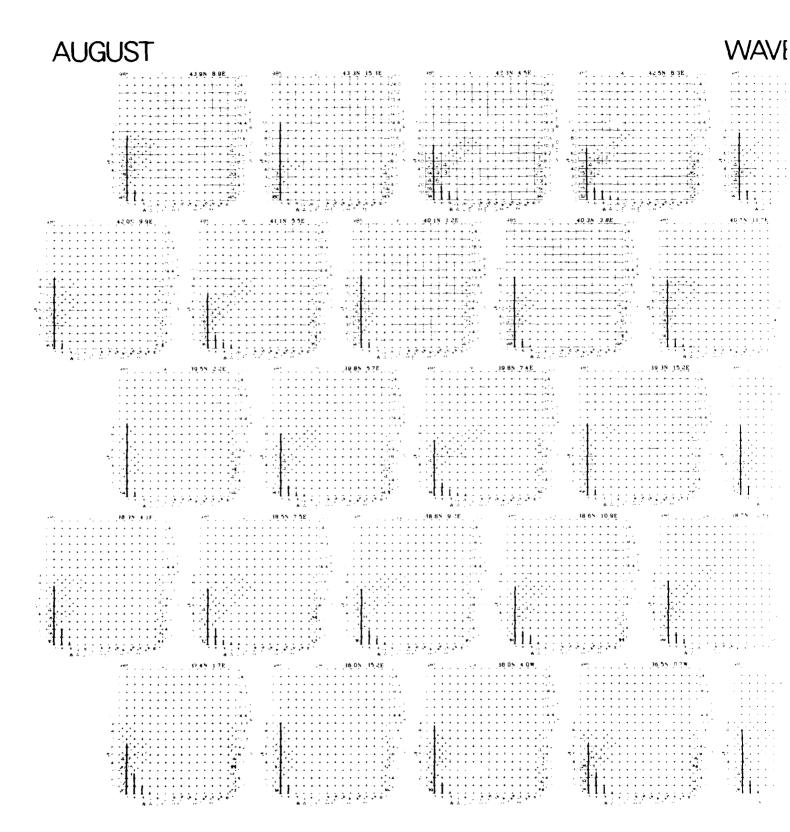


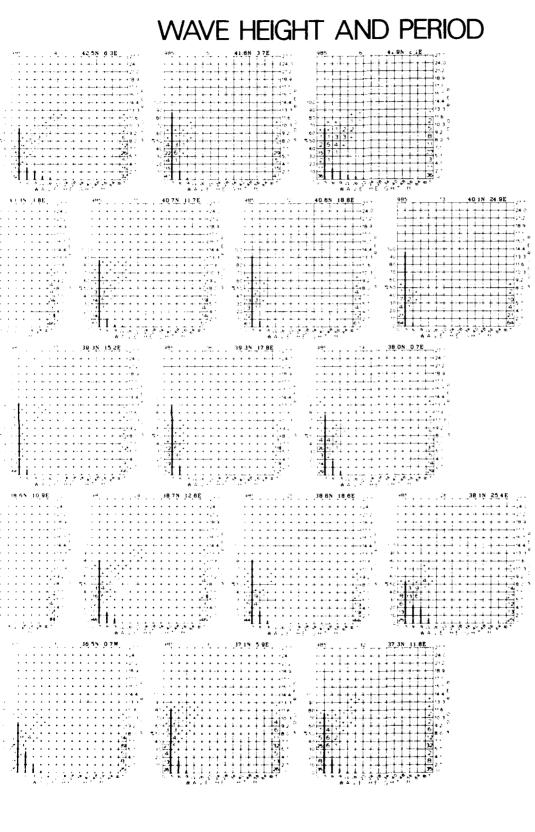


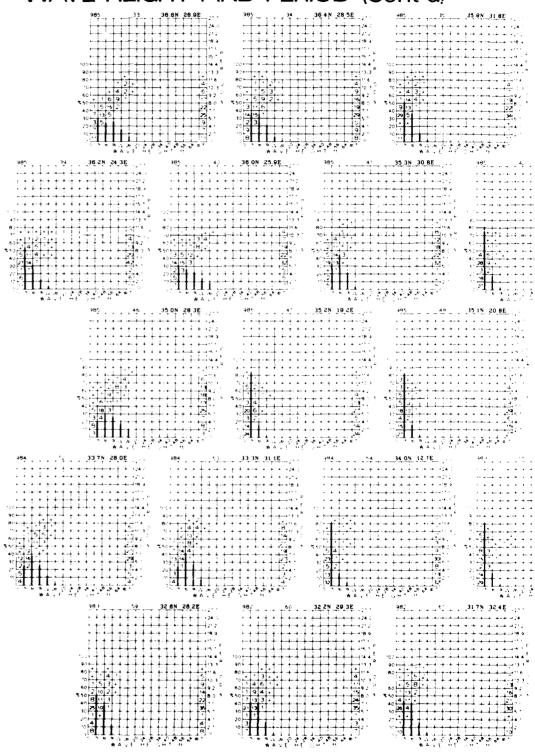


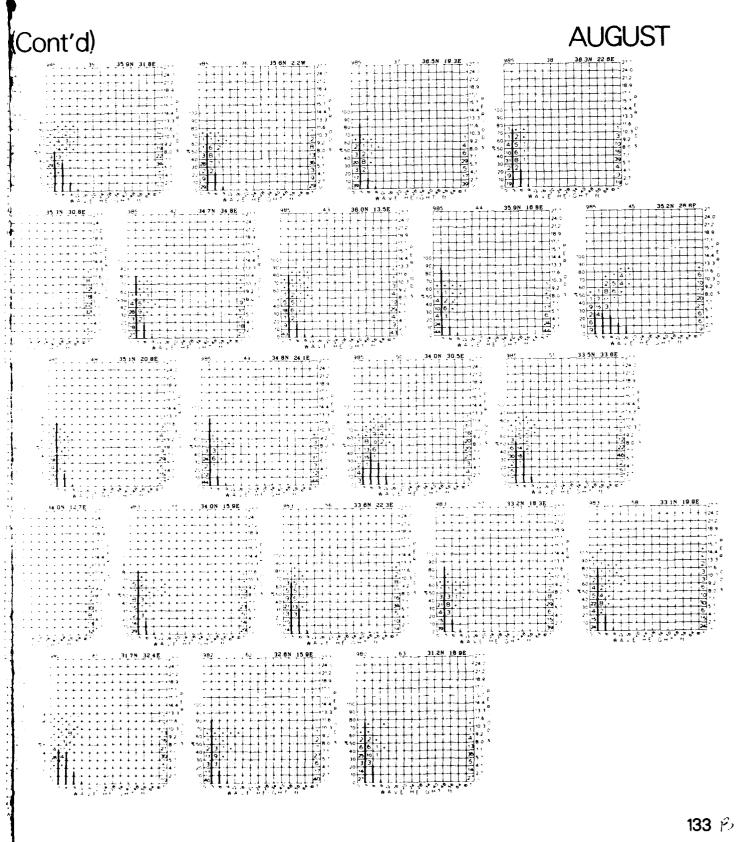


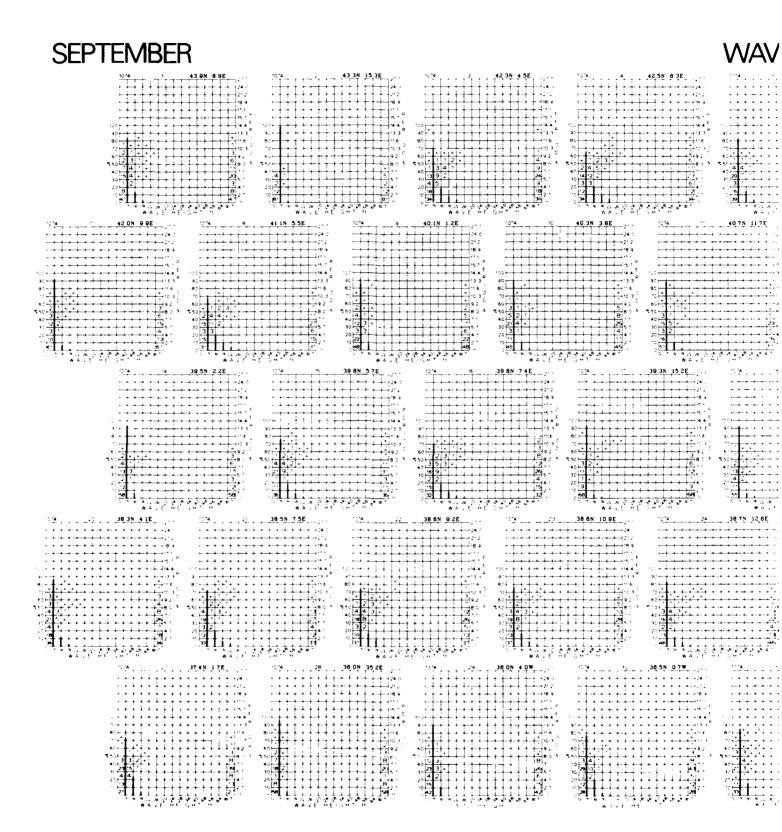


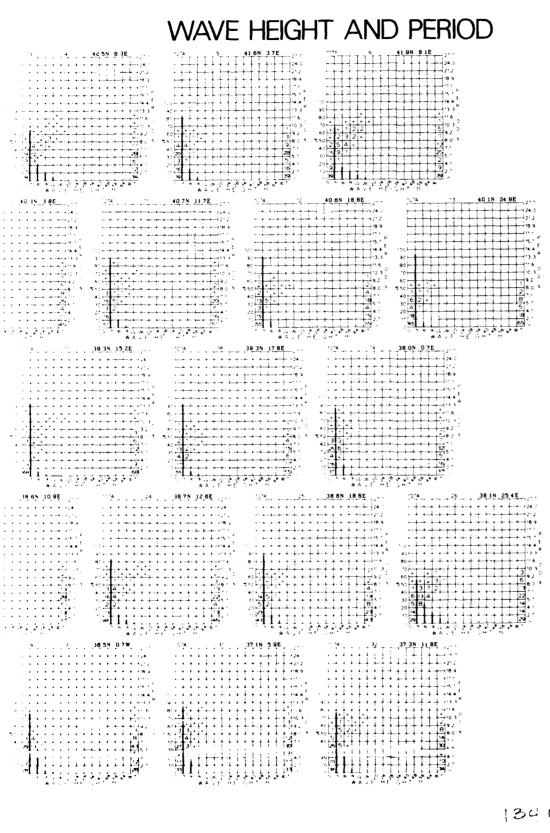


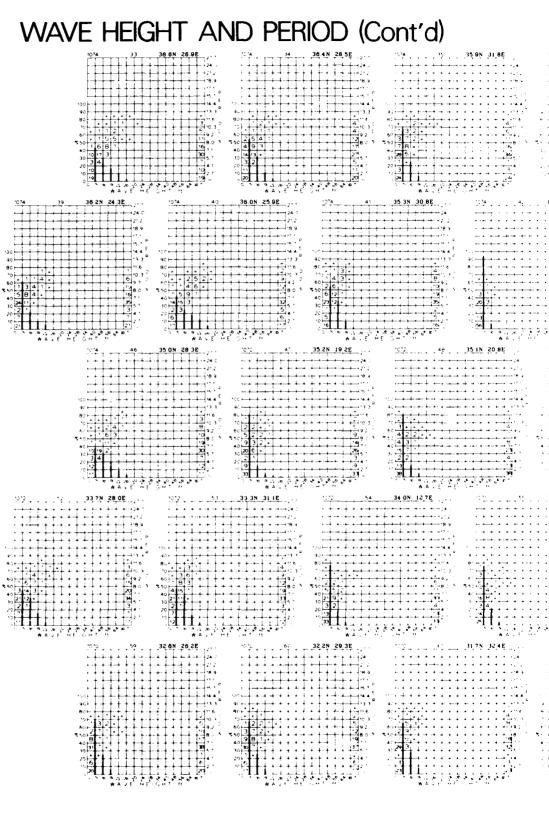


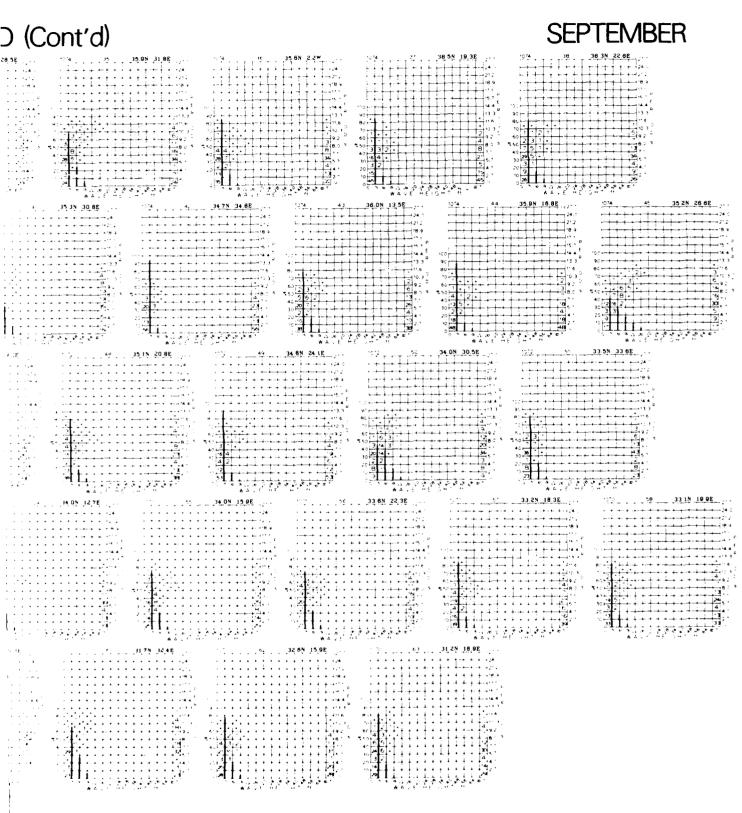


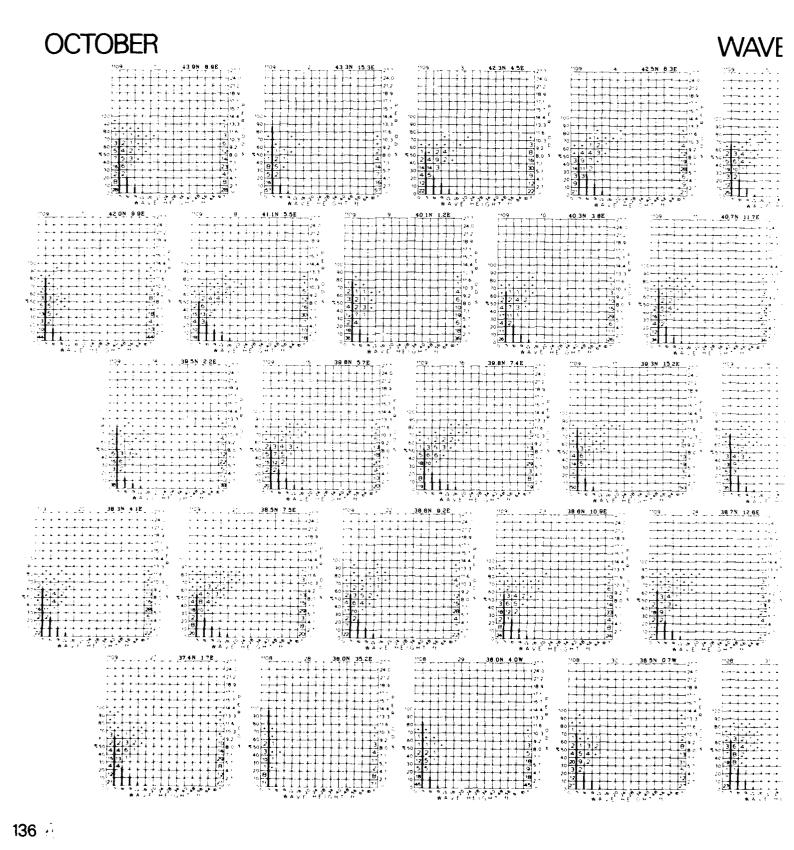


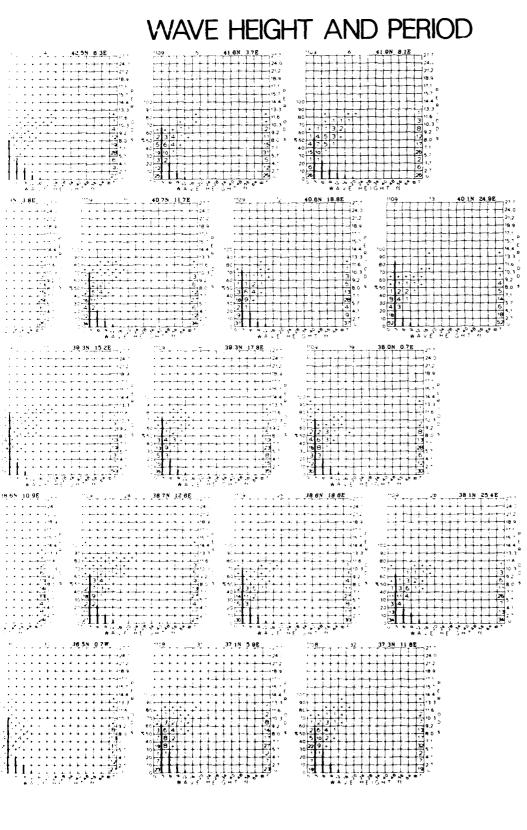


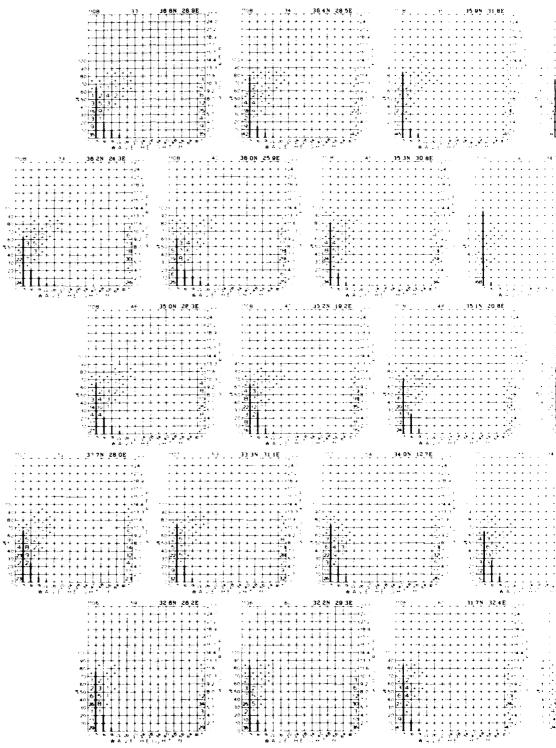


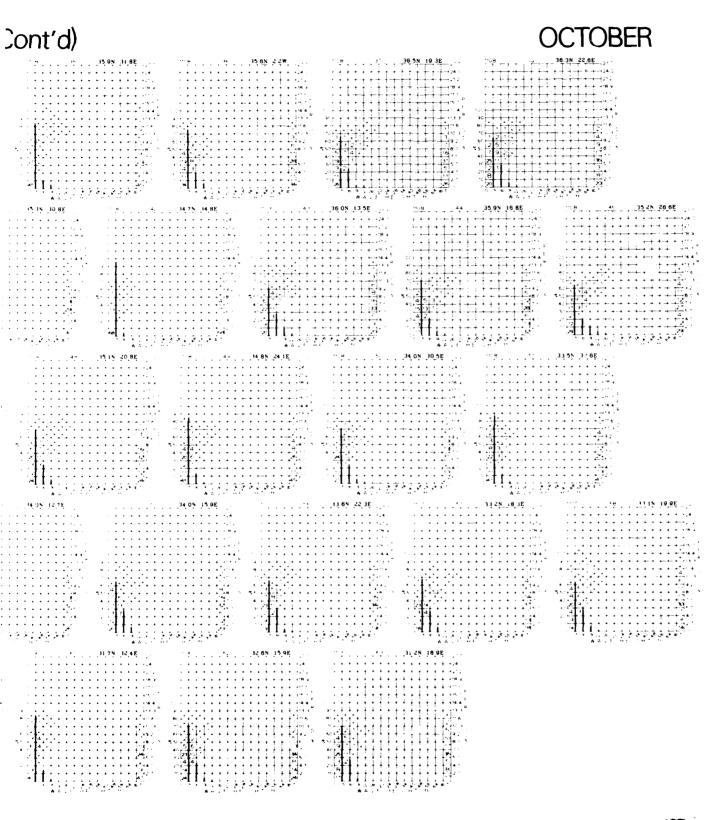


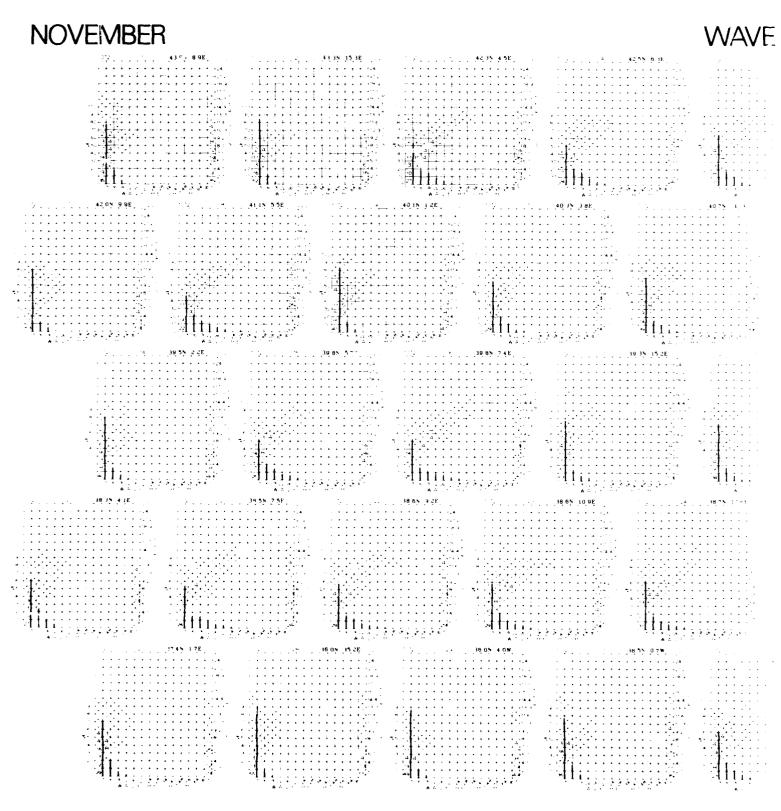


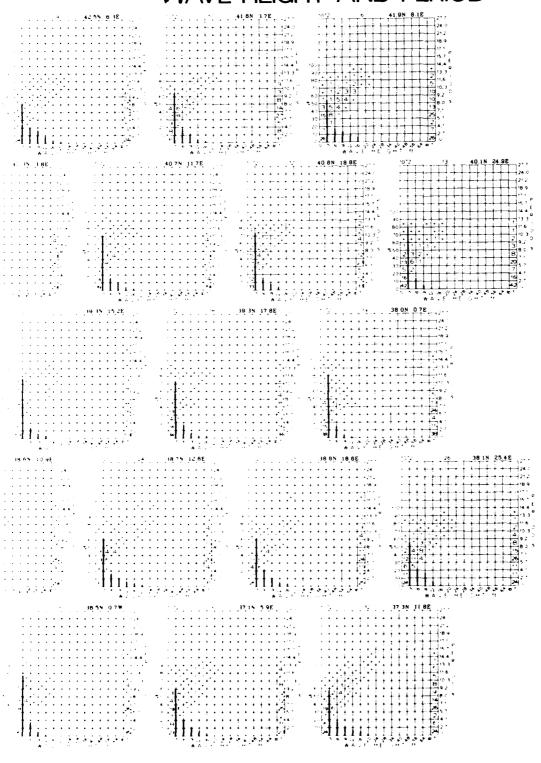


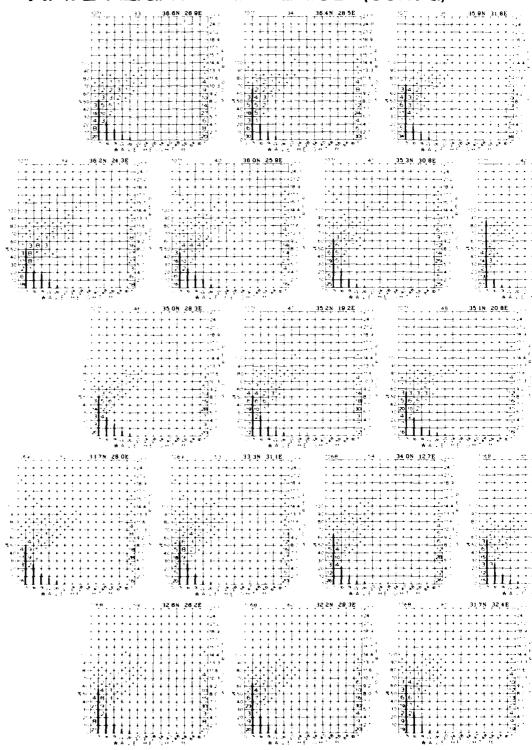


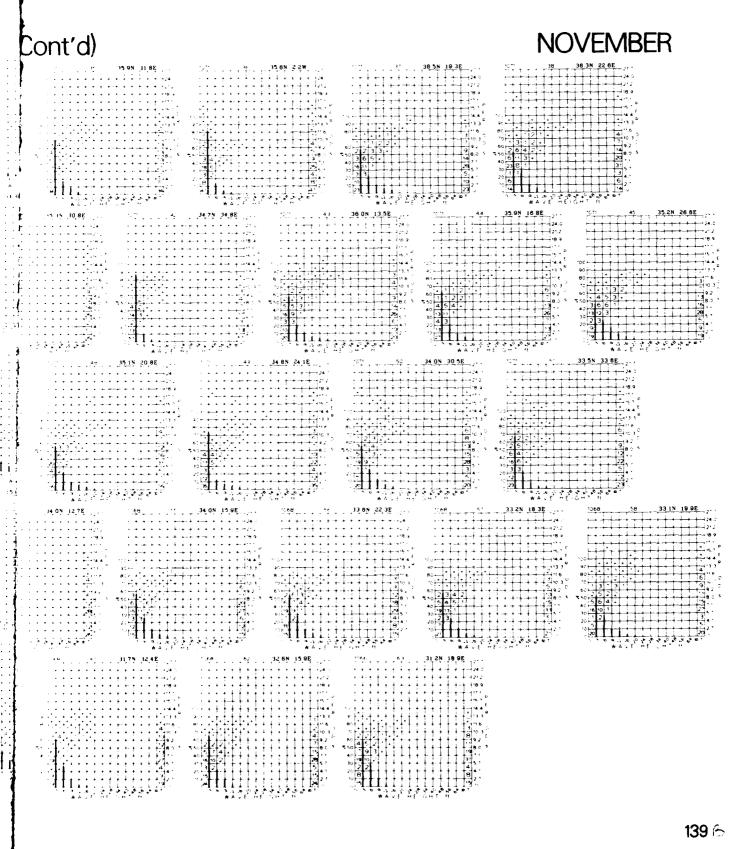


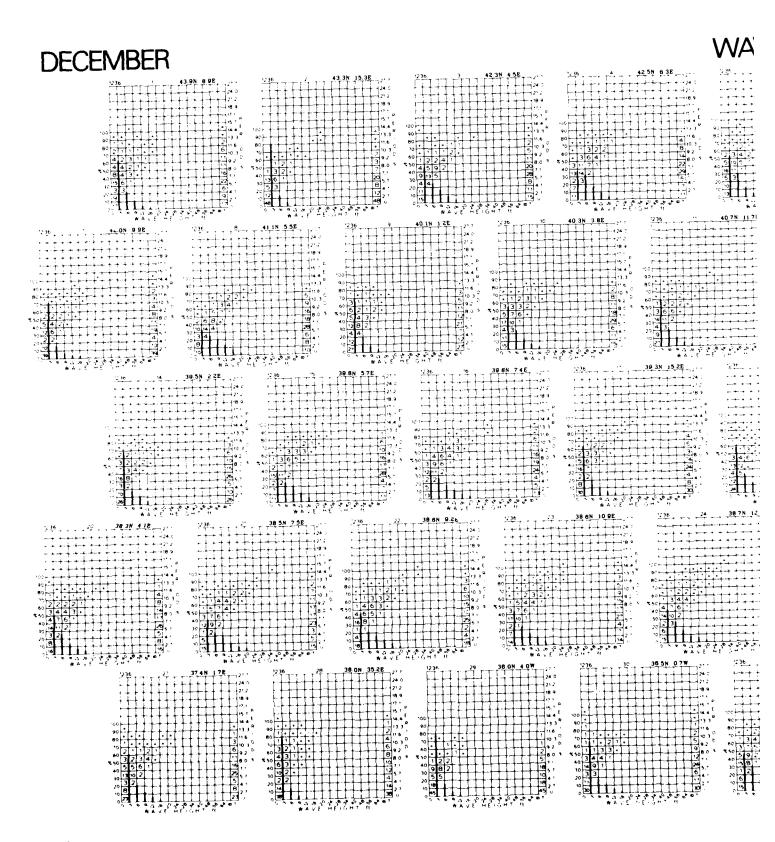


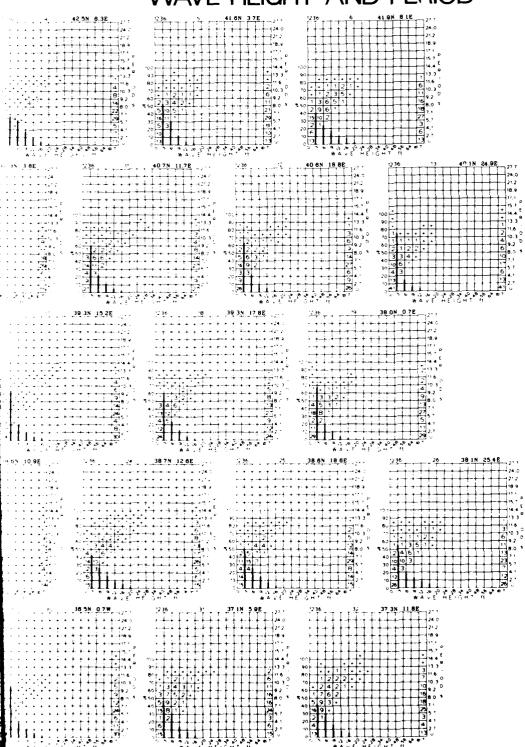


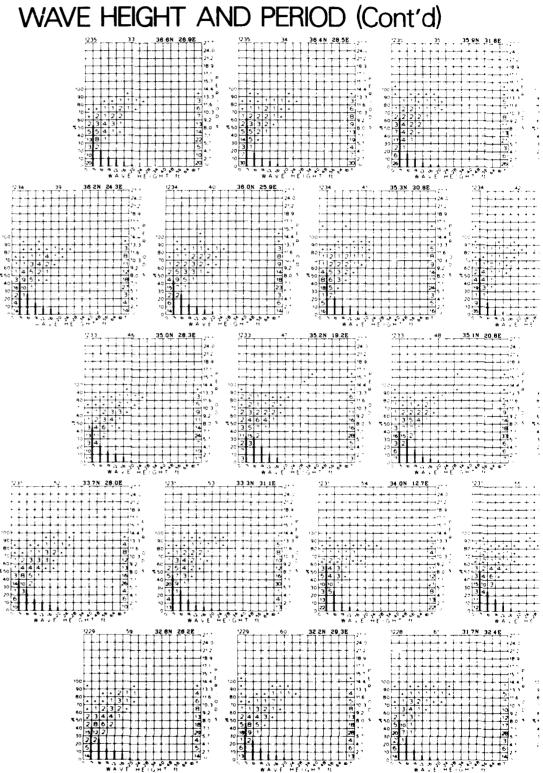


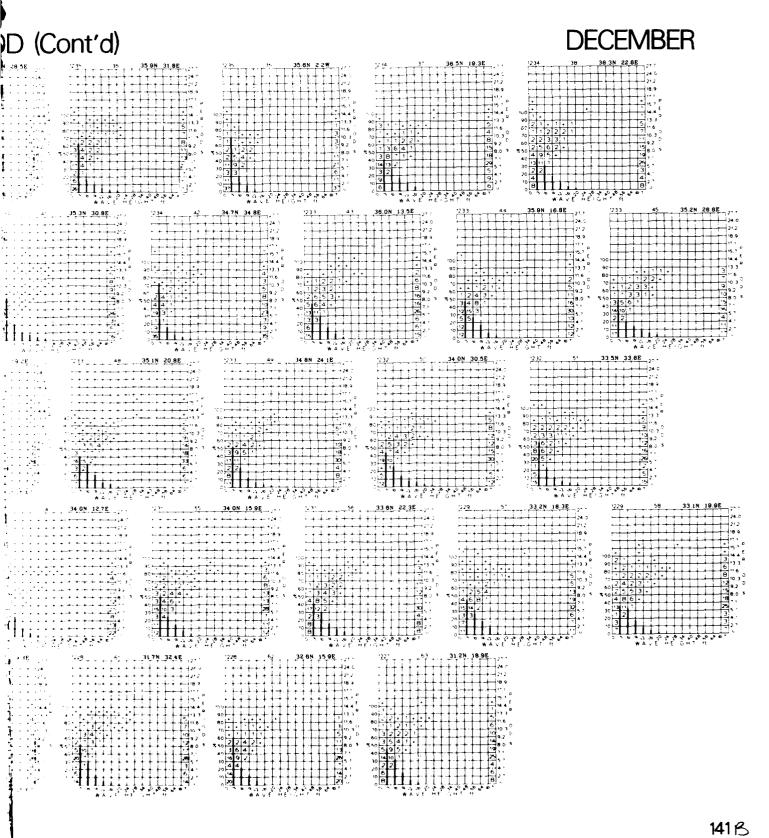


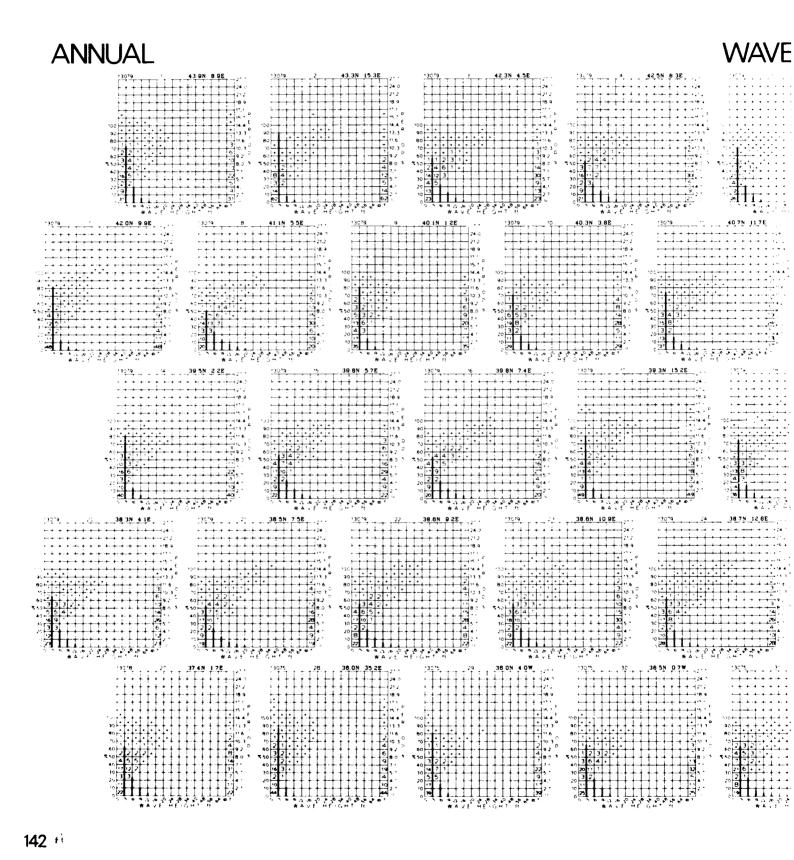


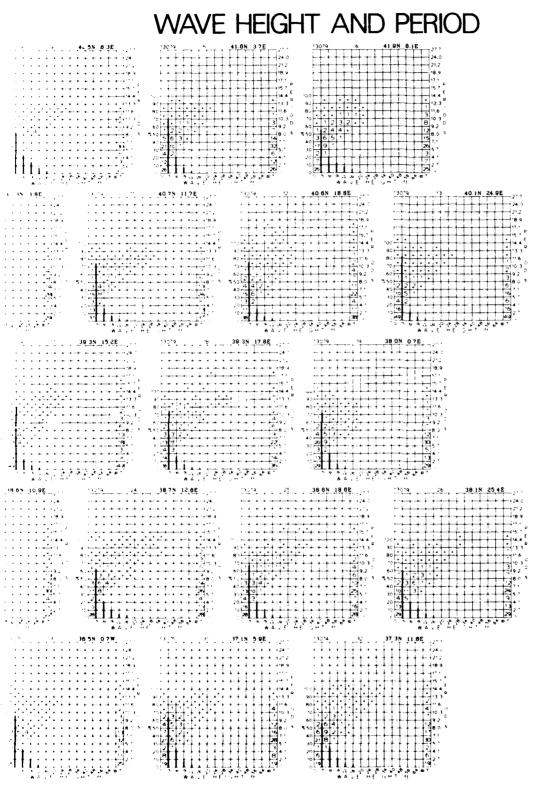


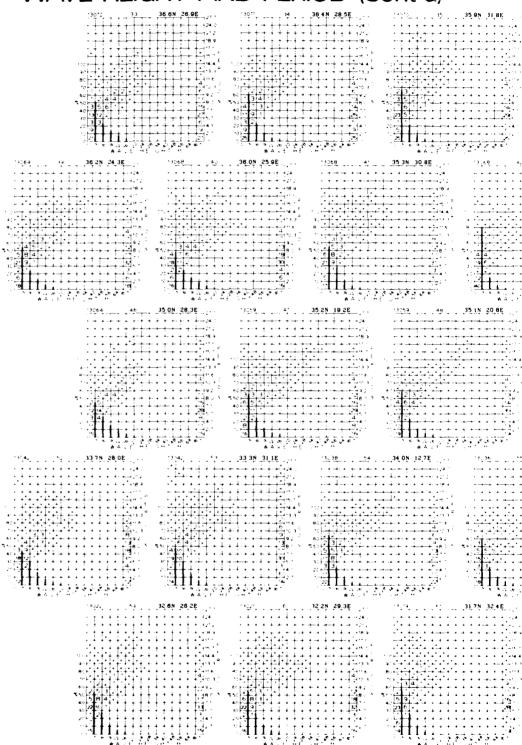


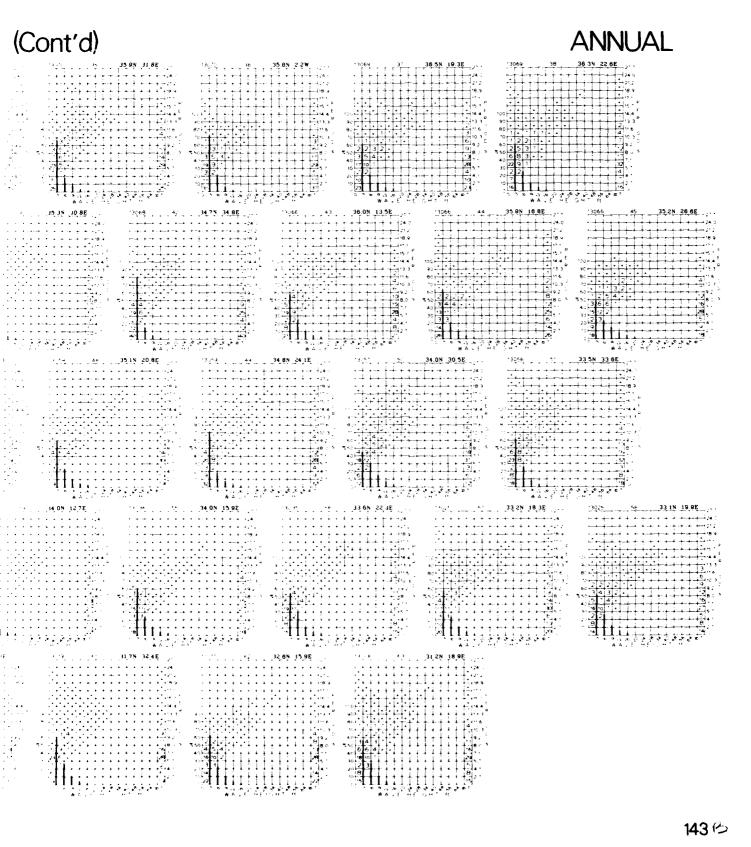






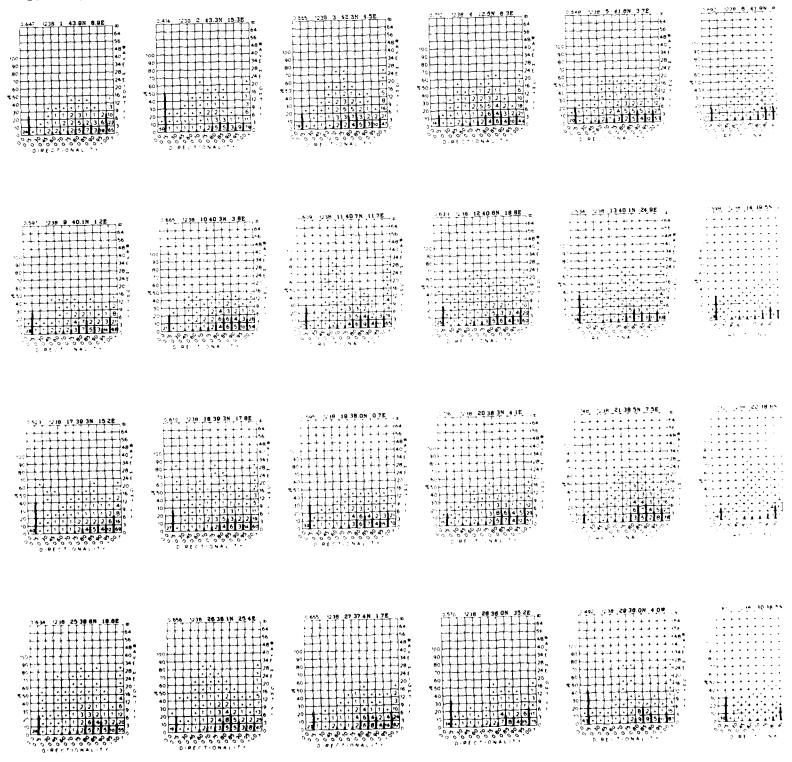




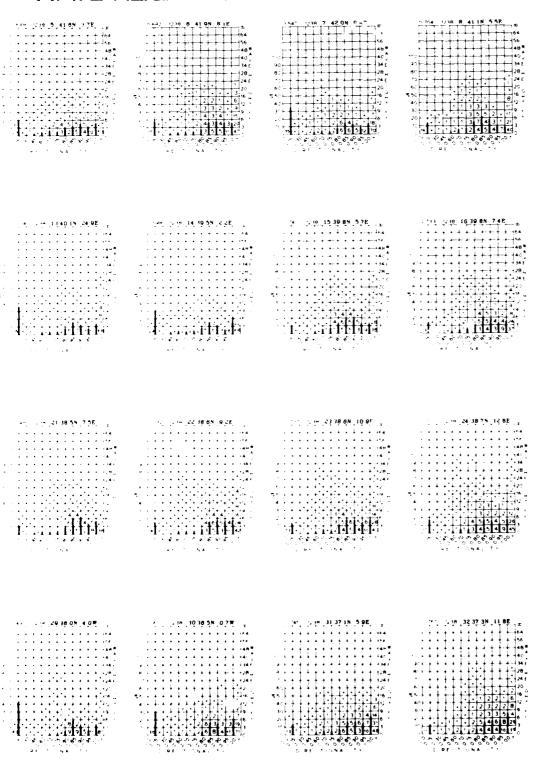


JANUARY

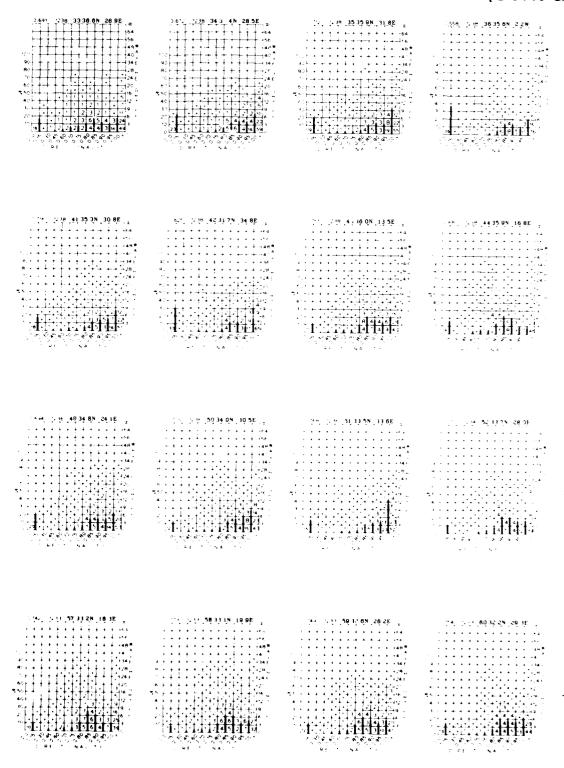
WAVE HEIGHT A



WAVE HEIGHT AND DIRECTIONALITY

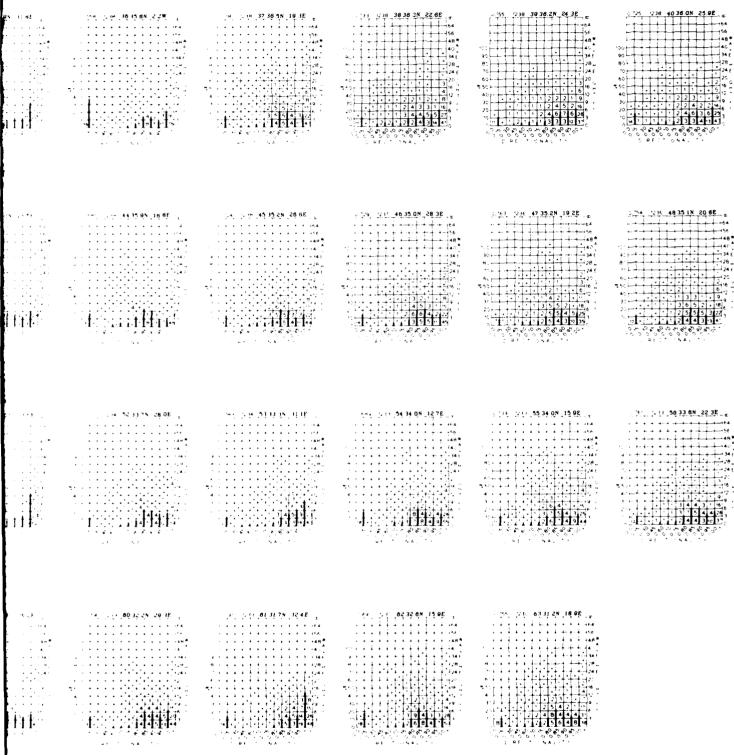


WAVE HEIGHT AND DIRECTIONALITY (Cont.d)



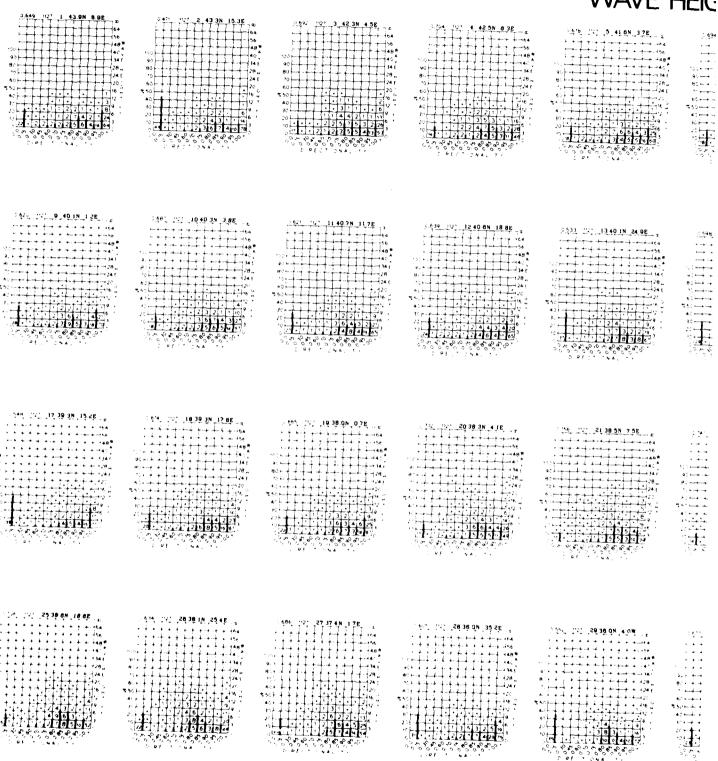
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JANUARY



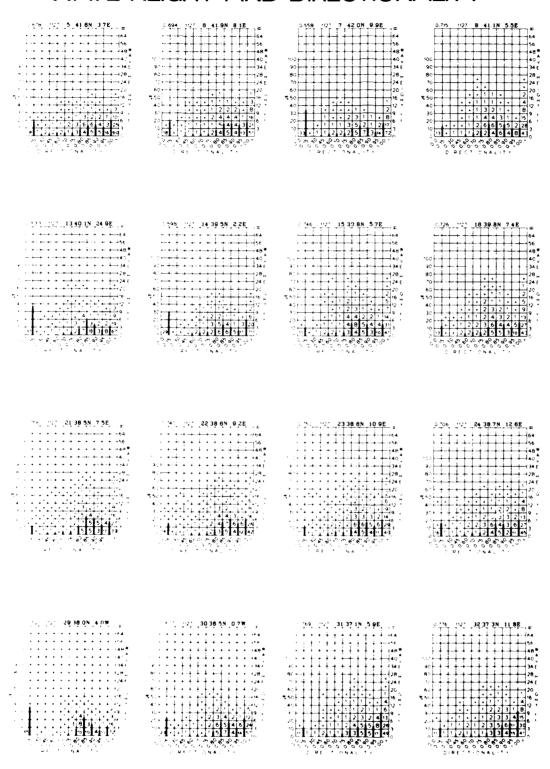
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WAVE HEIG

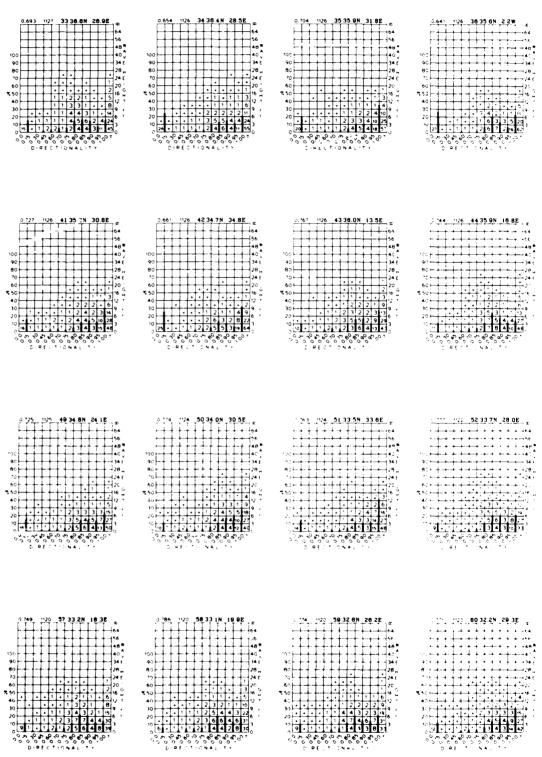


146 A

WAVE HEIGHT AND DIRECTIONALITY

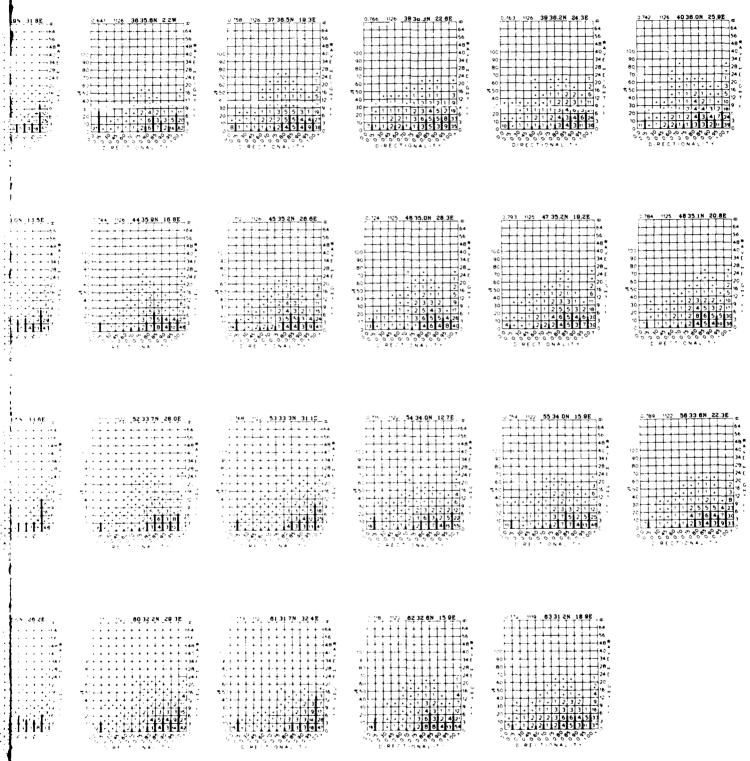


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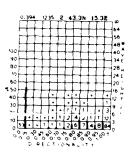


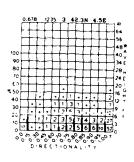
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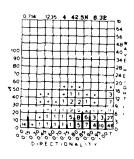
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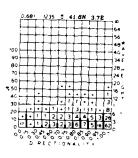


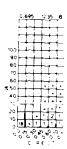
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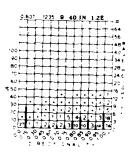


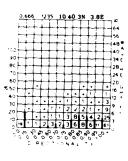


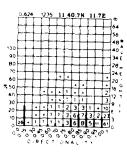


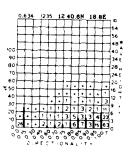


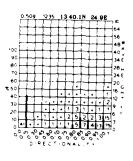
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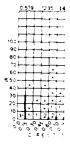


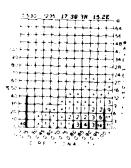


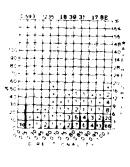


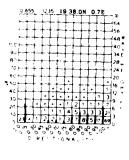


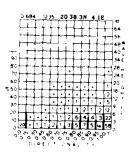


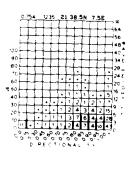




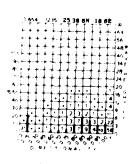


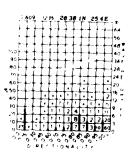


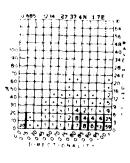


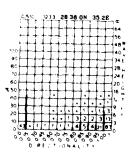


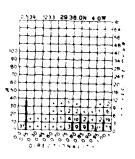






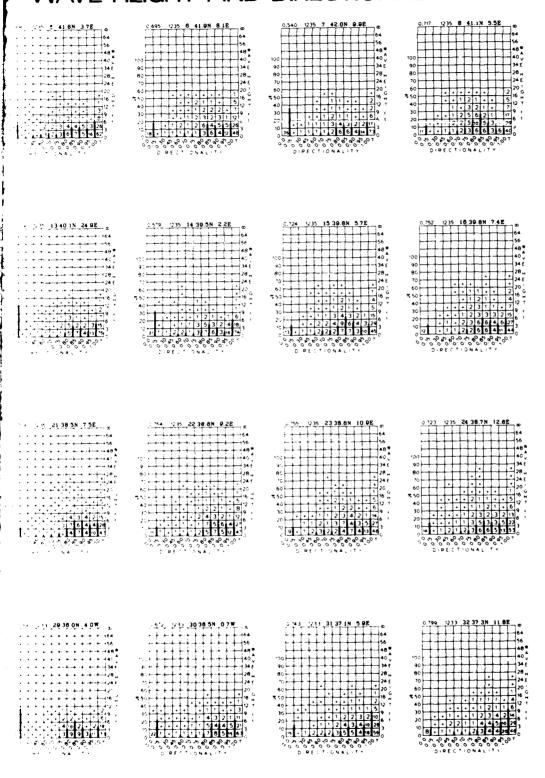




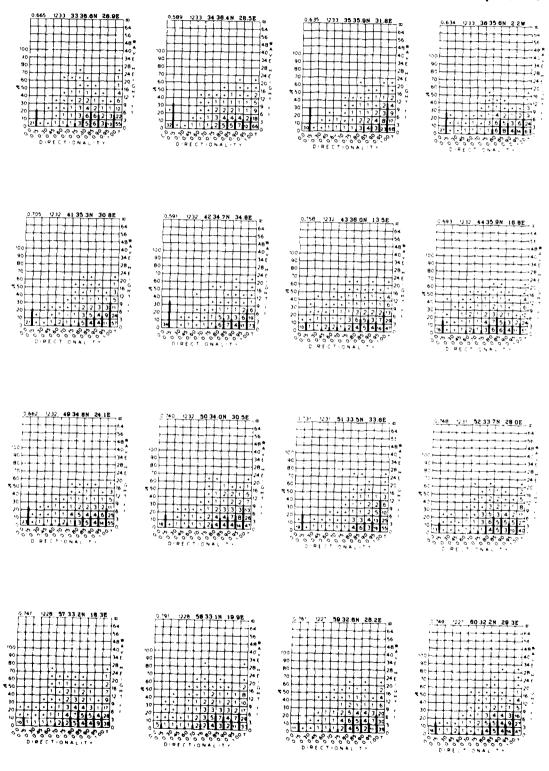




WAVE HEIGHT AND DIRECTIONALITY

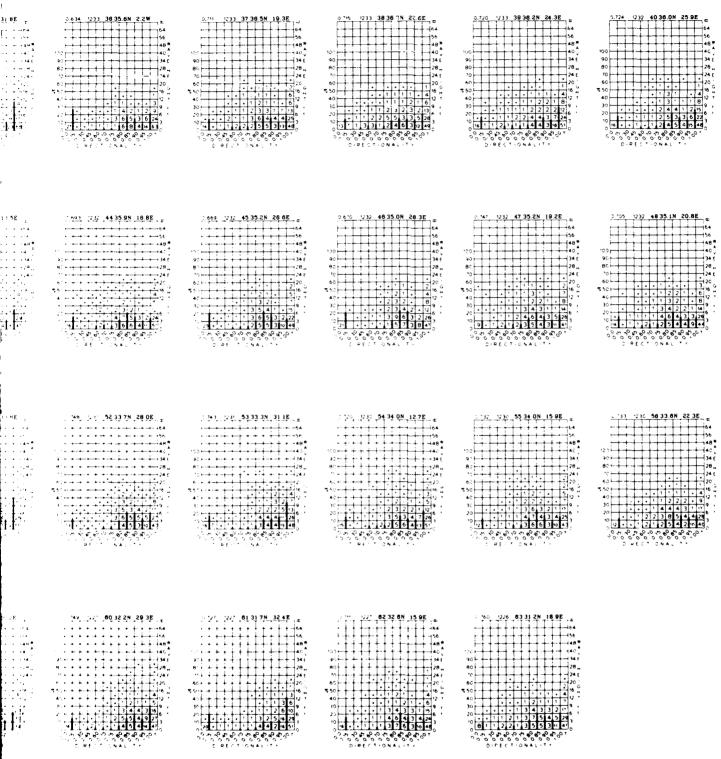


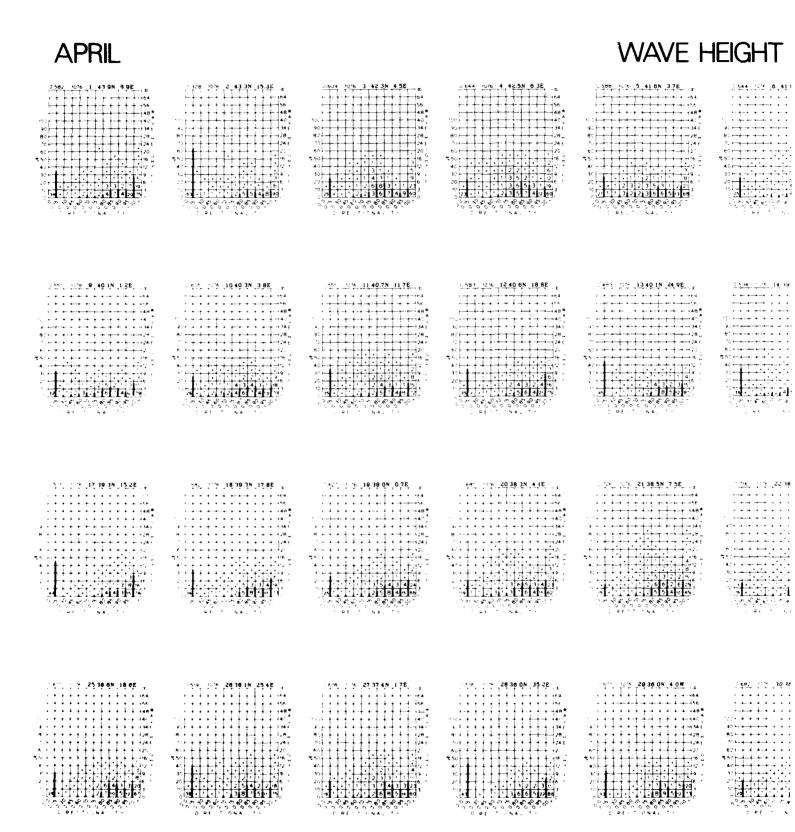
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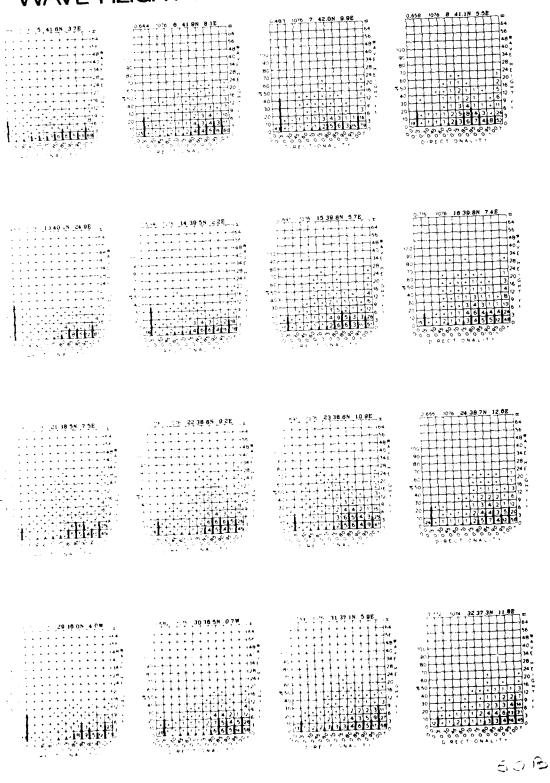


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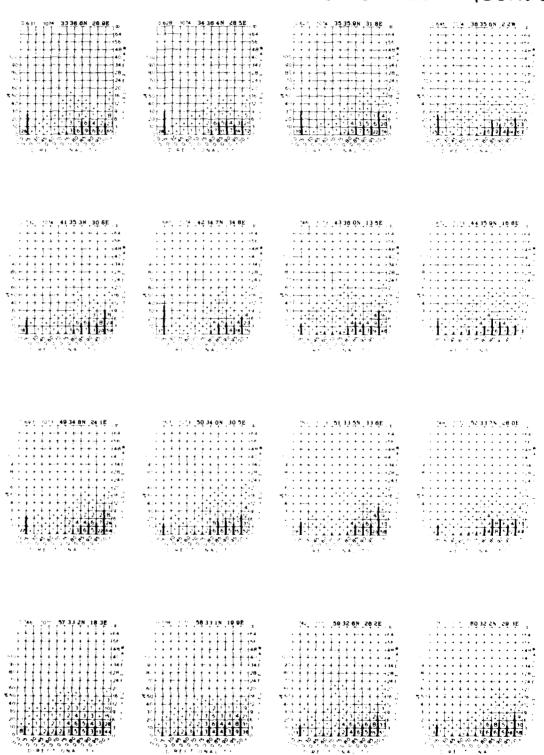
MARCH





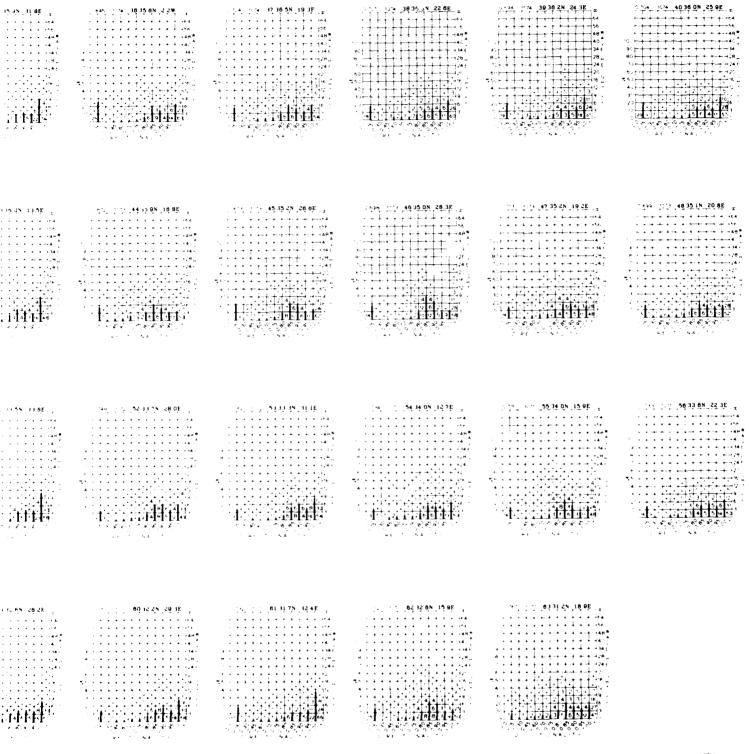


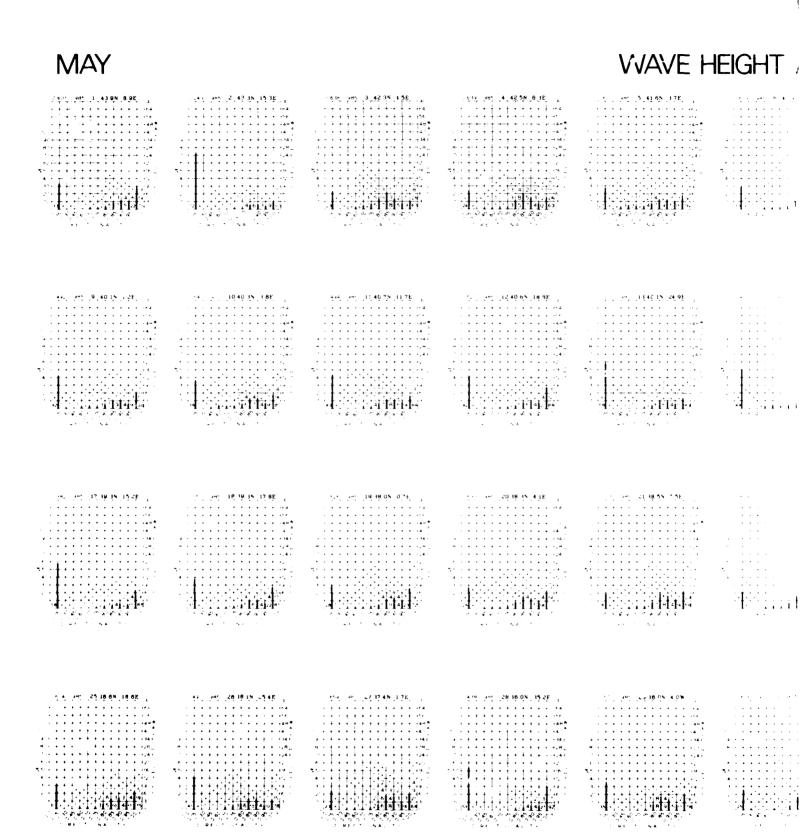
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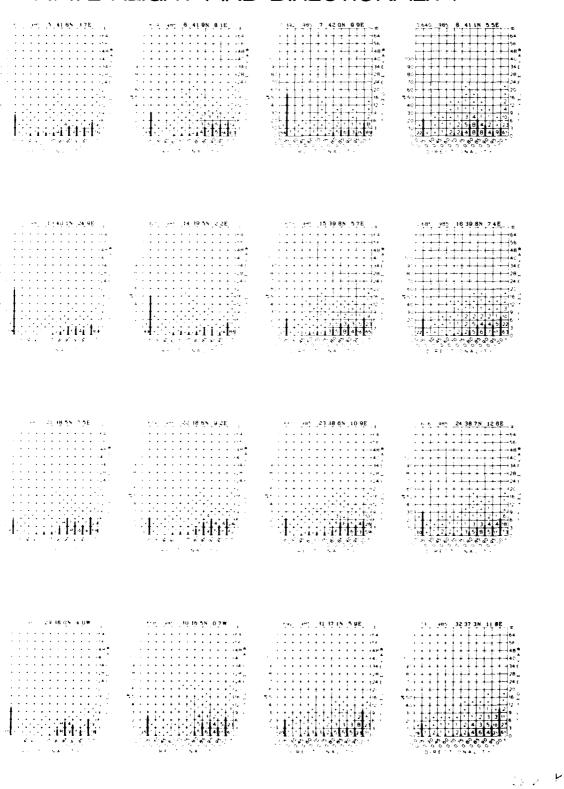


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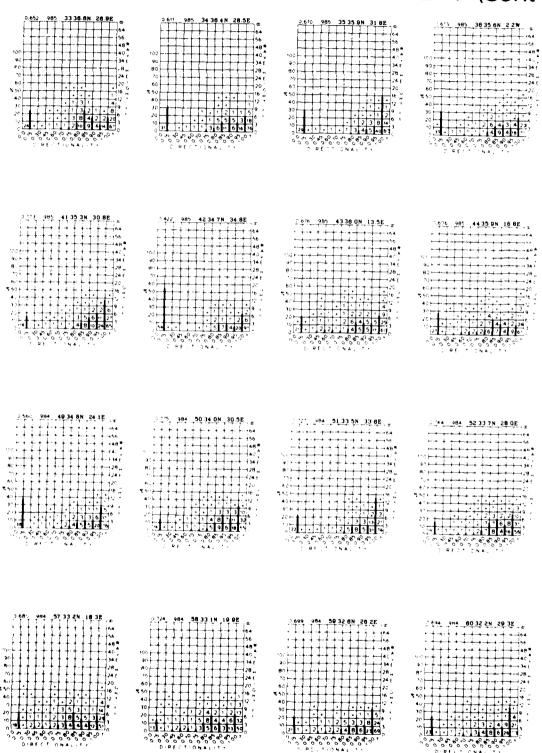
APRIL



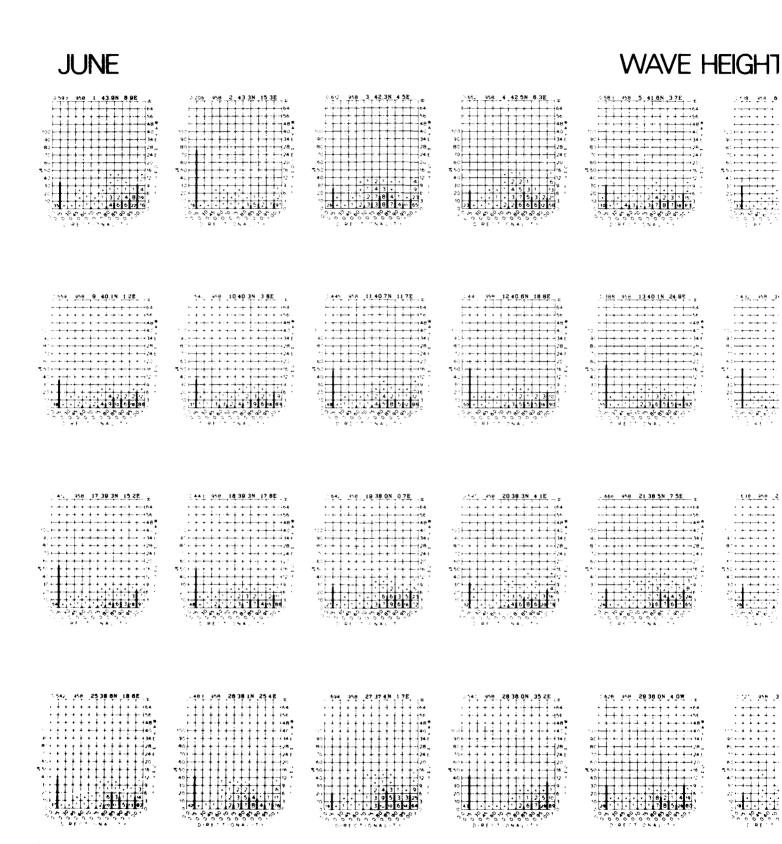




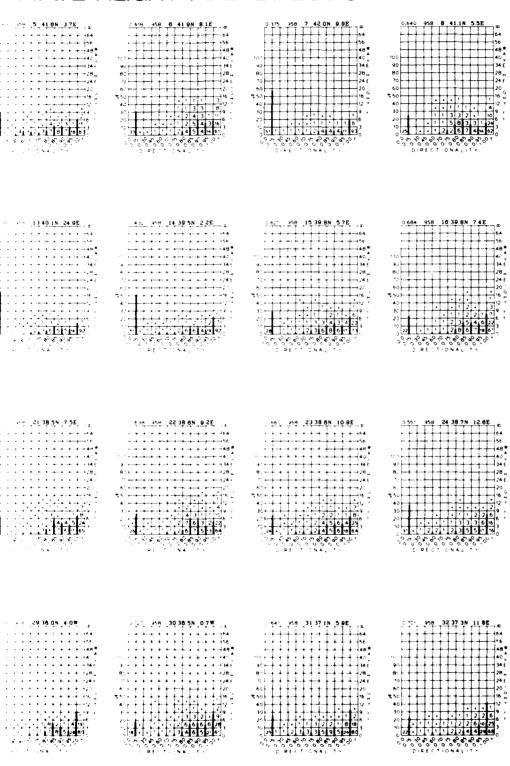
WAVE HEIGHT AND DIRECTIONALITY (Cont'



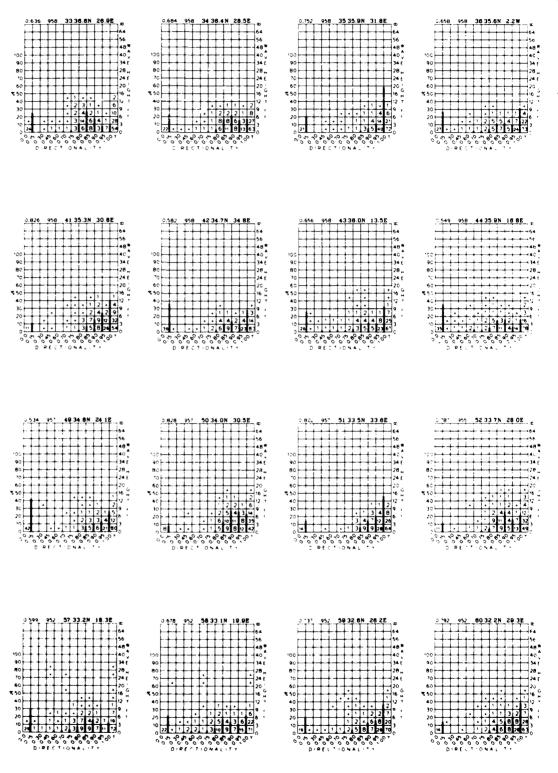
TIONALITY (Cont'd) MAY 7.50 - 1.12 | 1.18 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1.10 | 1. 48 4435 9N 18 8E , 644 38 '45 15 2N 28 8E , 64 1 16 UN 11 15 E



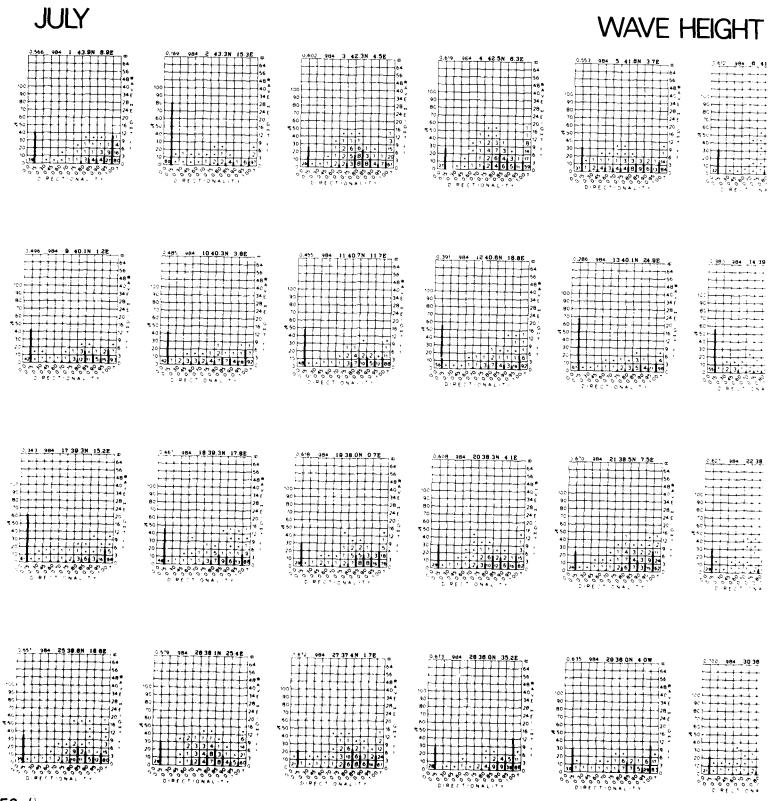
154 F



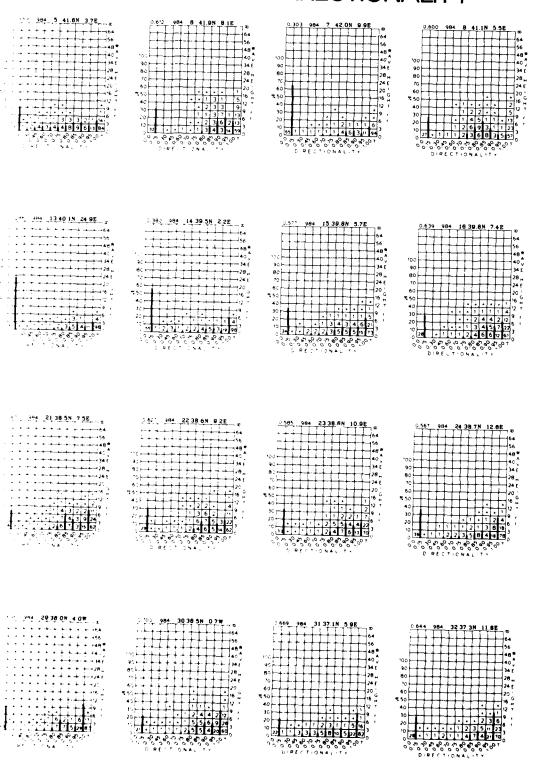
WAVE HEIGHT AND DIRECTIONALITY (Cont'd)



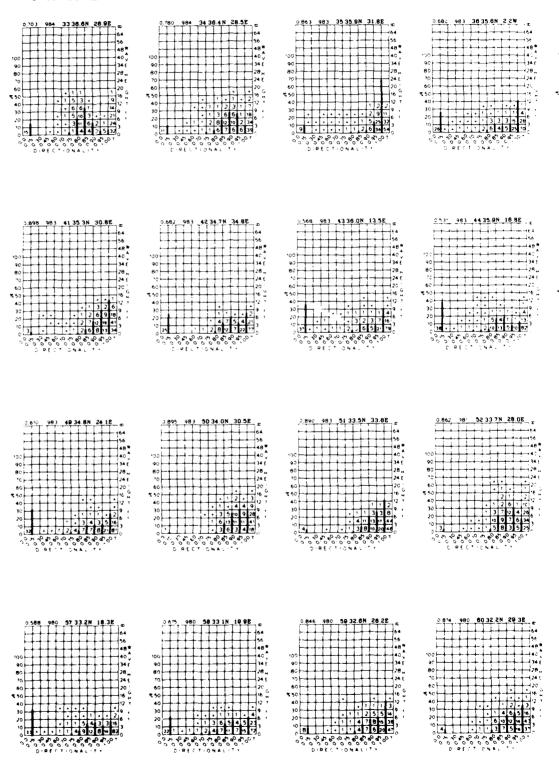
JUNF TIONALITY (Cont'd) 35 35 9N 31 BE 0 1 8 to 33 6E T



156 A



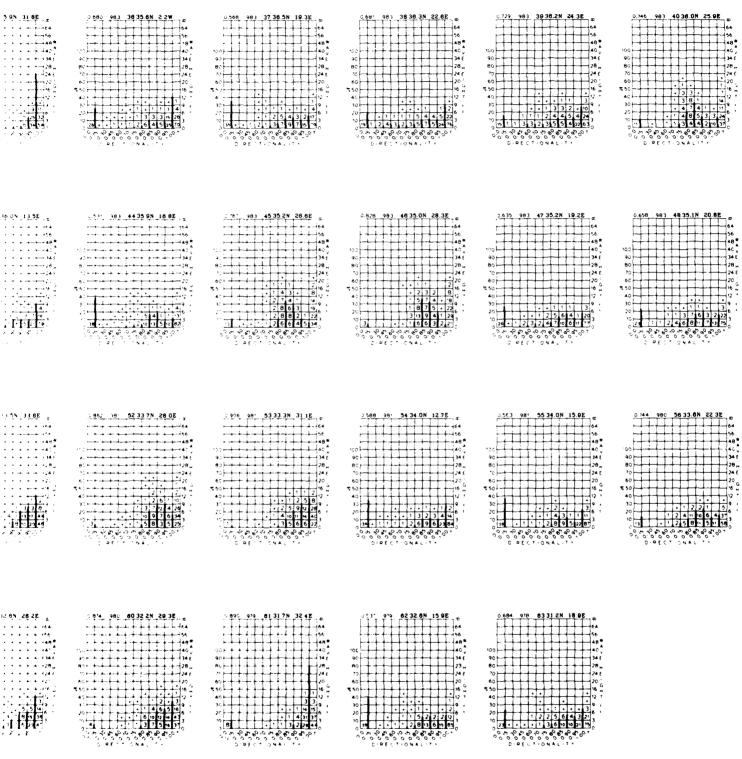
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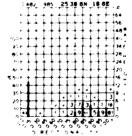
1340

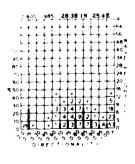
10NALITY (Cont'd)

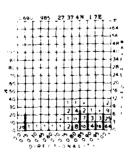


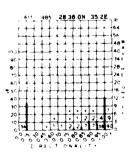


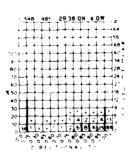
WAVE HEIGHT **AUGUST** 481 985 5 41 6N 37E 316 985 1340.IN 24.0E 9.395 985 14 79 0.345 985 12 40.6N 18.8E 0.41, 285 18 38 3N 17.8E 102 have done as a

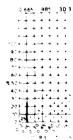




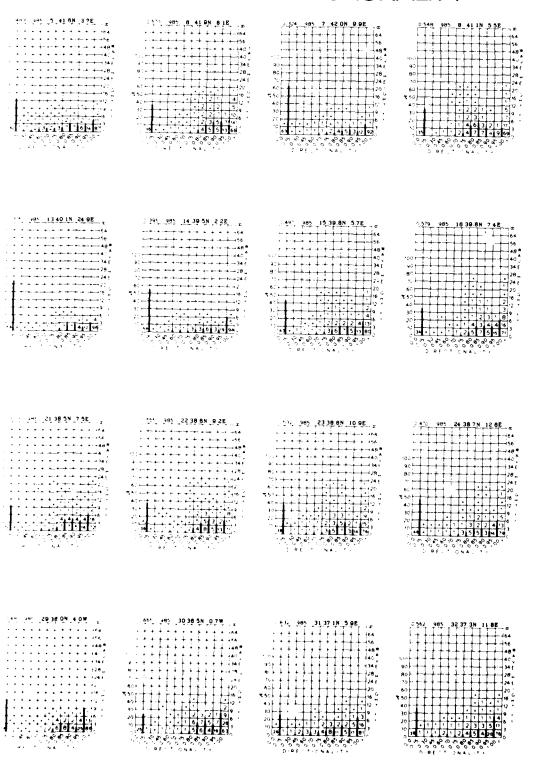




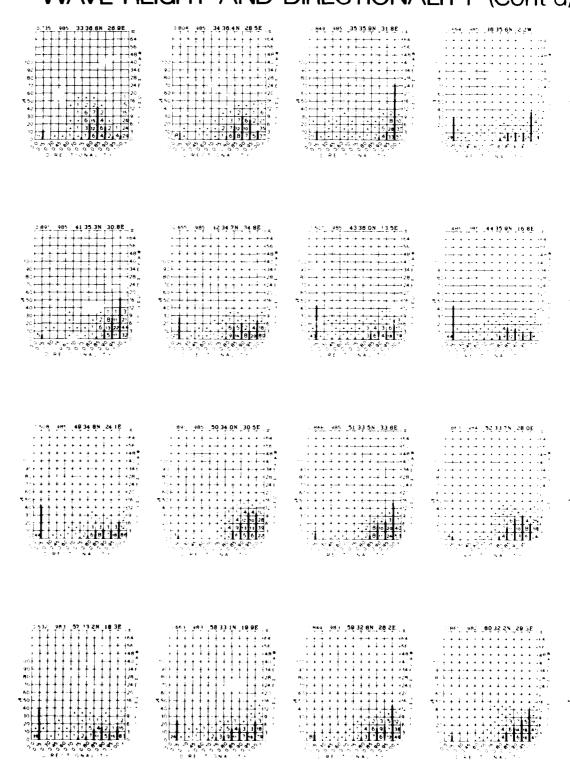




158 F



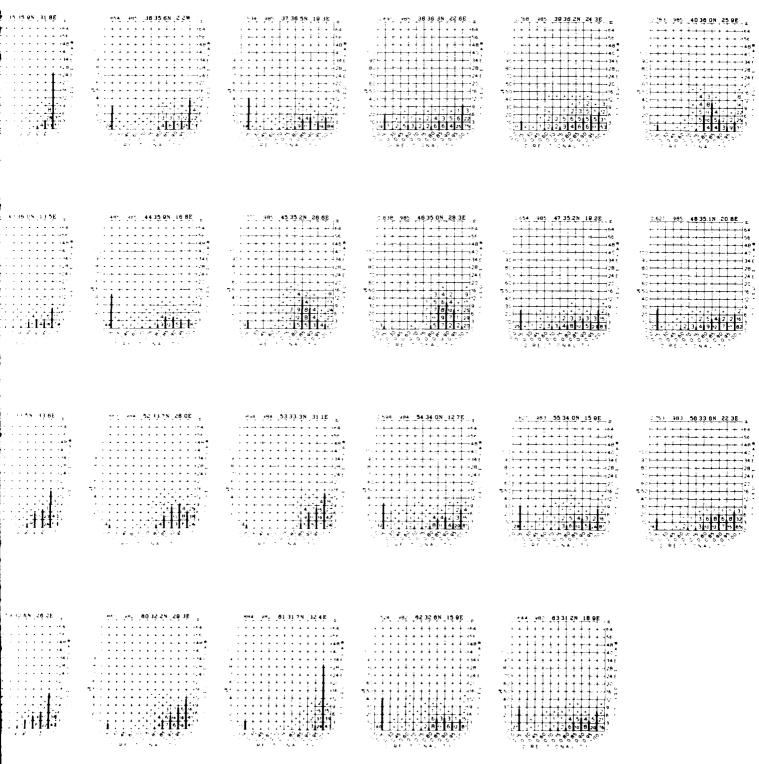
WAVE HEIGHT AND DIRECTIONALITY (Cont'd)



1500 1

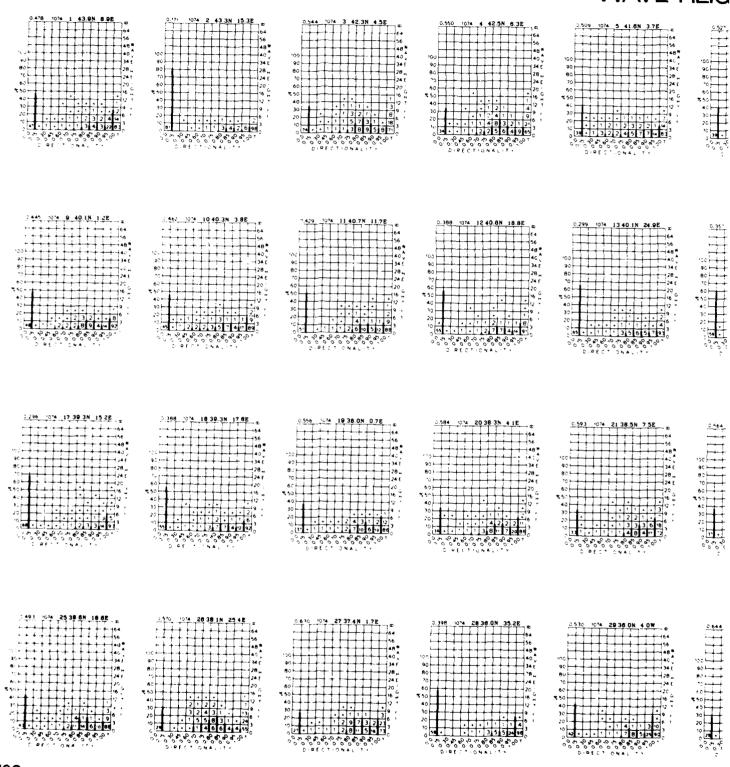
ETIONALITY (Cont'd)

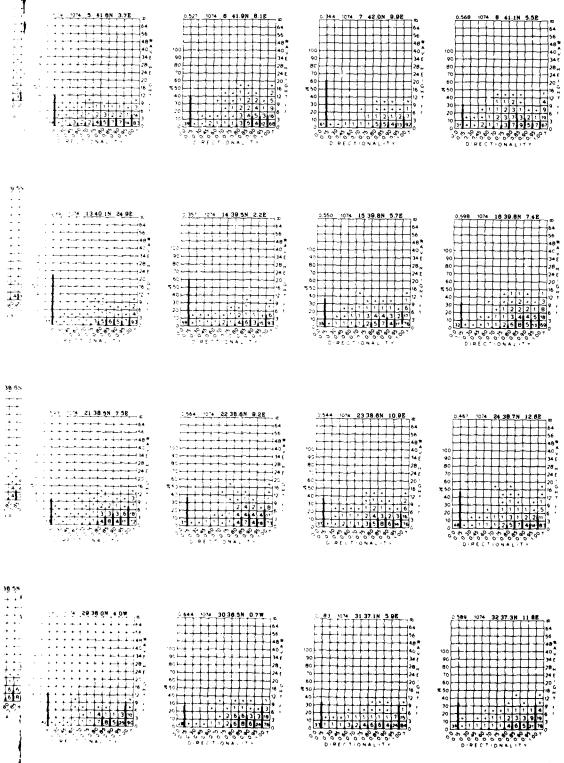
AUGUST



SEPTEMBER

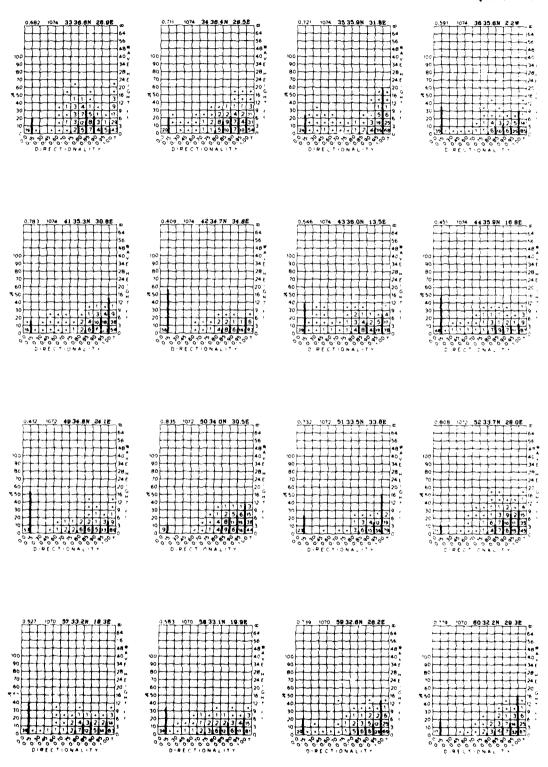
WAVE HEIG





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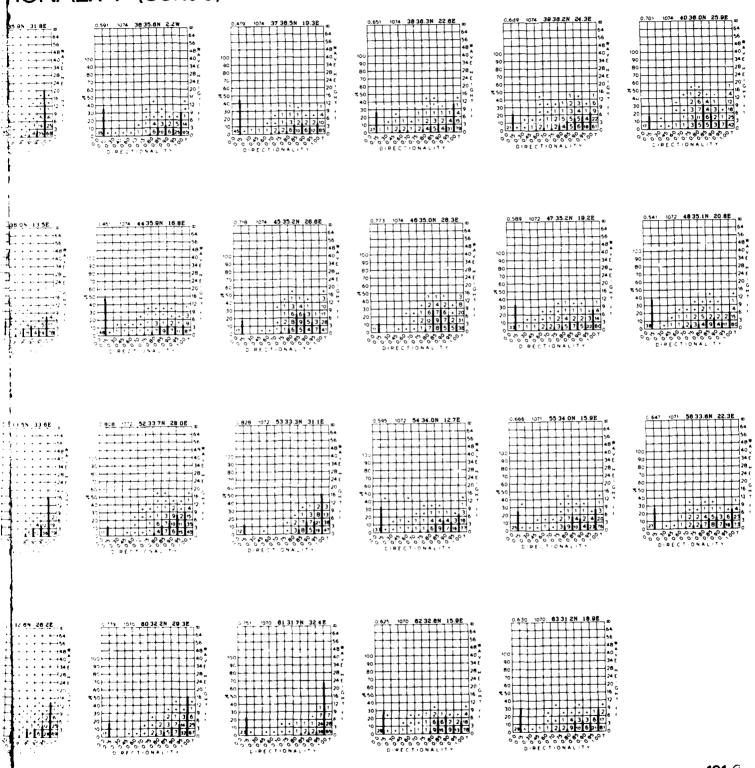


16:1

The Review of States of Company and

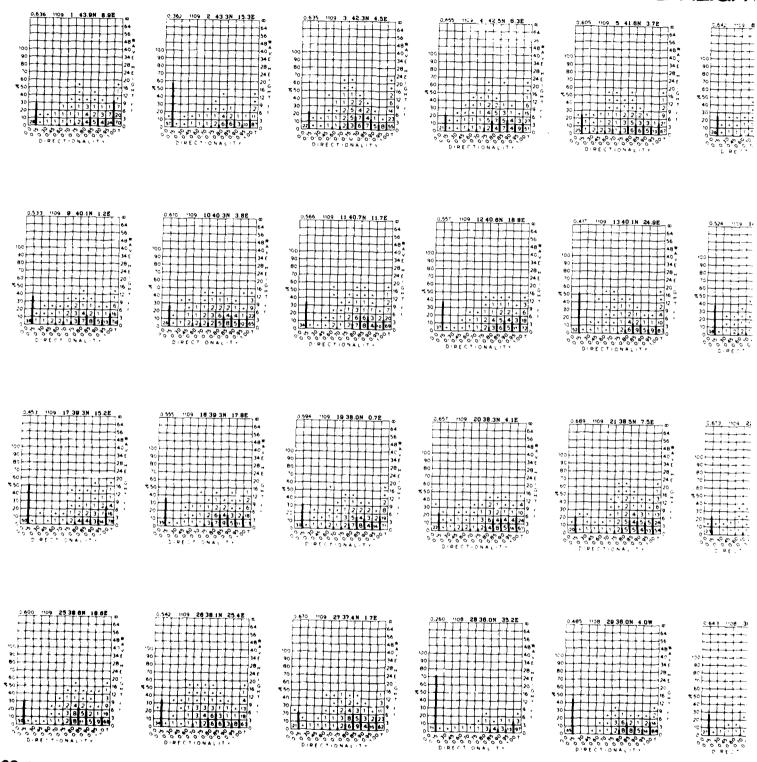
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SEPTEMBER

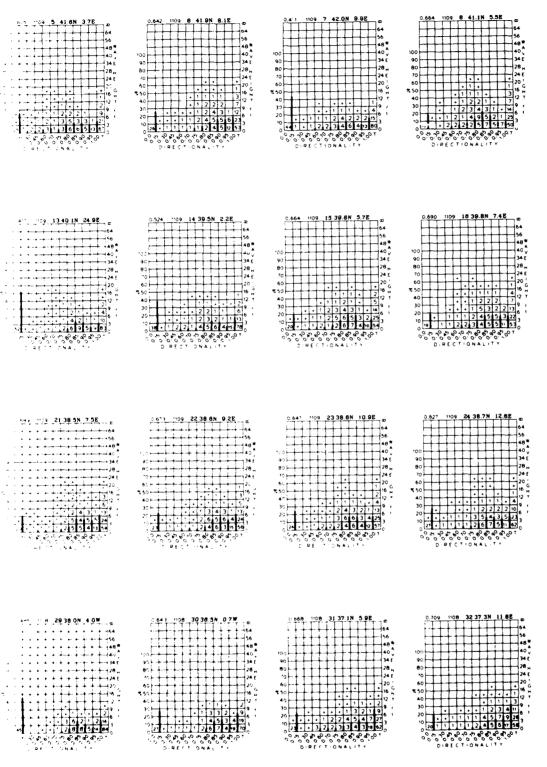


OCTOBER

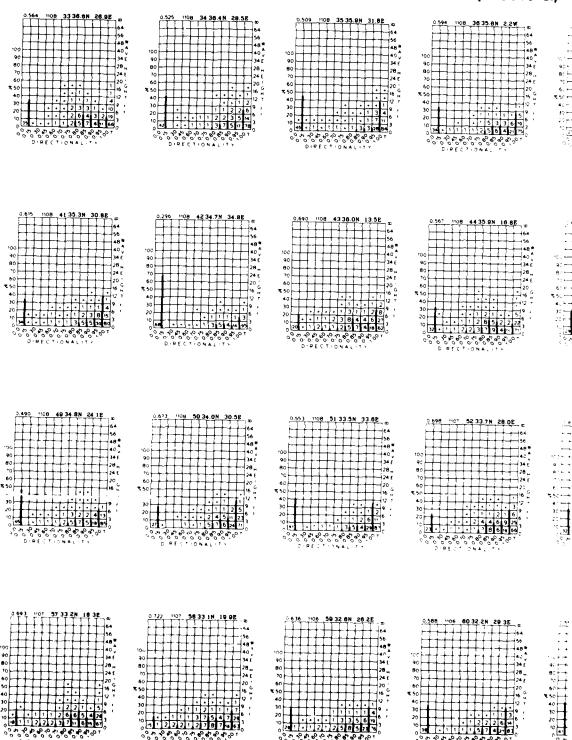
WAVE HEIGHT



162 A



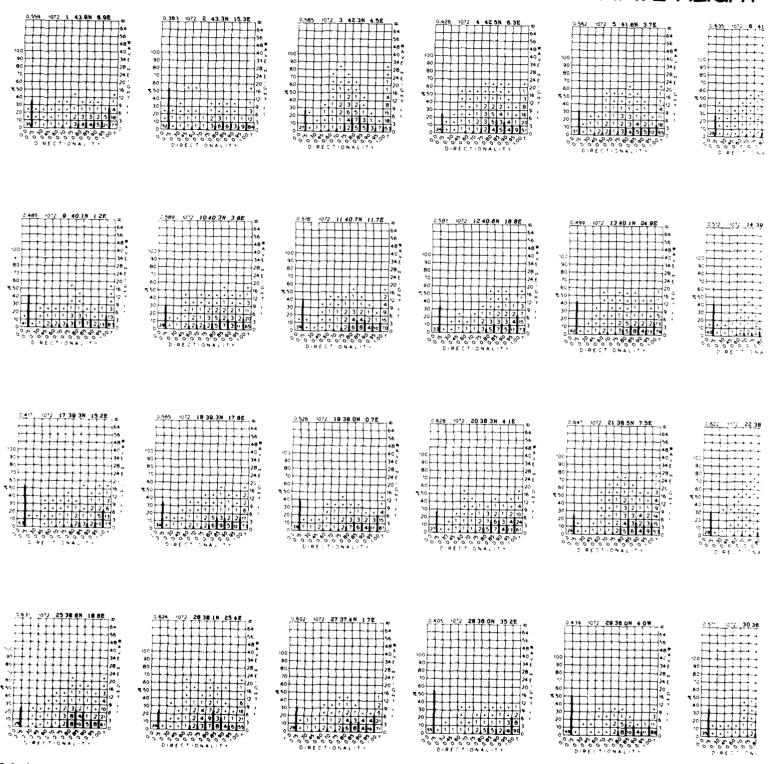
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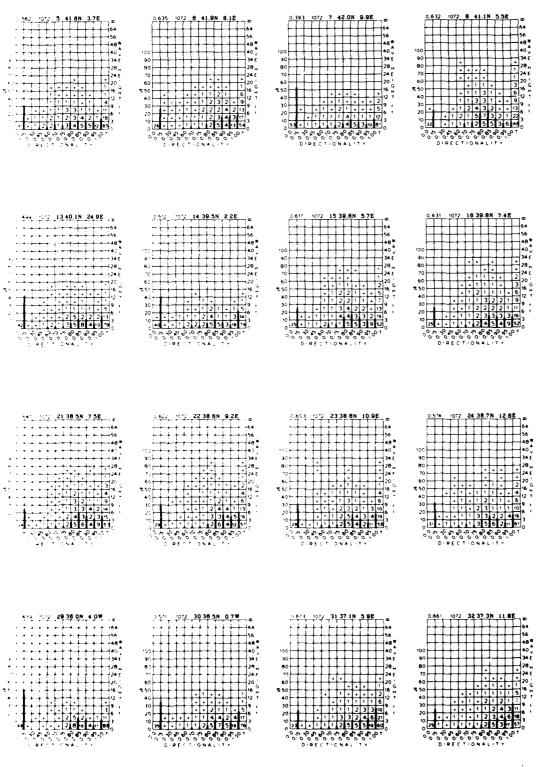


OCTOBER ONALITY (Cont'd) # JI 08 % 1 31 8E . E C.649 107 54 34 0N 12.78 p 25 33 7N 28 0F 48 4 48 PN 338E Harman 6N 28 28

NOVEMBER

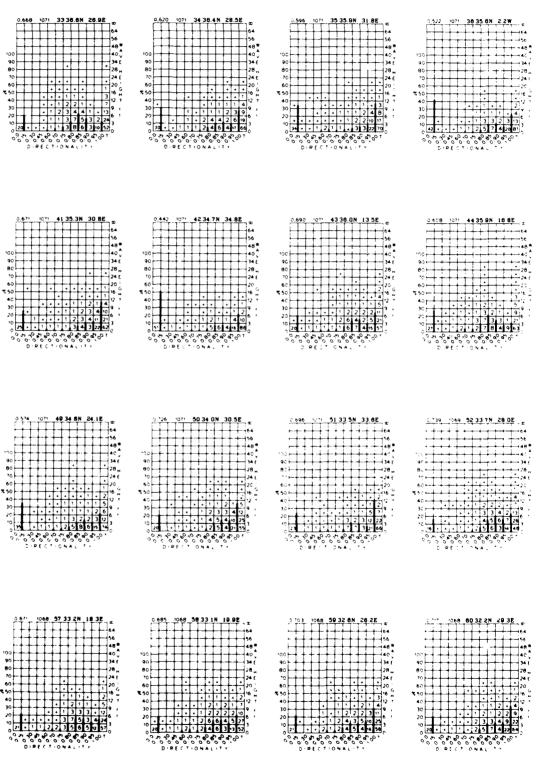
WAVE HEIGHT





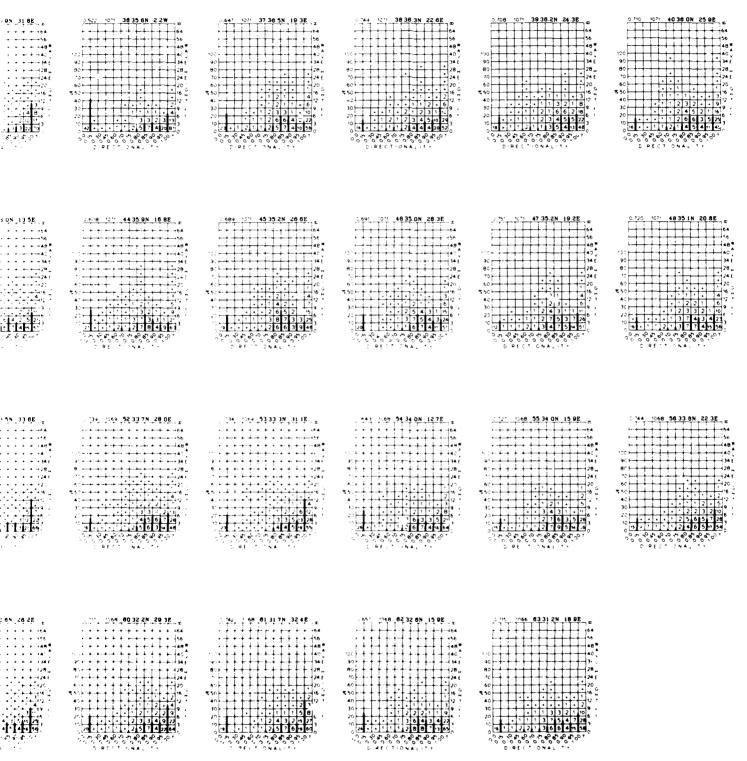
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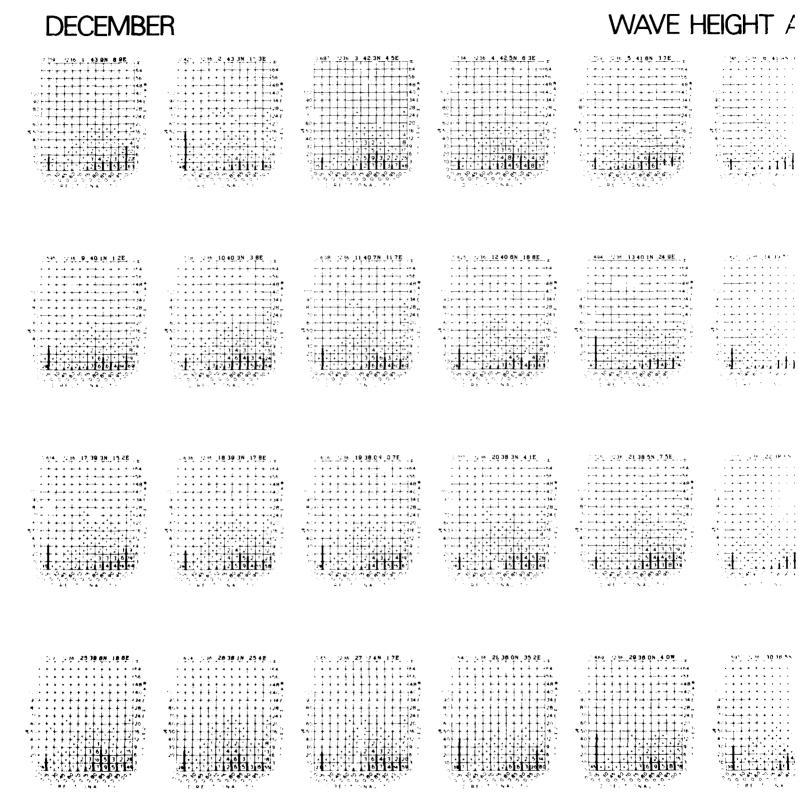
WAVE HEIGHT AND DIRECTIONALITY (Cont'd)



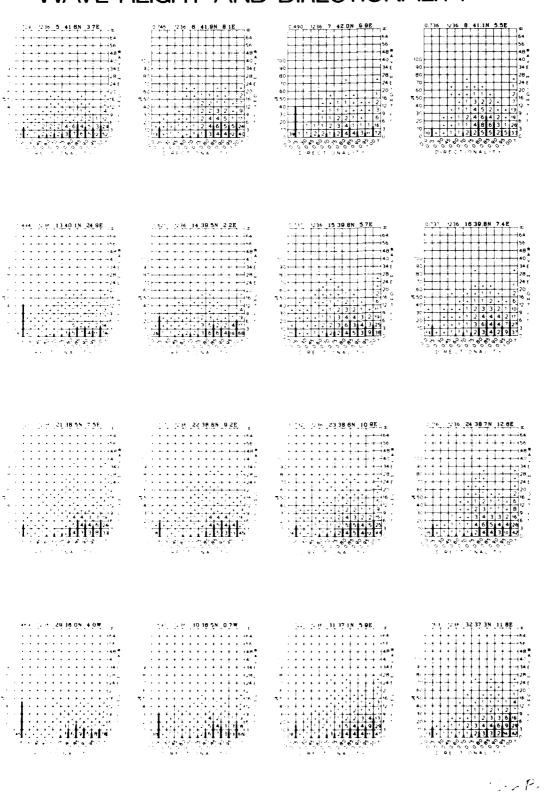
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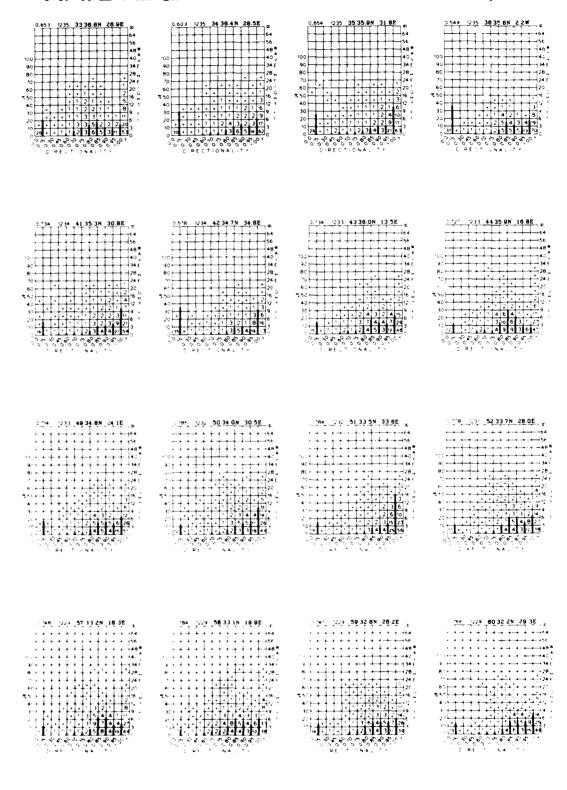




166 🖰

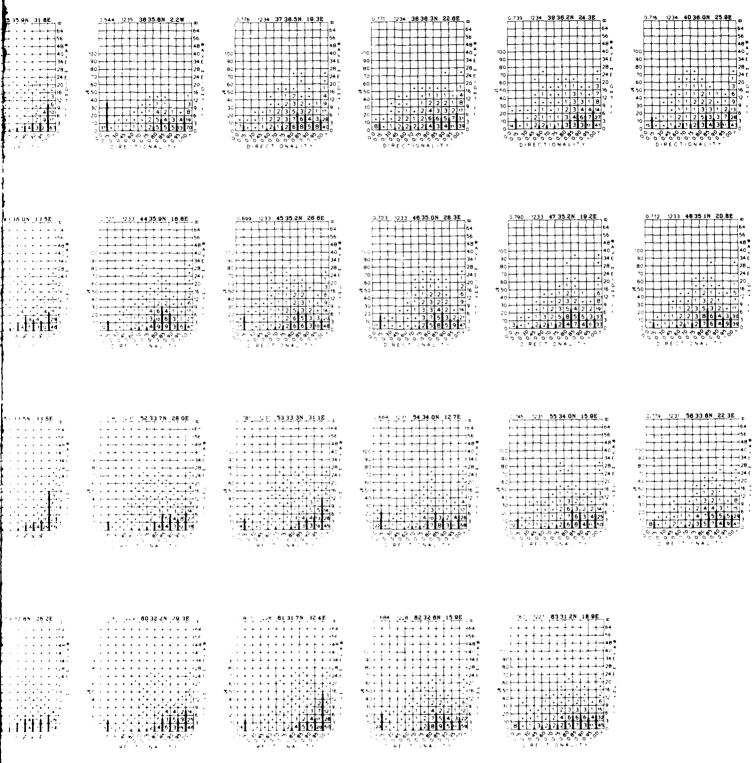


WAVE HEIGHT AND DIRECTIONALITY (Cont'd



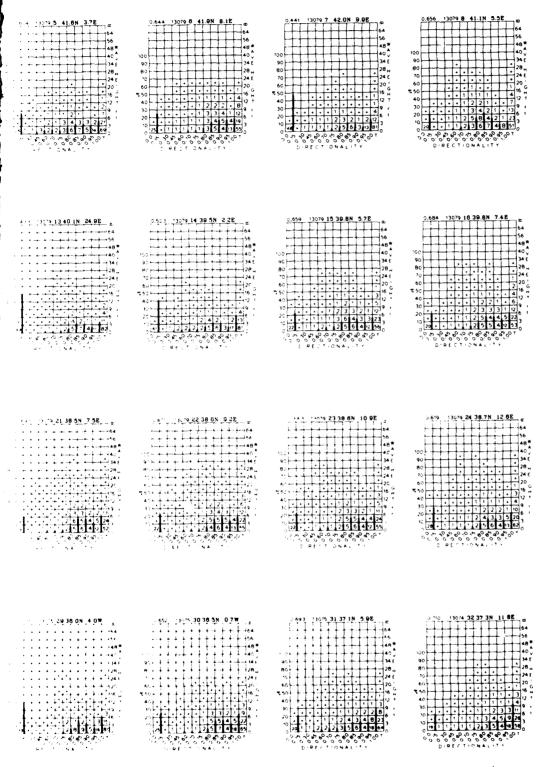
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DECEMBER

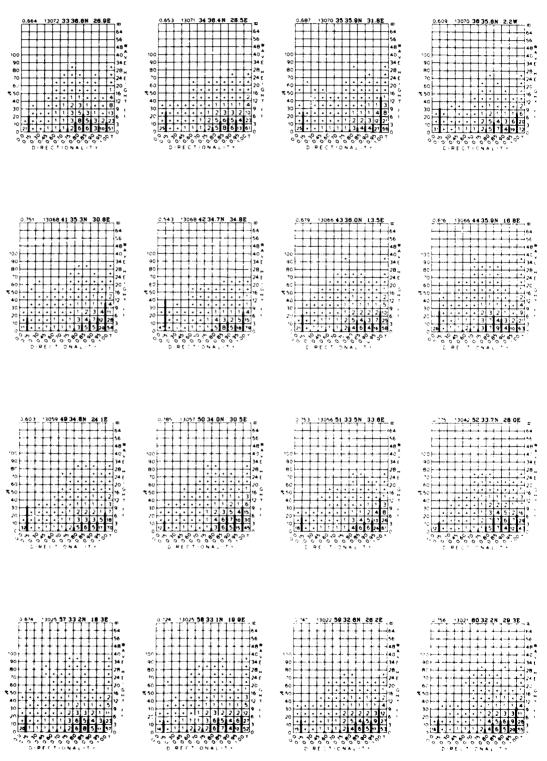


ANNUAL WAVE HEIGHT 2537 3070 10 40 3N 3.8P 640 1N 1.2P 55 10 40 3N 3.8P 640 1N 1.2P 55 10 40 3N 3.8P 640 1N 1.2P 641 1N 1 <u>0.503 (13079-1</u> 90 100 20 30 6N 10 6E

WAVE HEIGHT AND DIRECTIONALITY



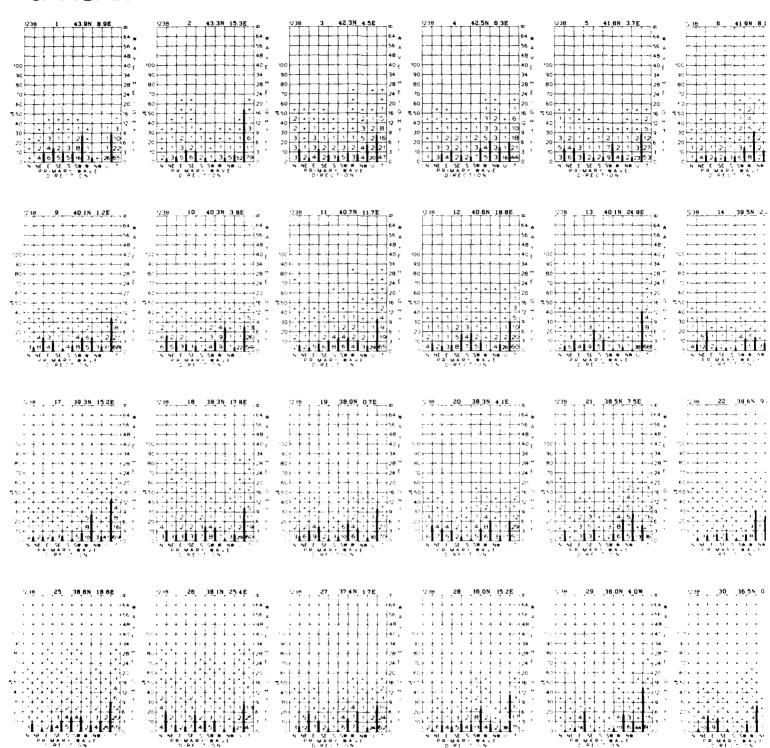
WAVE HEIGHT AND DIRECTIONALITY (Cont'd)



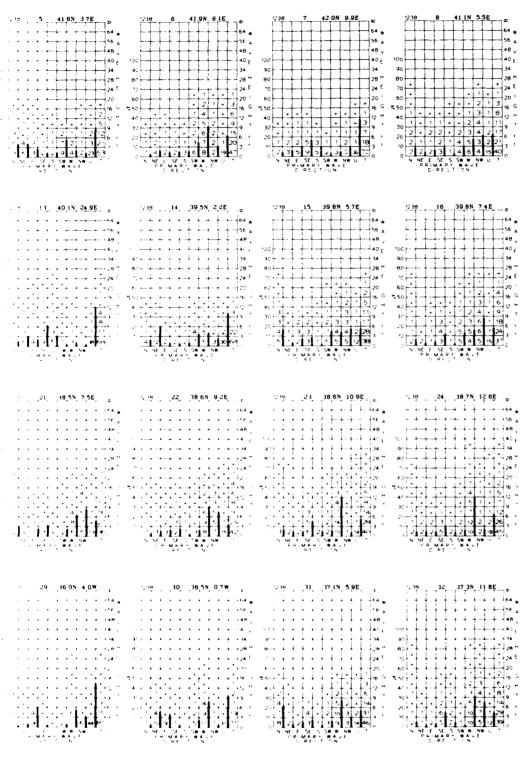
NALITY (Cont'd) **ANNUAL** 1009 61 31 7N 32 4E 7 1009 61 7009 61

JANUARY

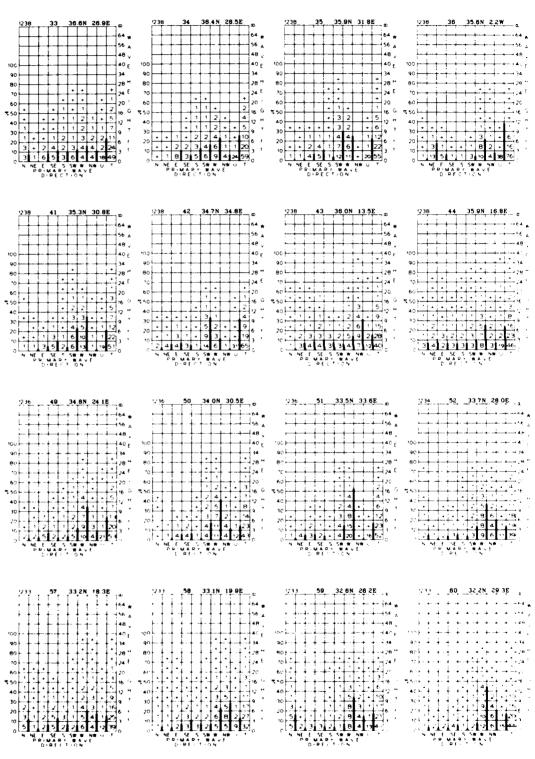
WAVE HEIGHT AND PRIMA



HEIGHT AND PRIMARY WAVE DIRECTION

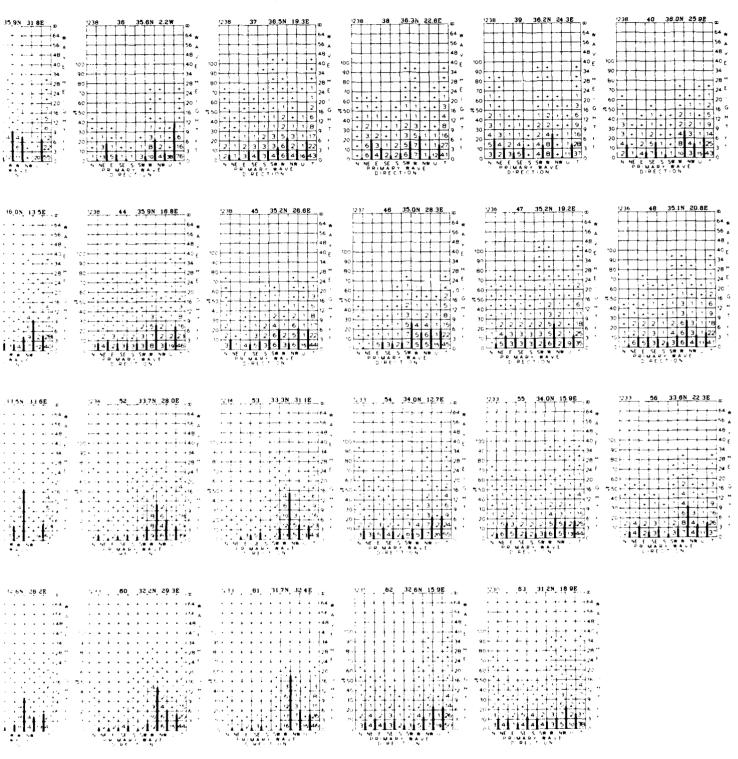


WAVE HEIGHT AND PRIMARY WAVE DIRECT



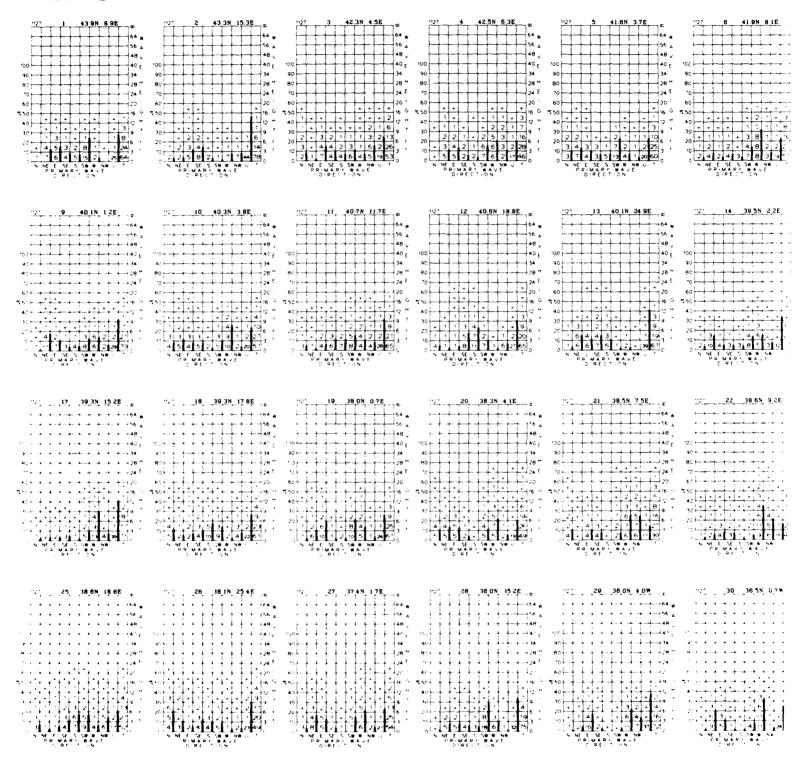
LRY WAVE DIRECTION (Cont'd)

JANUARY

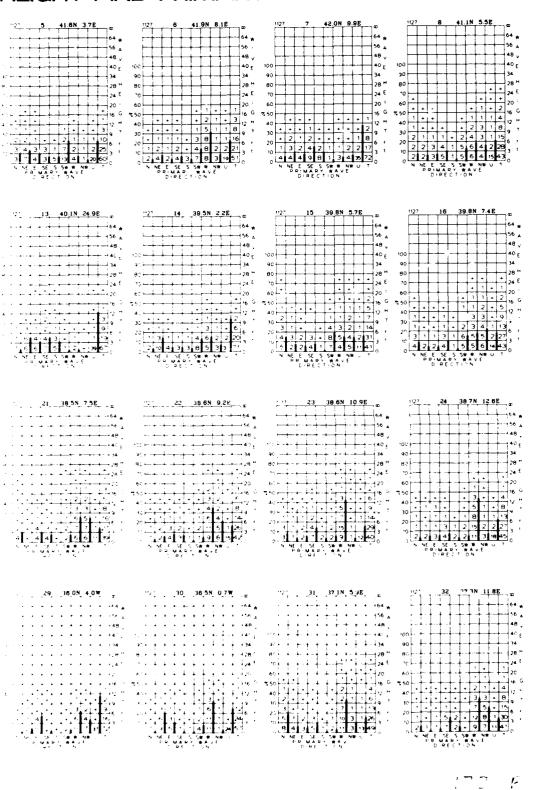


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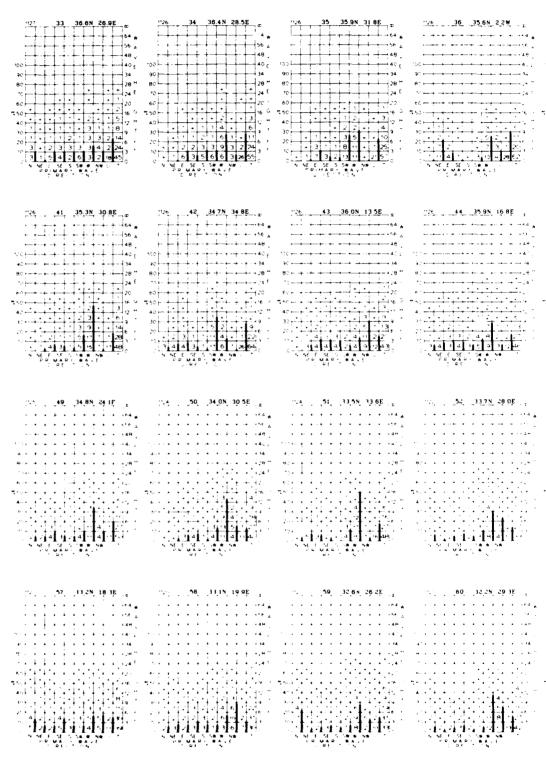
WAVE HEIGHT AND PRIMAF



HEIGHT AND PRIMARY WAVE DIRECTION

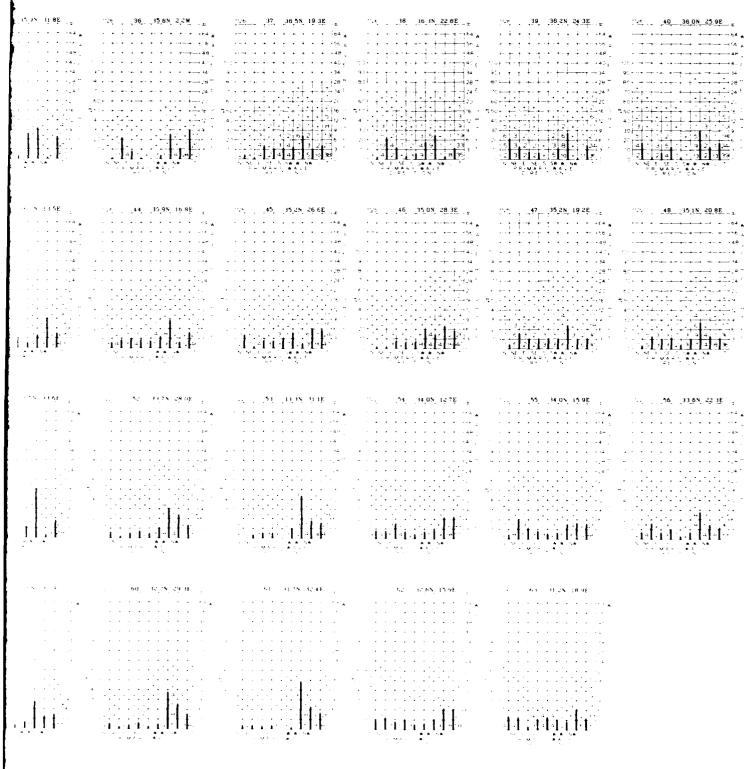


WAVE HEIGHT AND PRIMARY WAVE DIRECTIC



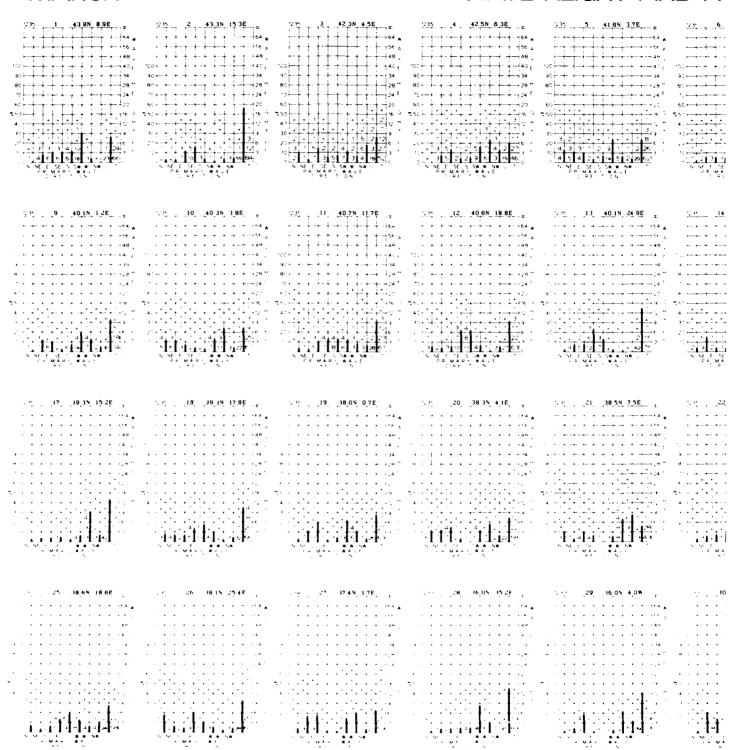
ARY WAVE DIRECTION (Cont'd)

FEBRUARY

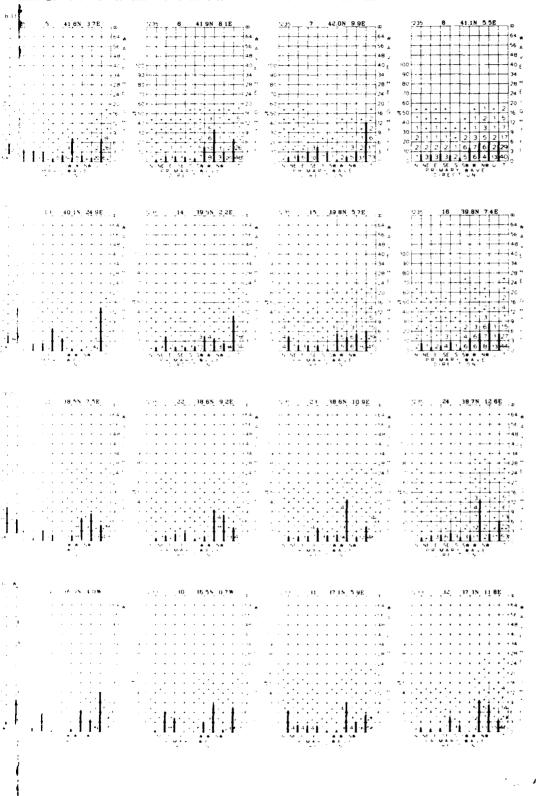


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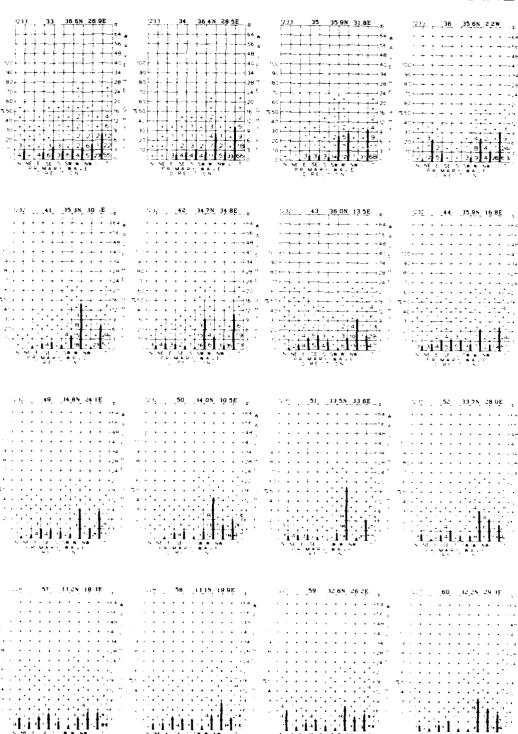
WAVE HEIGHT AND PF



AEIGHT AND PRIMARY WAVE DIRECTION

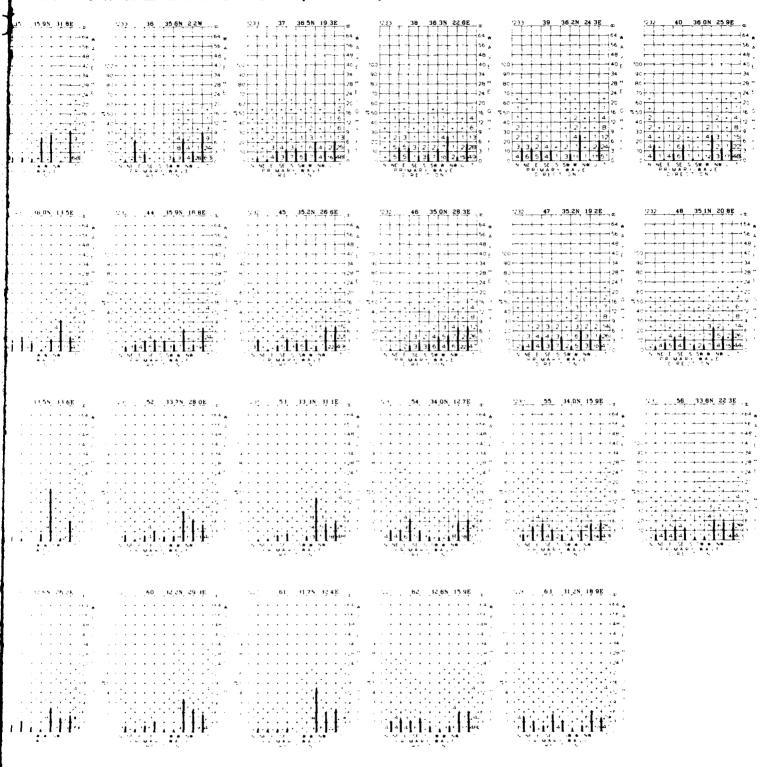


WAVE HEIGHT AND PRIMARY WAVE DIREC



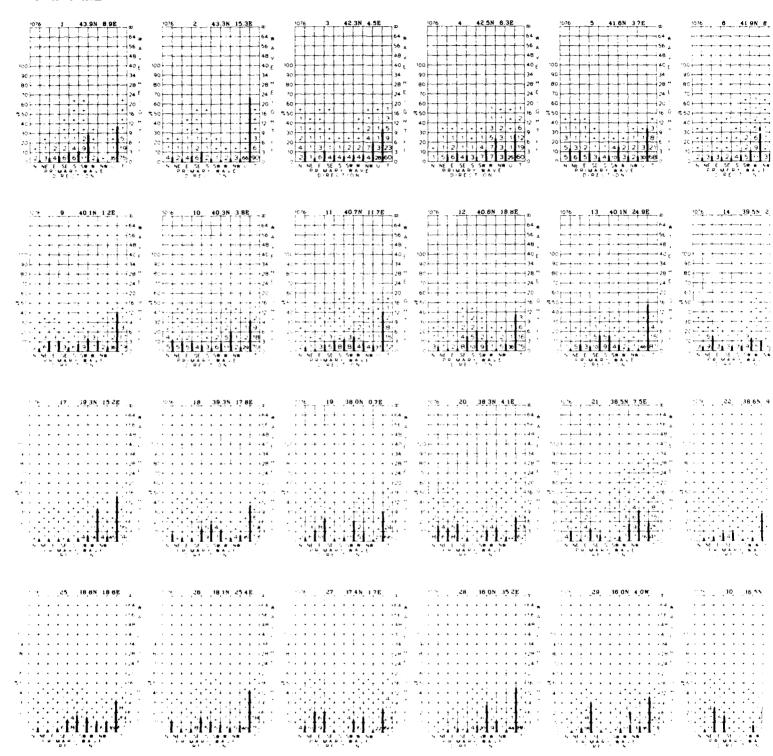
JARY WAVE DIRECTION (Cont'd)

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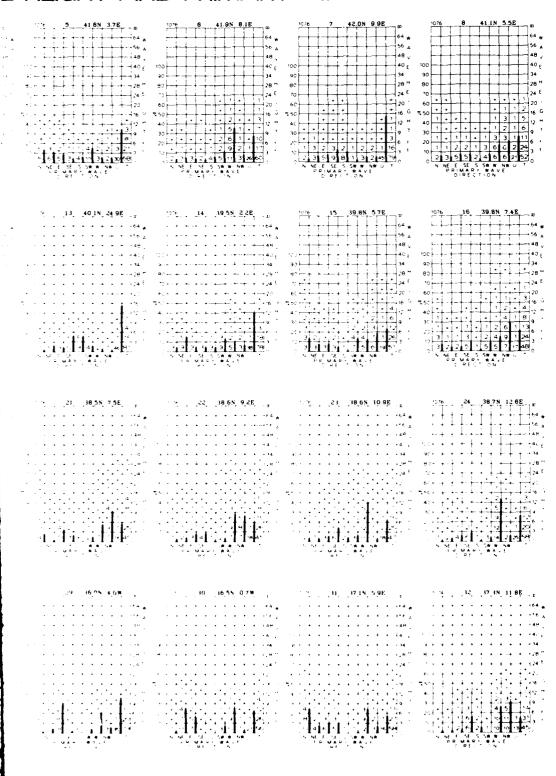


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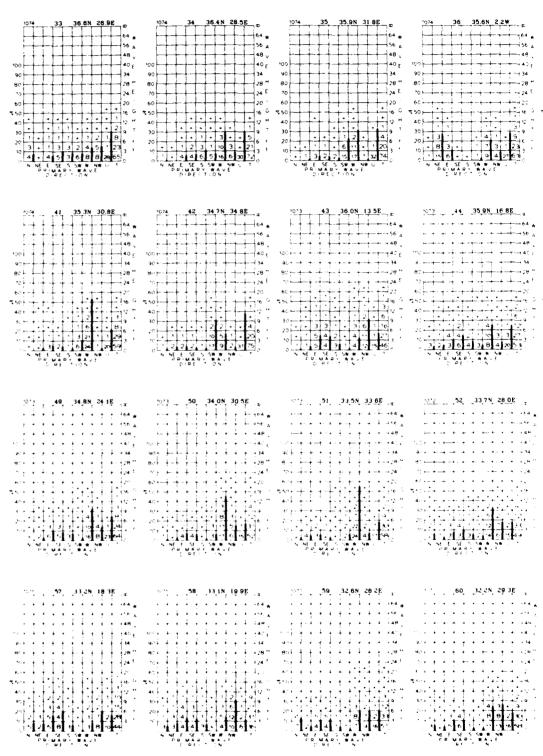
WAVE HEIGHT AND PRIMA



E HEIGHT AND PRIMARY WAVE DIRECTION

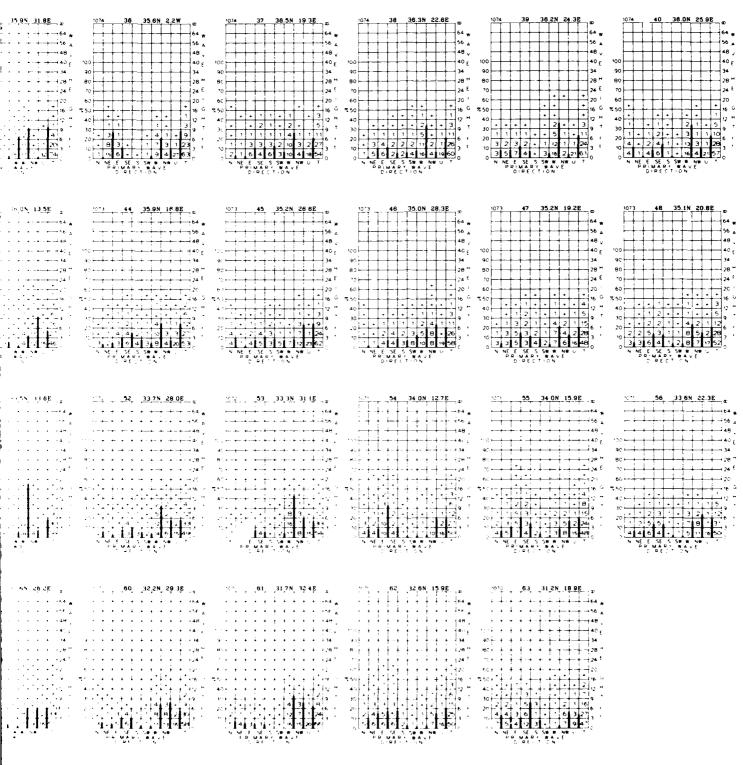


WAVE HEIGHT AND PRIMARY WAVE DIRECT



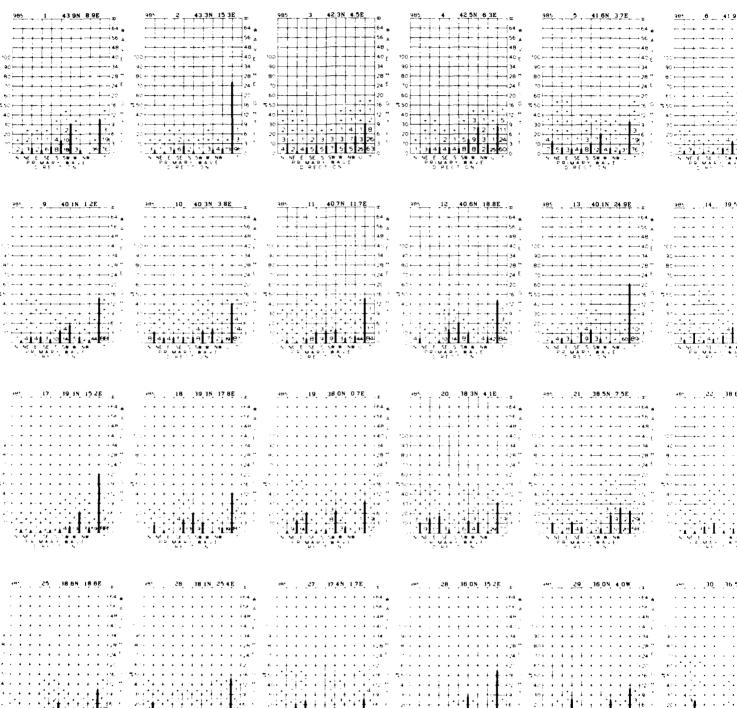
ARY WAVE DIRECTION (Cont'd)

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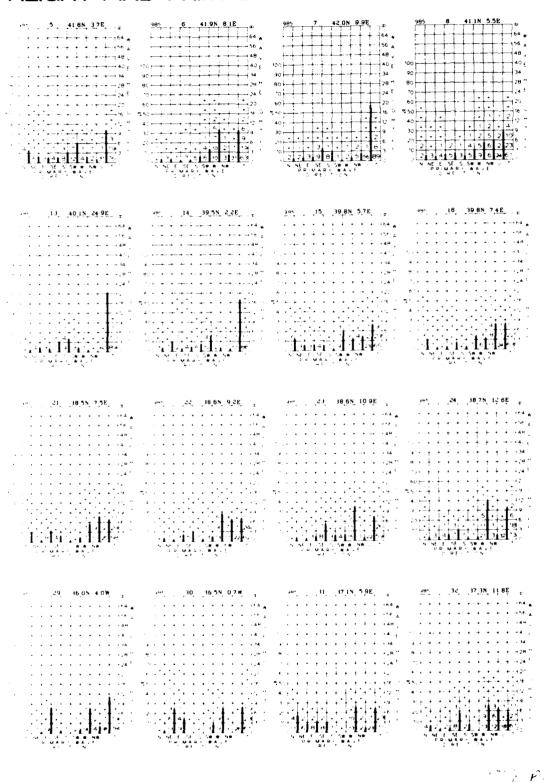


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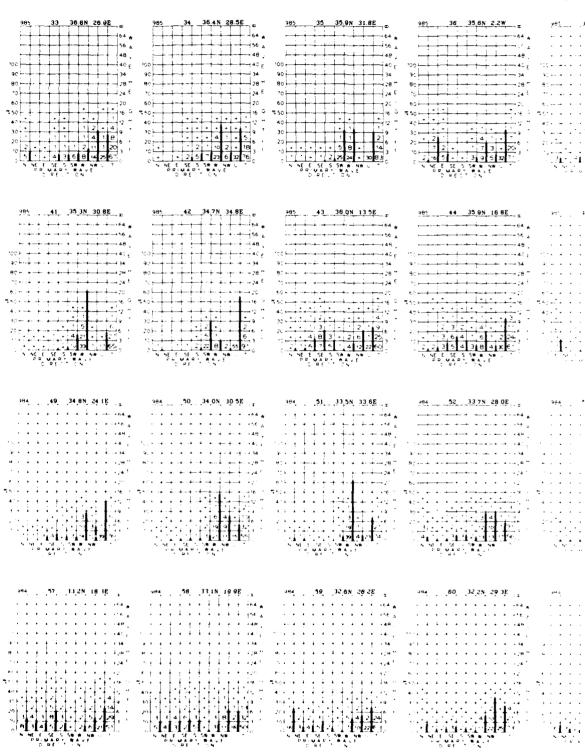
WAVE HEIGHT AND PRIN



HEIGHT AND PRIMARY WAVE DIRECTION

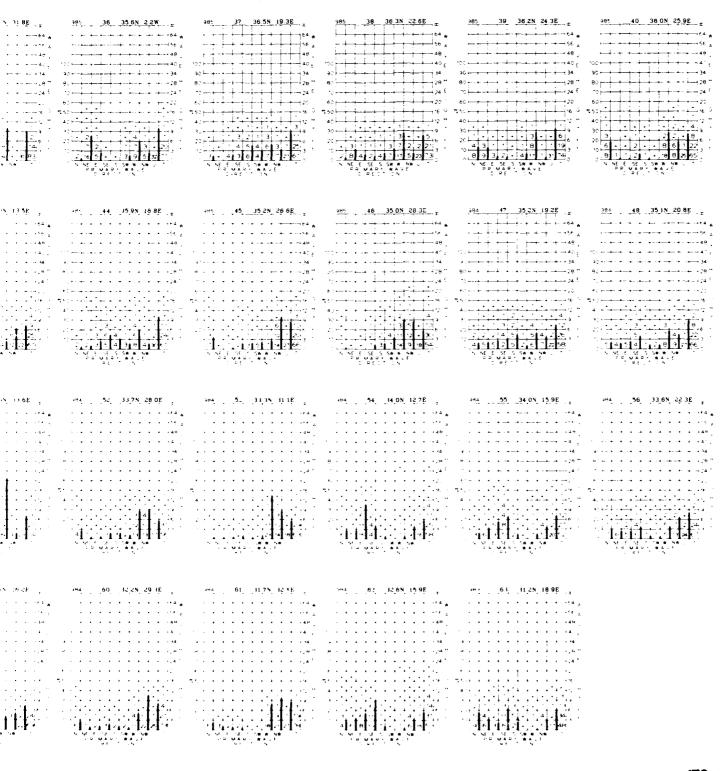


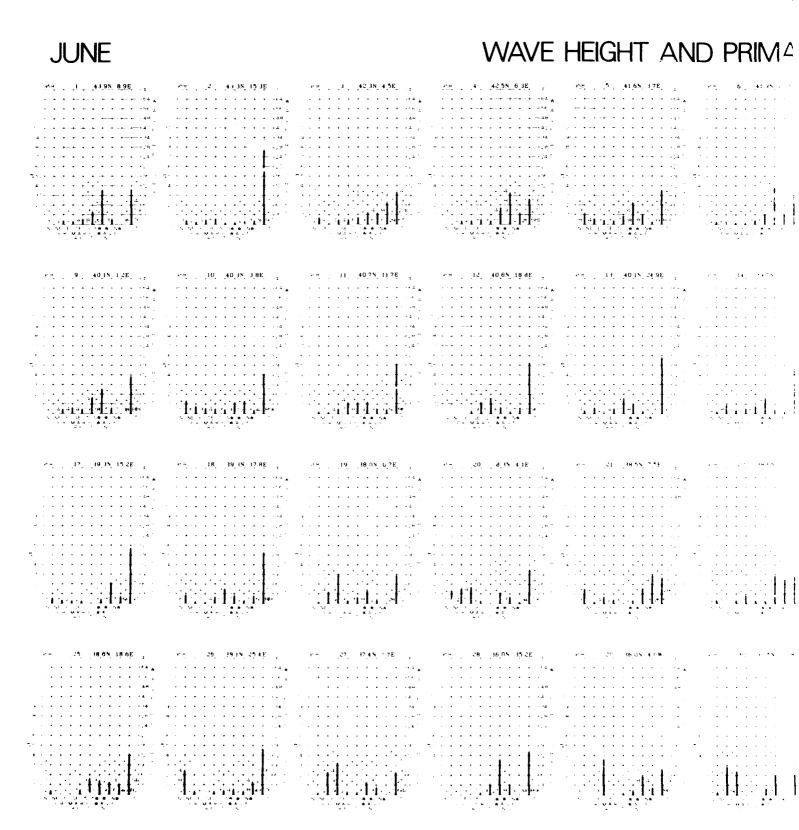
WAVE HEIGHT AND PRIMARY WAVE DIRECTION



RY WAVE DIRECTION (Cont'd)

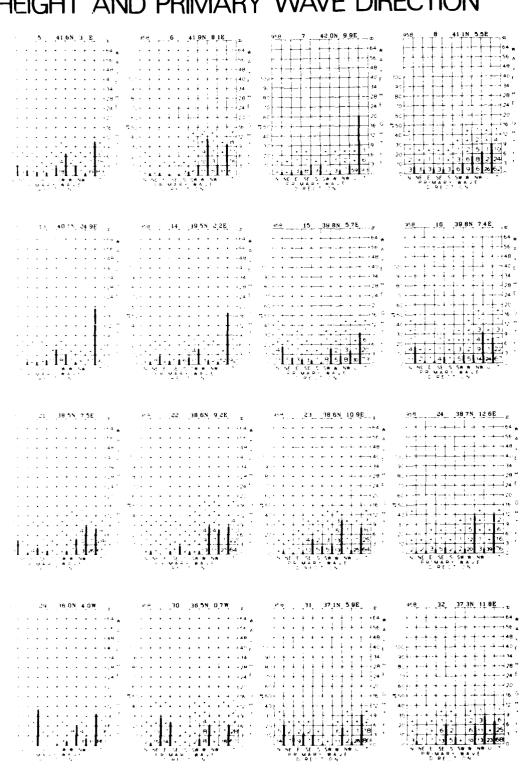
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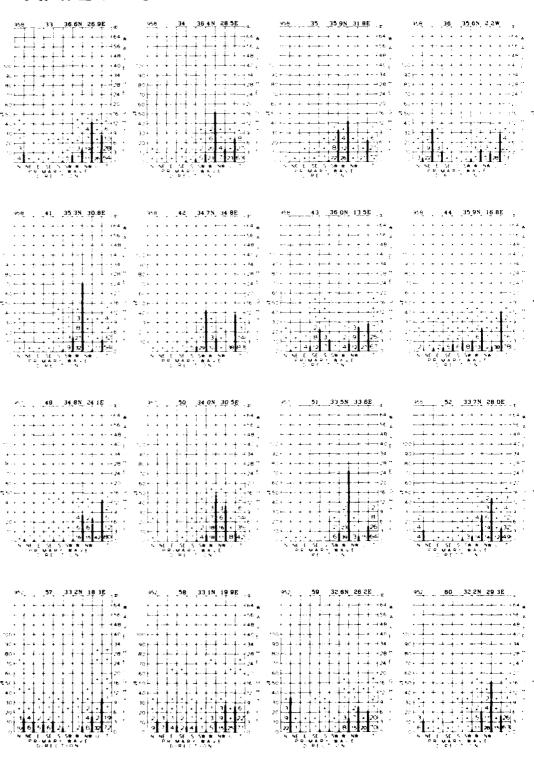


180 A

HEIGHT AND PRIMARY WAVE DIRECTION

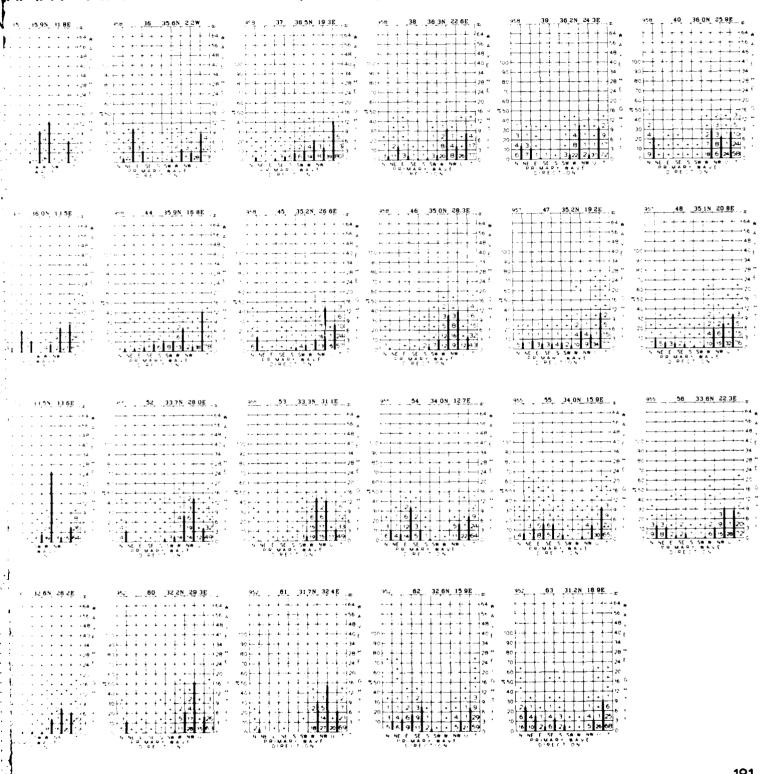


WAVE HEIGHT AND PRIMARY WAVE DIRECT



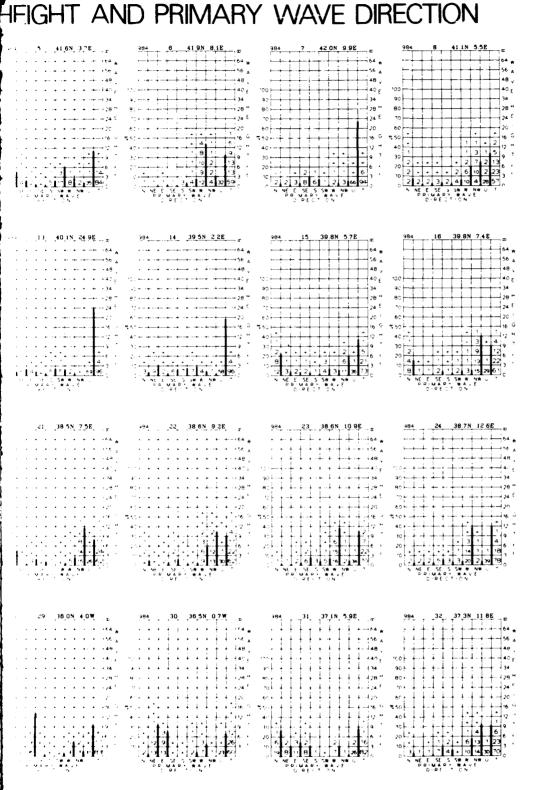
MARY WAVE DIRECTION (Cont'd)

JUNE

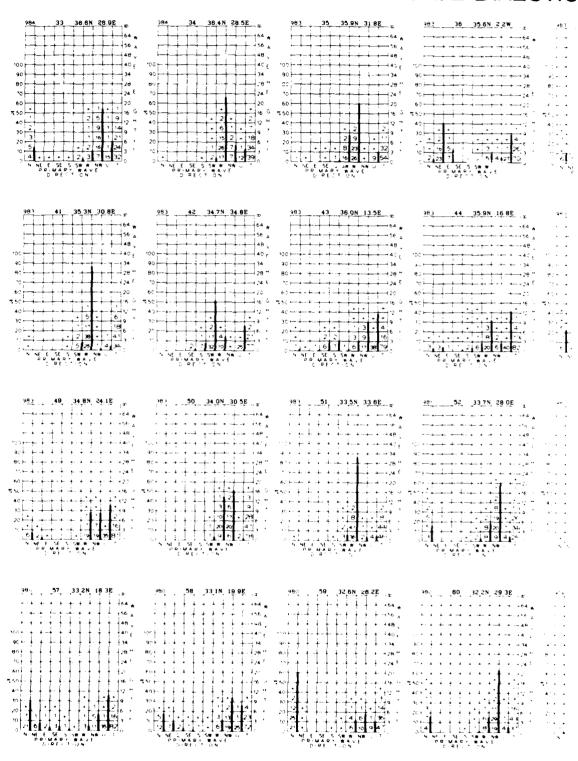


JULY WAVE HEIGHT AND PRIMA 984 5 41.6N 3.7E 984 6 41.9N 8 984 1 43 9N 8 9E 994 2 43 3N 15 3E 50 44 48 48 48 , 40 ₆ 984 10 40 3N 3.8E 984 11 40.7N 11.7E 984 12 40.6N 18.8E 984 13 40.6N 18.8E 984 12 40.6N 1

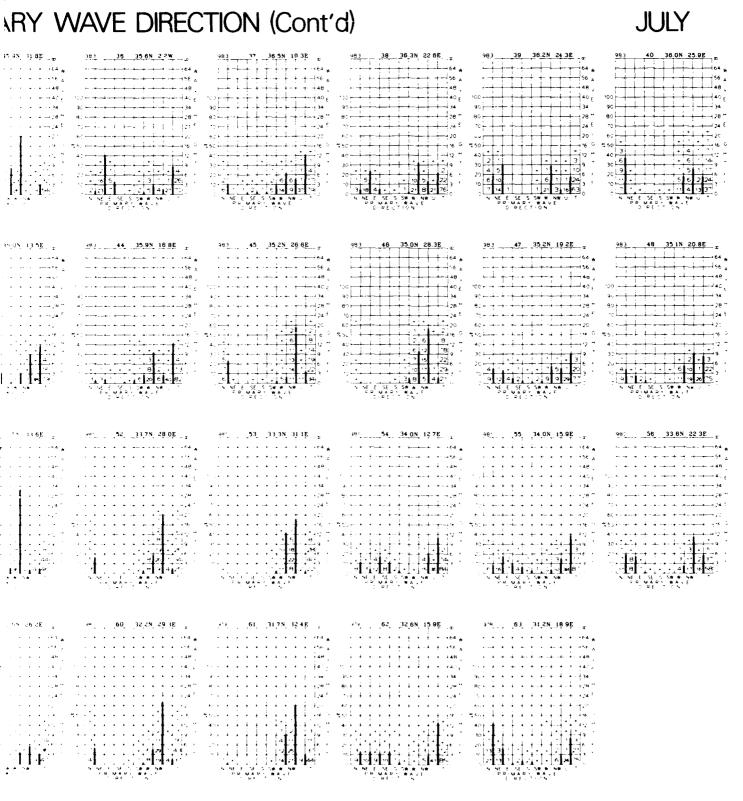
HFIGHT AND PRIMARY WAVE DIRECTION



WAVE HEIGHT AND PRIMARY WAVE DIRECTIC

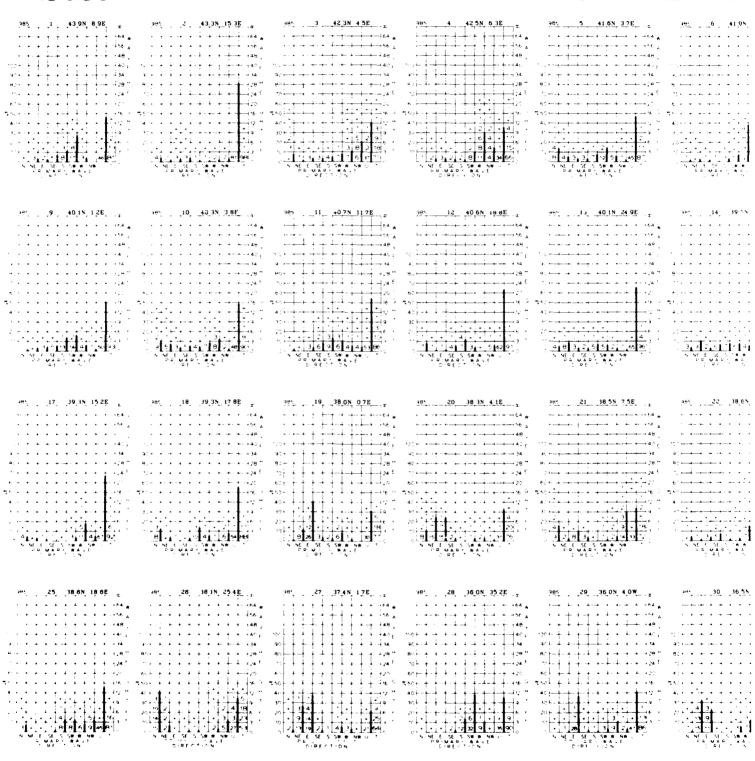


16 15 6

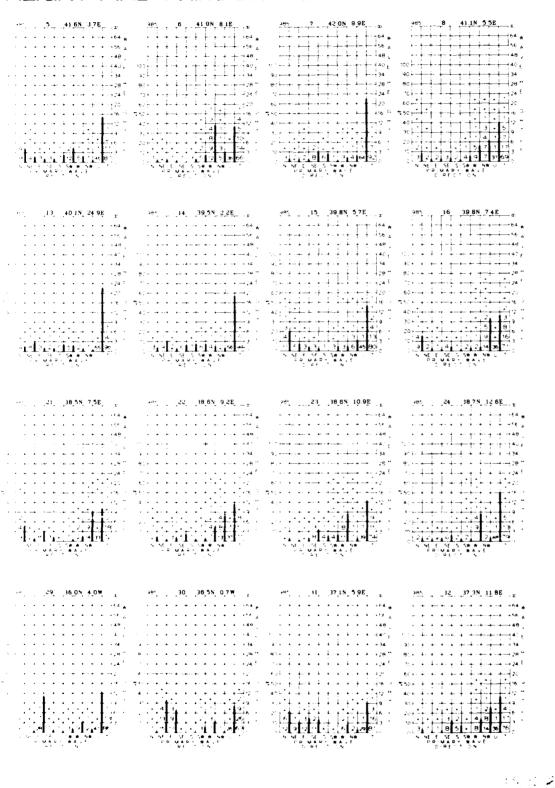


AUGUST

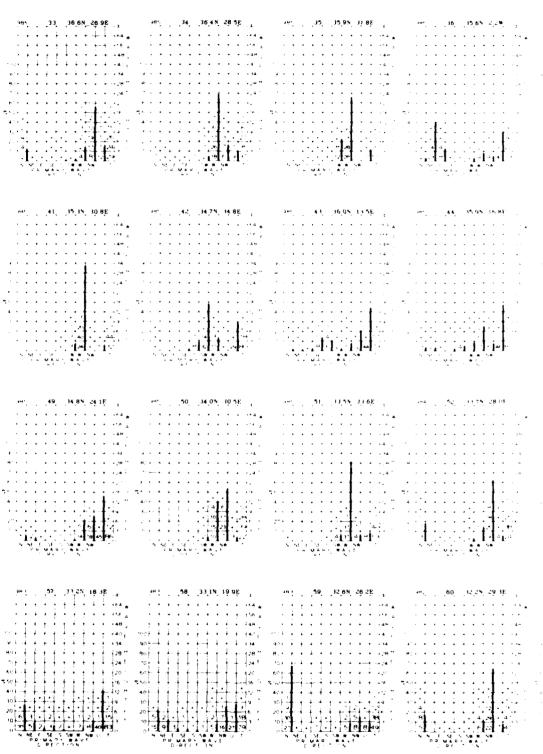
WAVE HEIGHT AND PRIM



HEIGHT AND PRIMARY WAVE DIRECTION

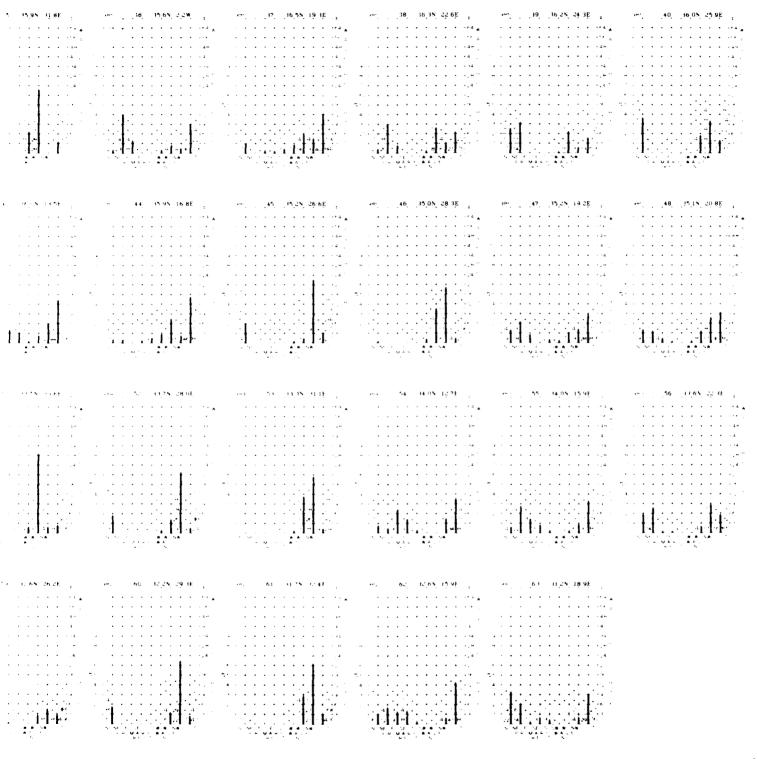


WAVE HEIGHT AND PRIMARY WAVE DIRECT



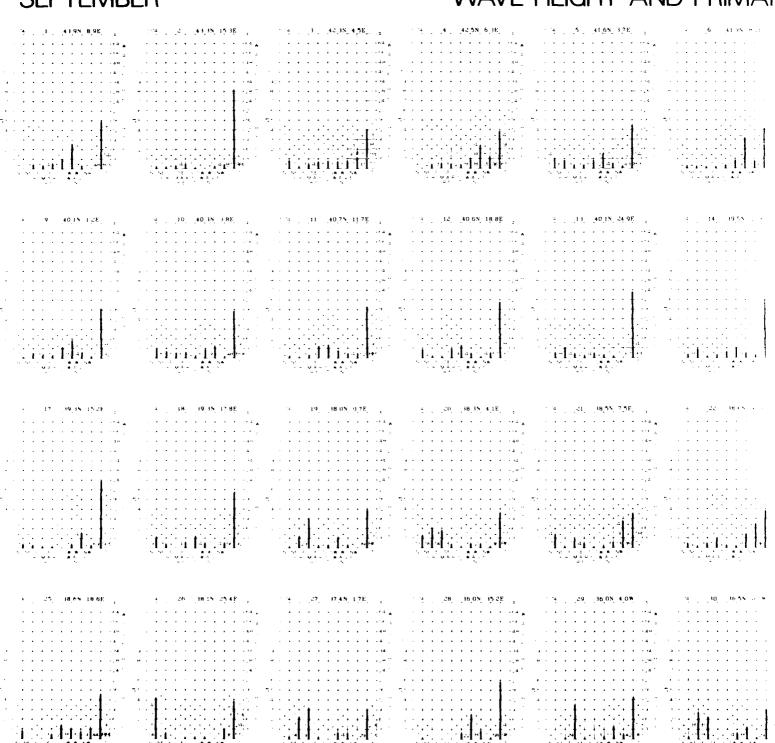
IARY WAVE DIRECTION (Cont'd)

AUGUST

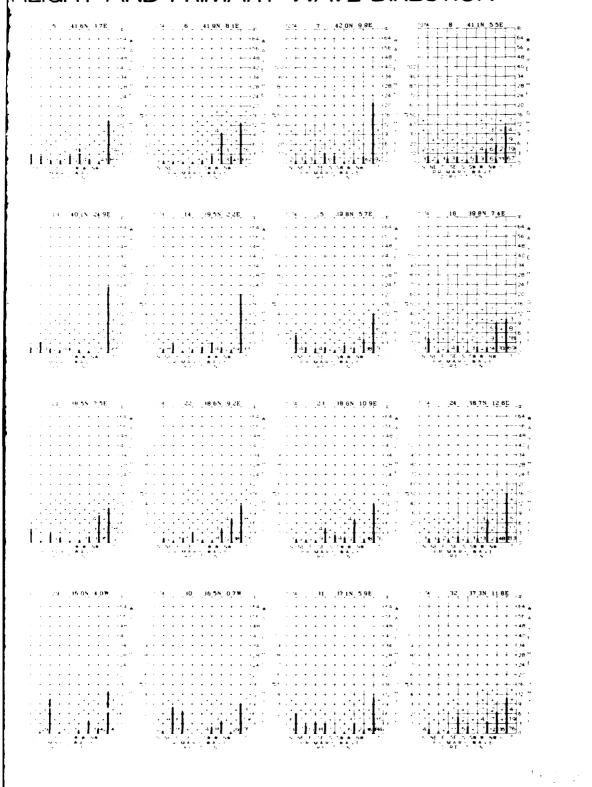


SEPTEMBER

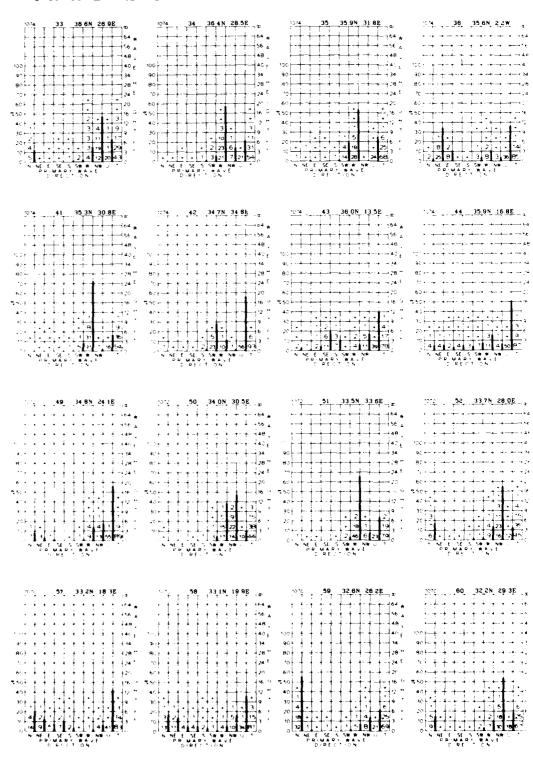
WAVE HEIGHT AND PRIMA!

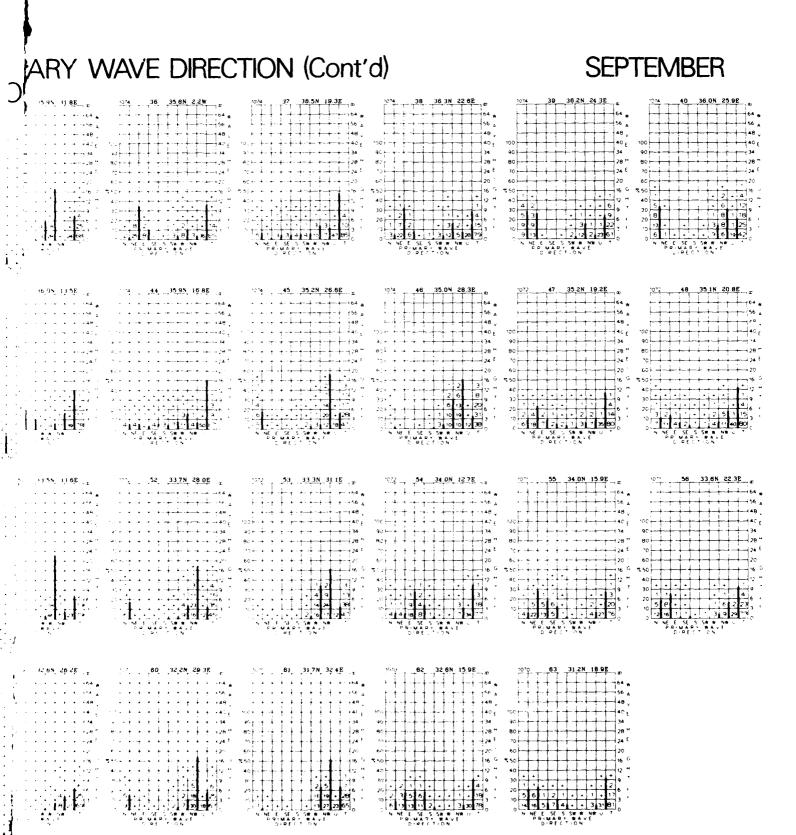


HEIGHT AND PRIMARY WAVE DIRECTION



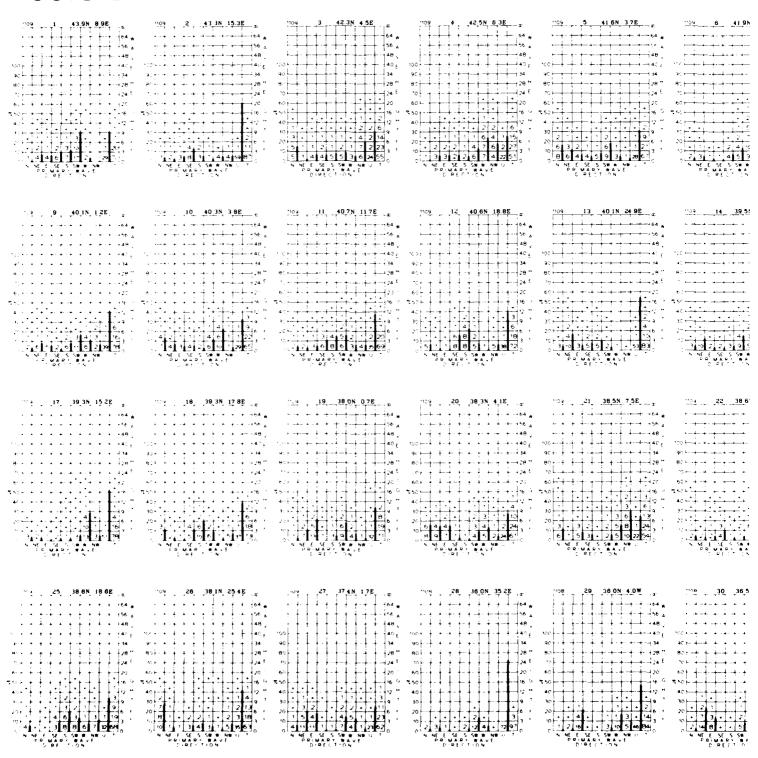
WAVE HEIGHT AND PRIMARY WAVE DIREC



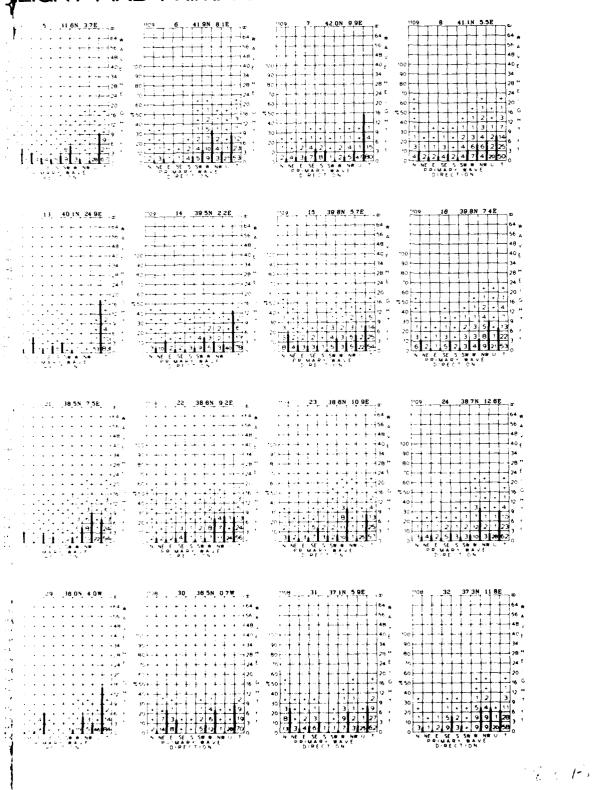


OCTOBER

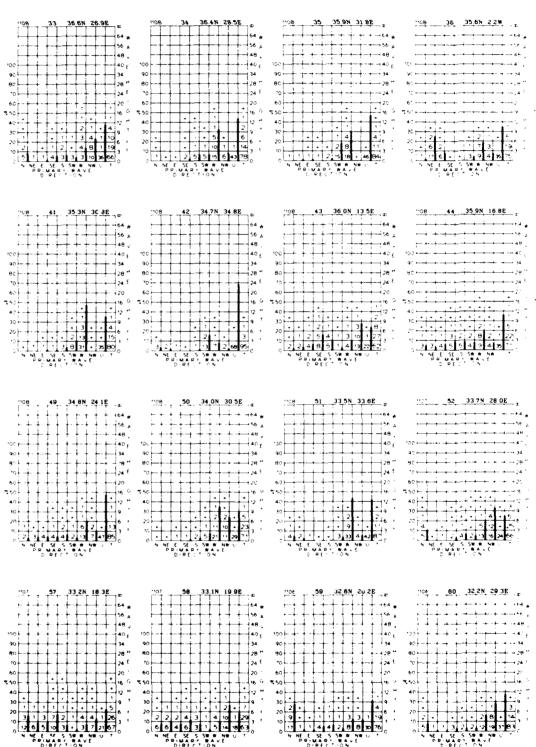
WAVE HEIGHT AND PRIN



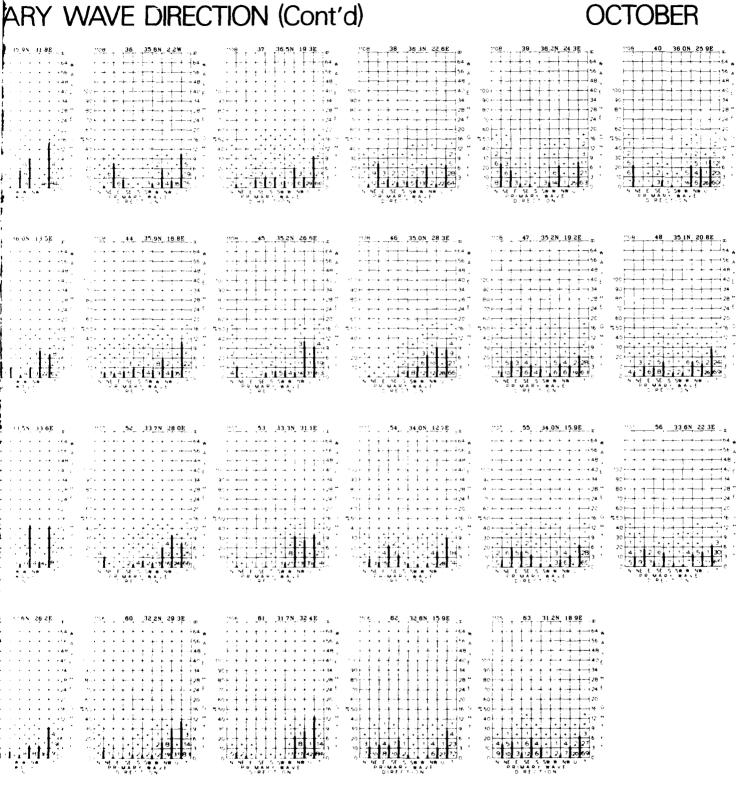
JEIGHT AND PRIMARY WAVE DIRECTION



WAVE HEIGHT AND PRIMARY WAVE DIRECT

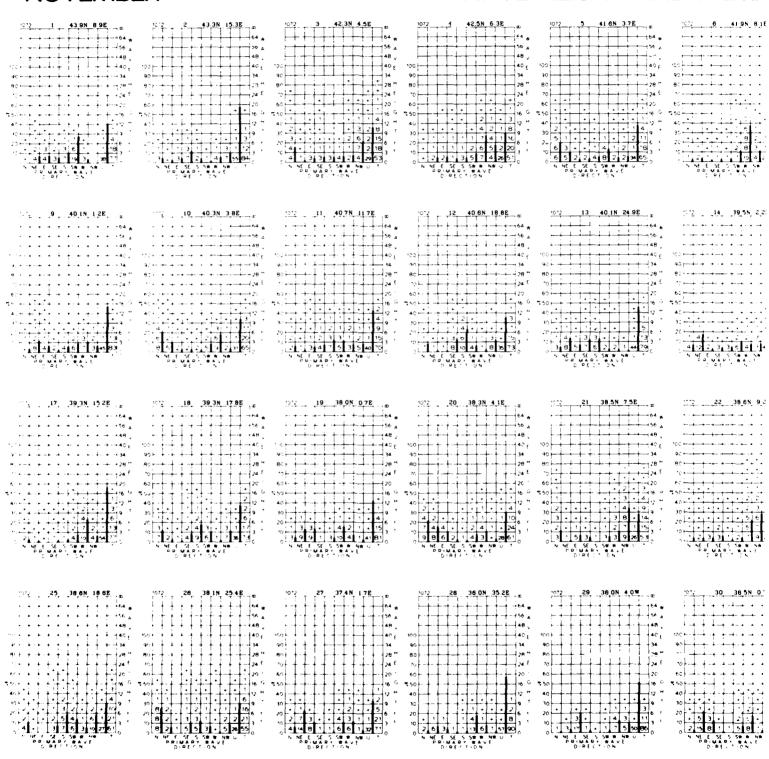


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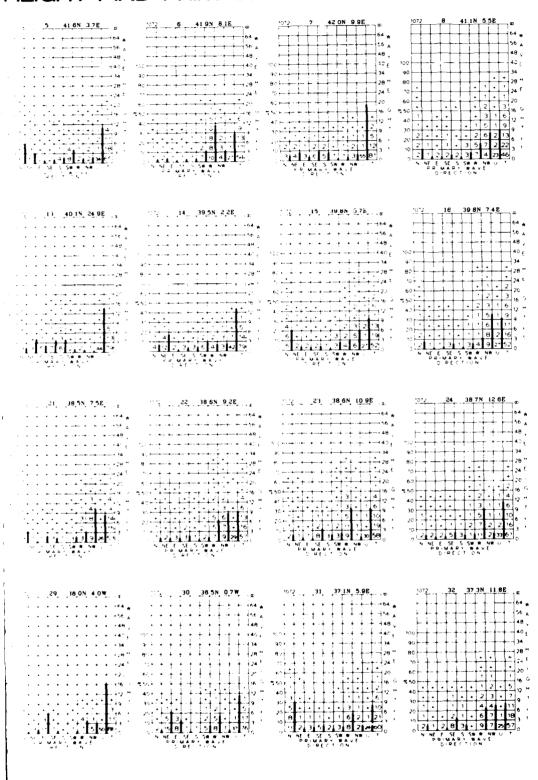


NOVEMBER

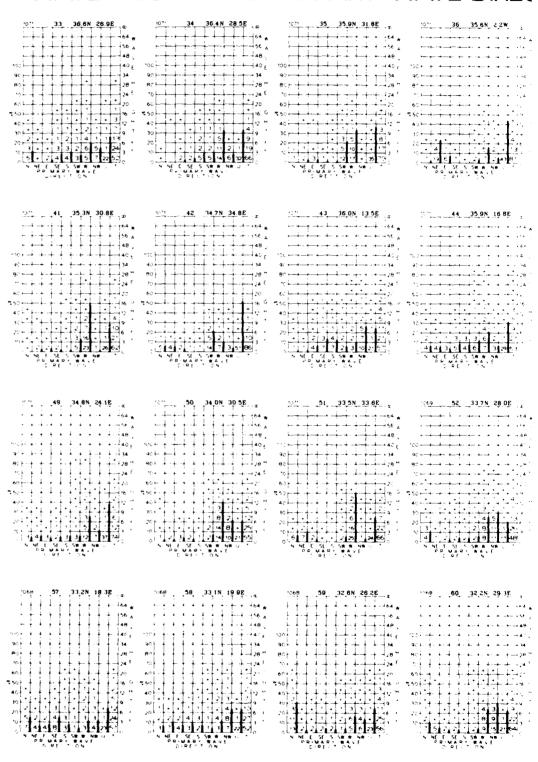
WAVE HEIGHT AND PRIMA



HEIGHT AND PRIMARY WAVE DIRECTION

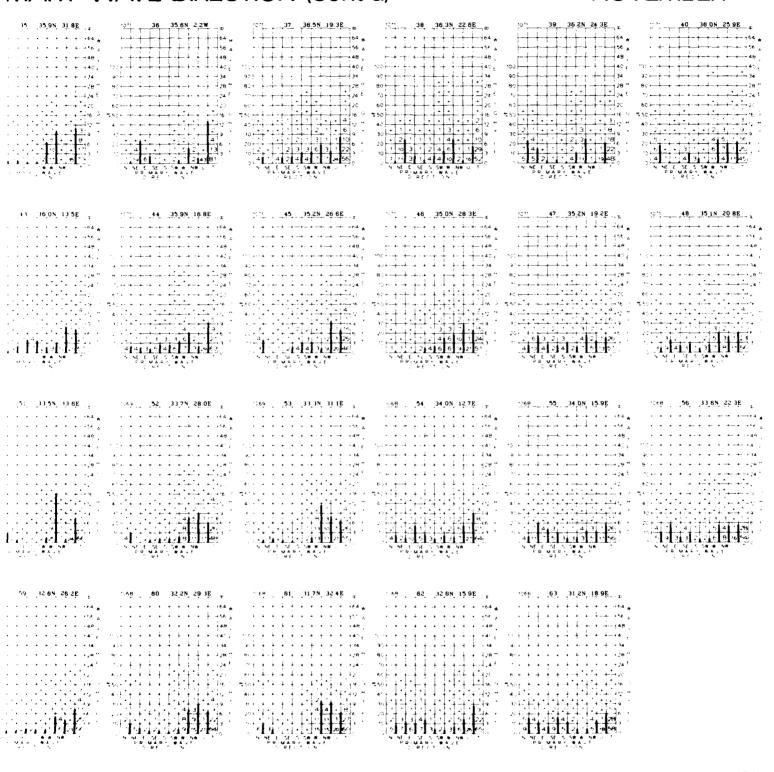


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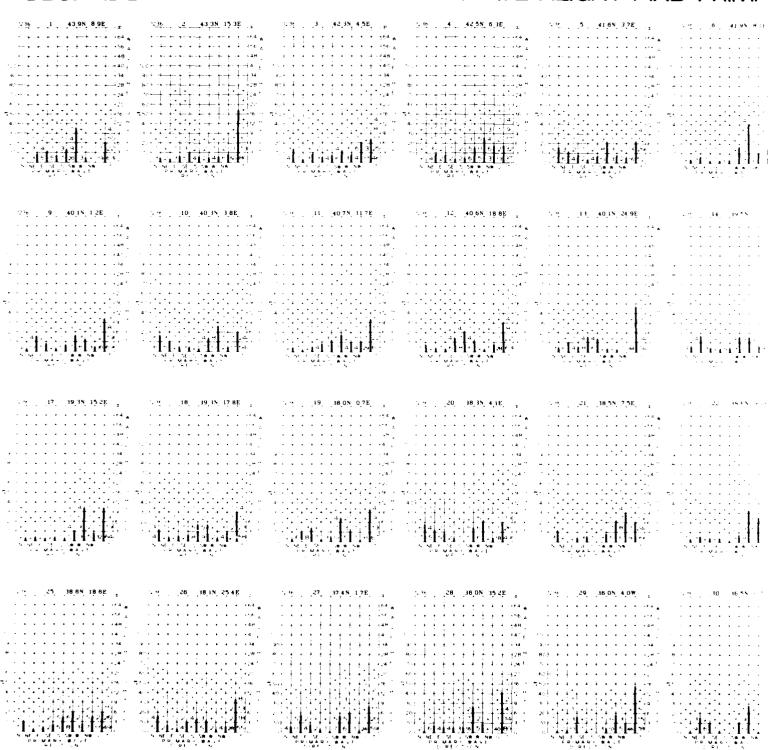
MARY WAVE DIRECTION (Cont'd)

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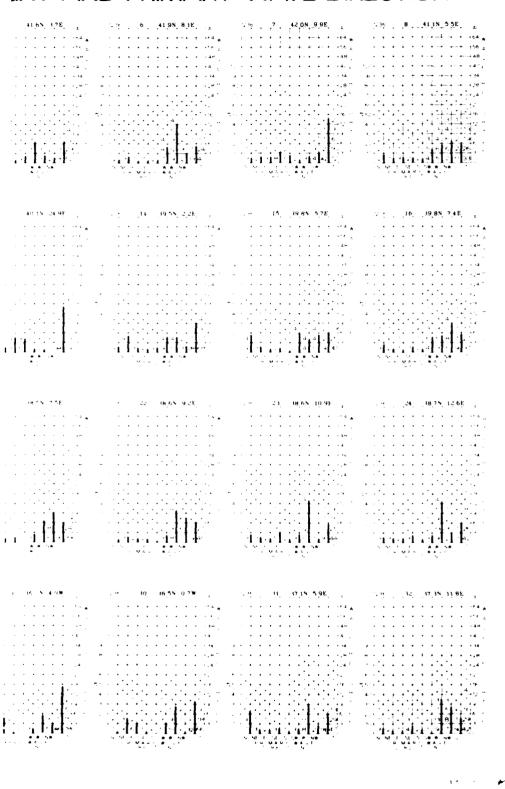


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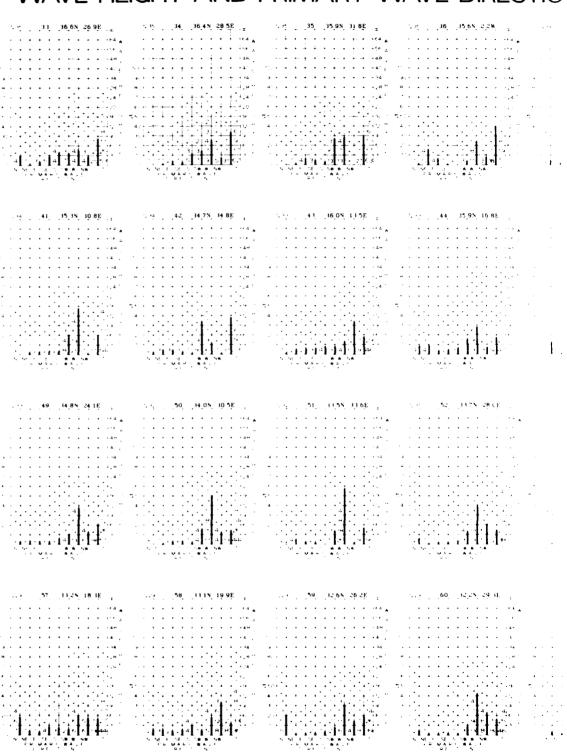
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3HT AND PRIMARY WAVE DIRECTION

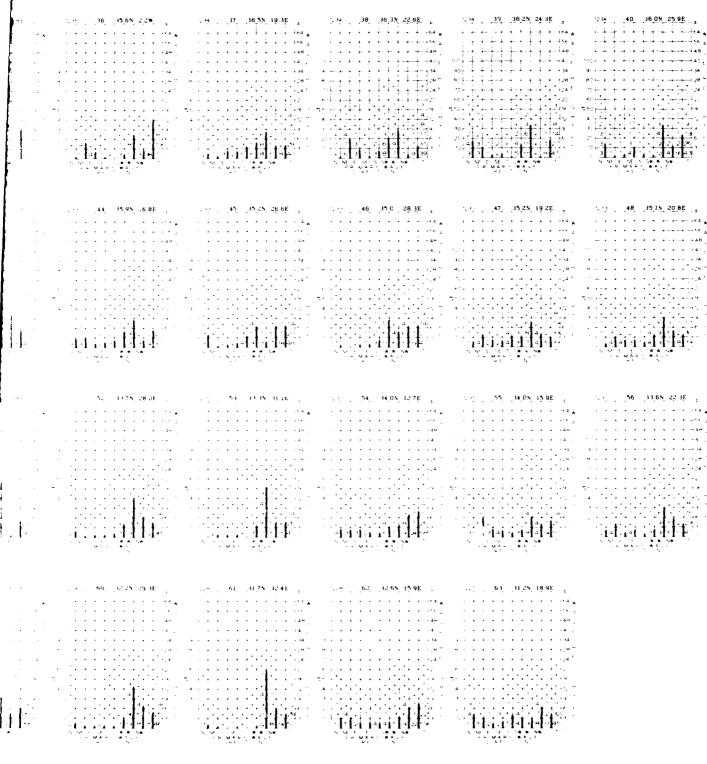


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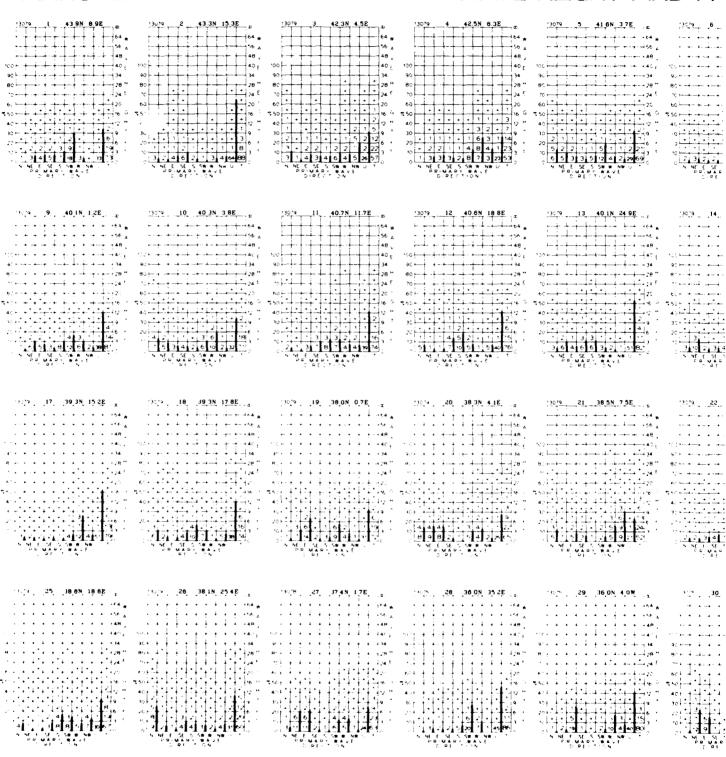


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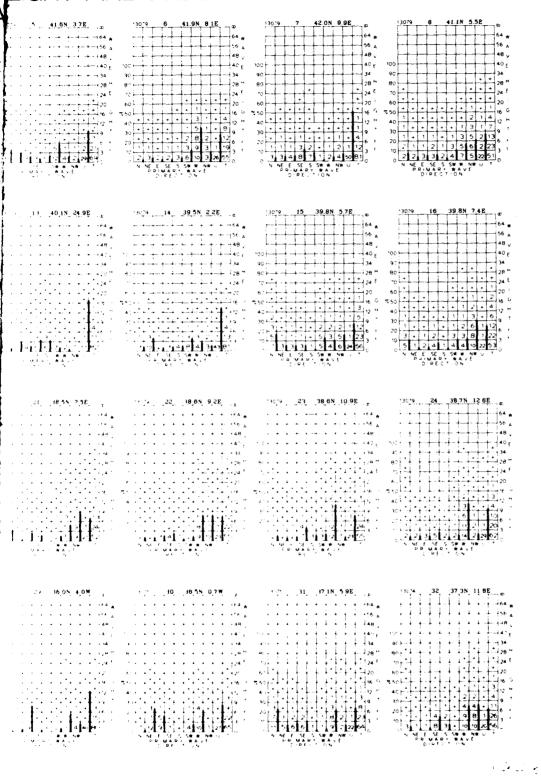


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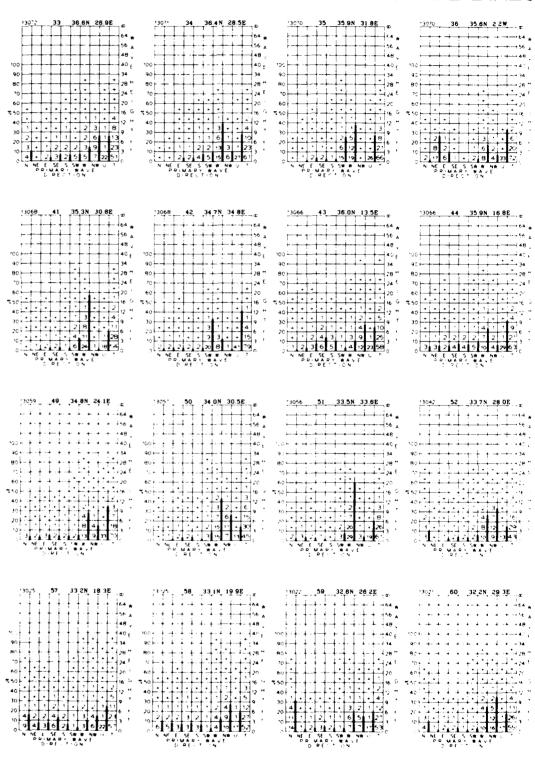
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EIGHT AND PRIMARY WAVE DIRECTION



WAVE HEIGHT AND PRIMARY WAVE DIRECT

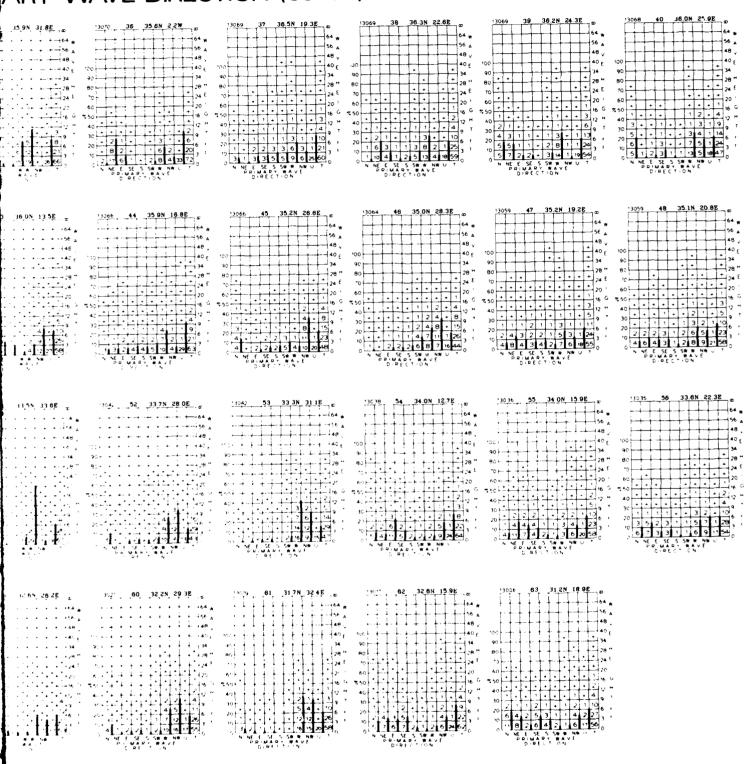


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Strate Committee Statement

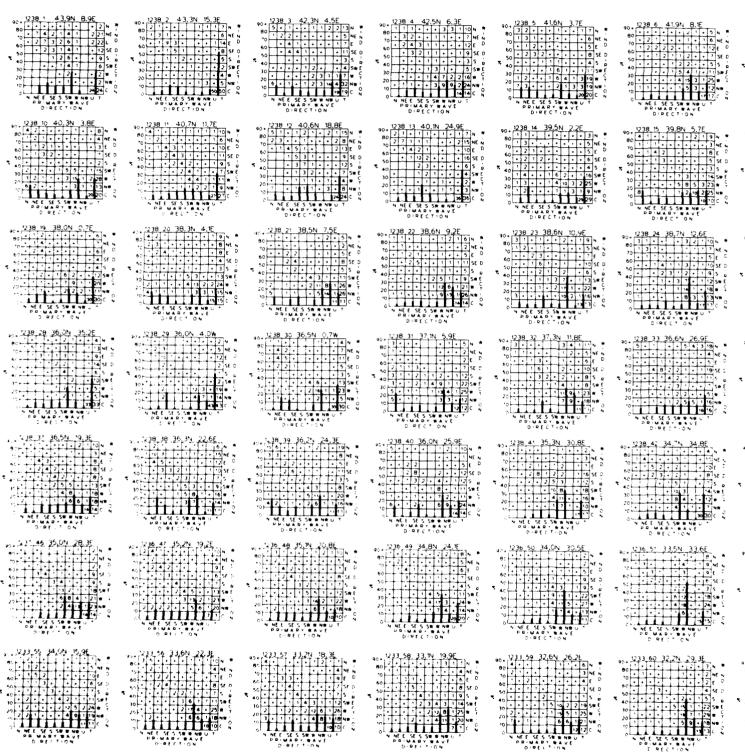
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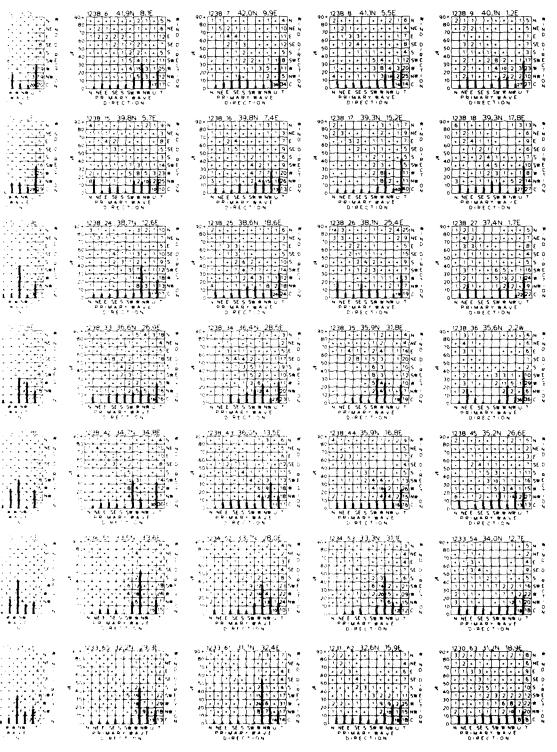
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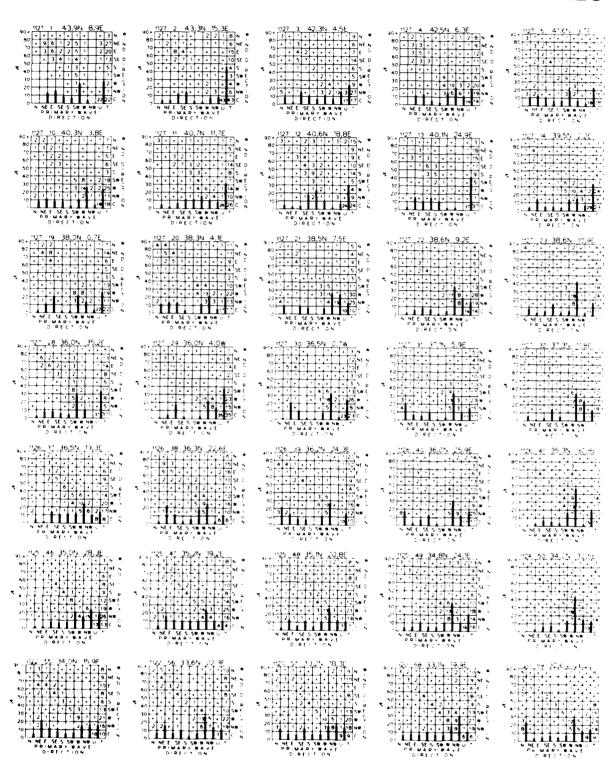


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WAVE DIRECTION AND WIND DIRECTION

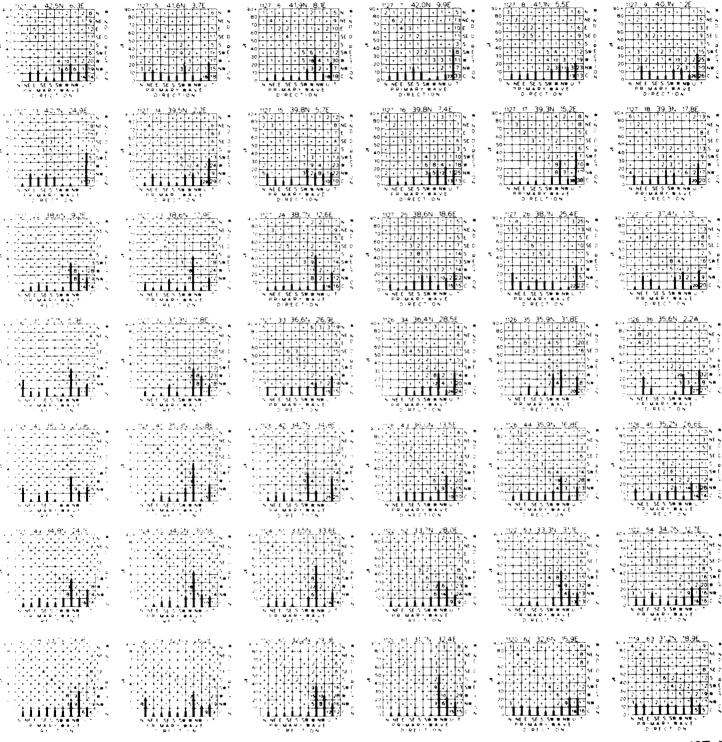


PRIMARY WAVE DIRECTION AND WIND DIRECT



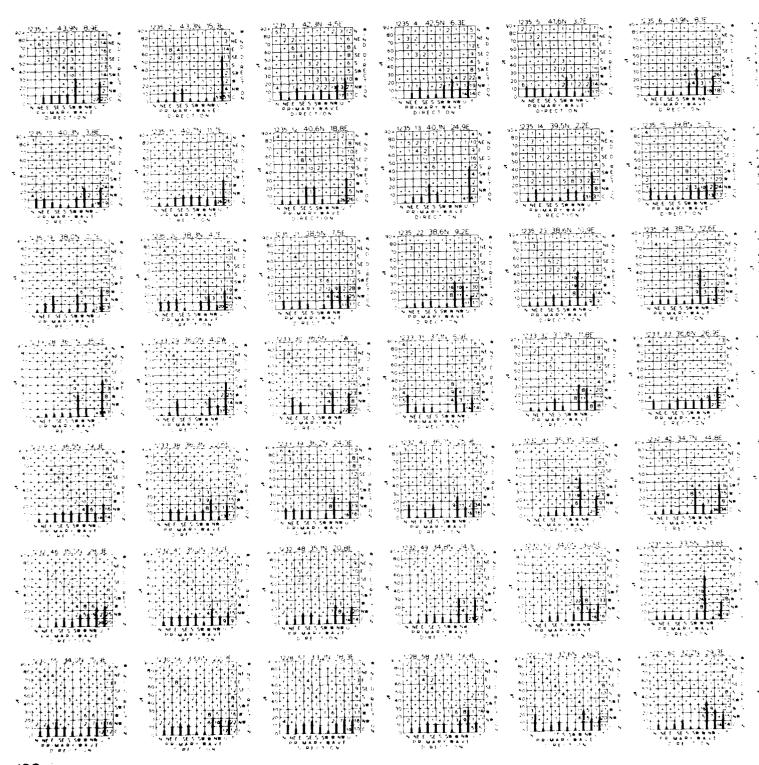
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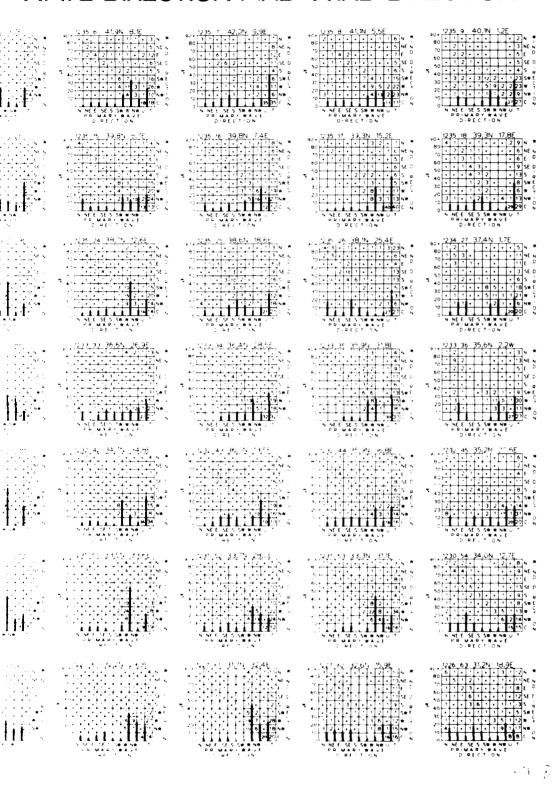


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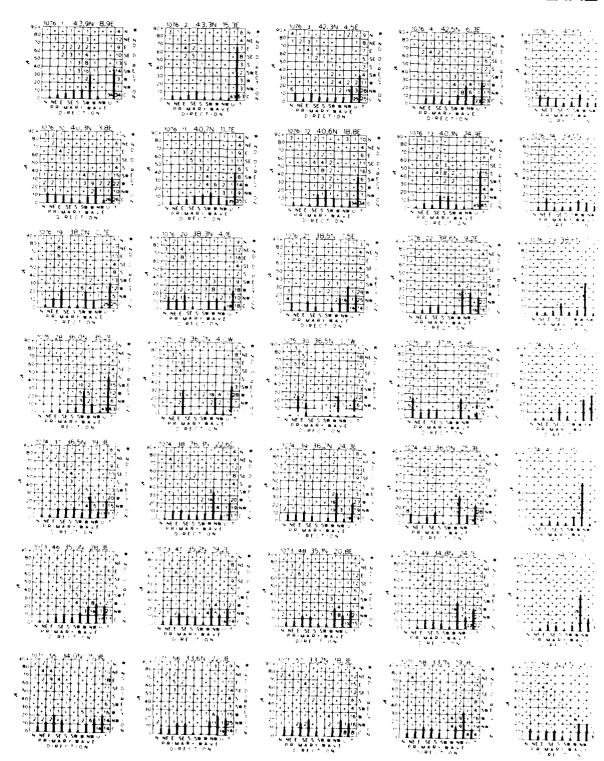
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WAVE DIRECTION AND WIND DIRECTION



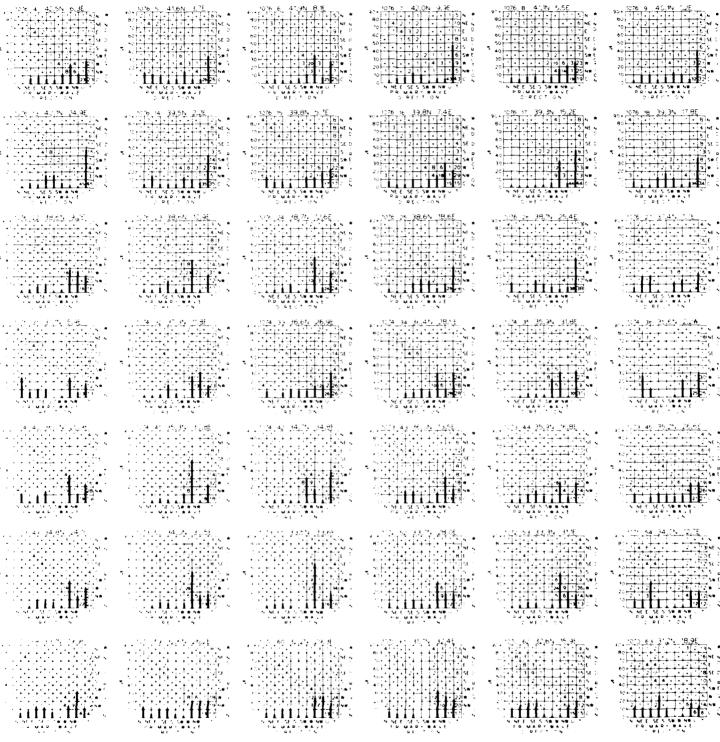
PRIMARY WAVE DIRECTION AND WIND DIRECTION



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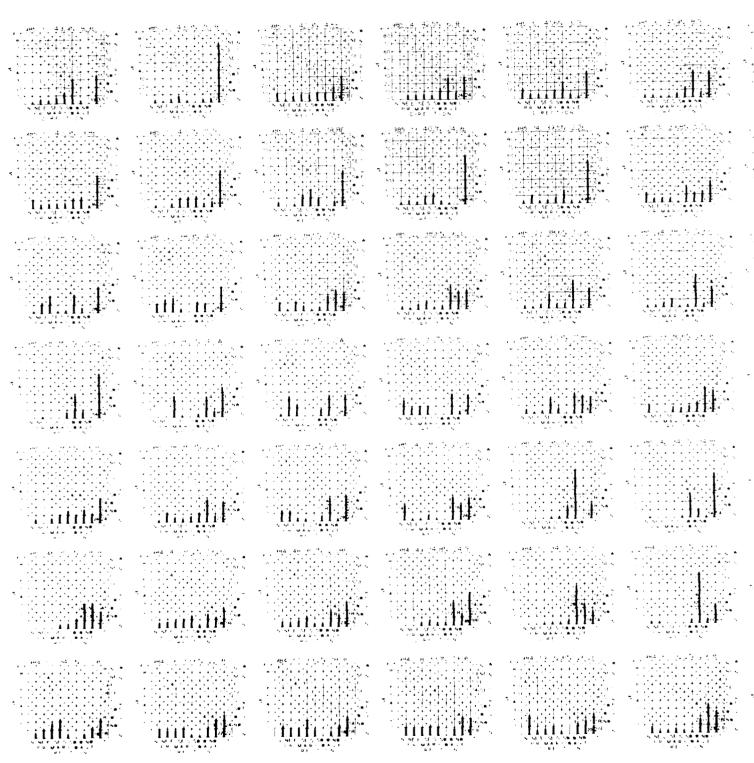
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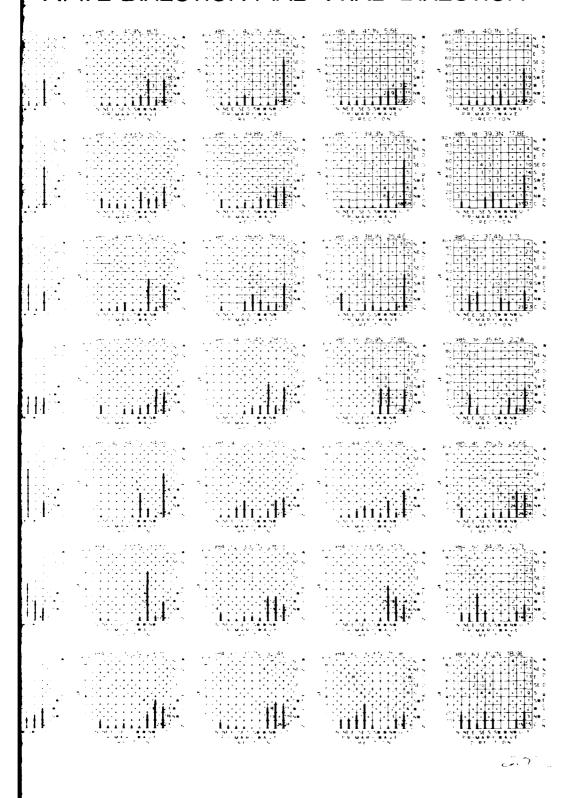


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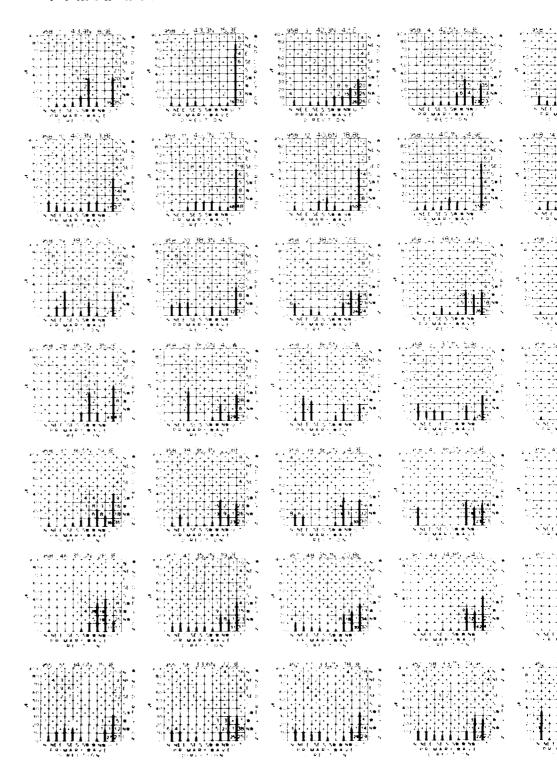
PRIMARY WAVE DIRECTION



WAVE DIRECTION AND WIND DIRECTION



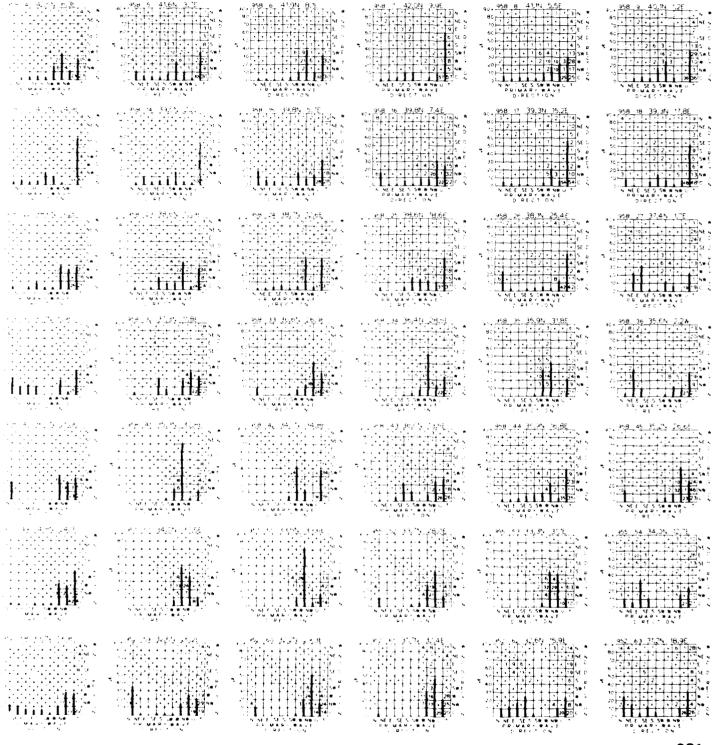
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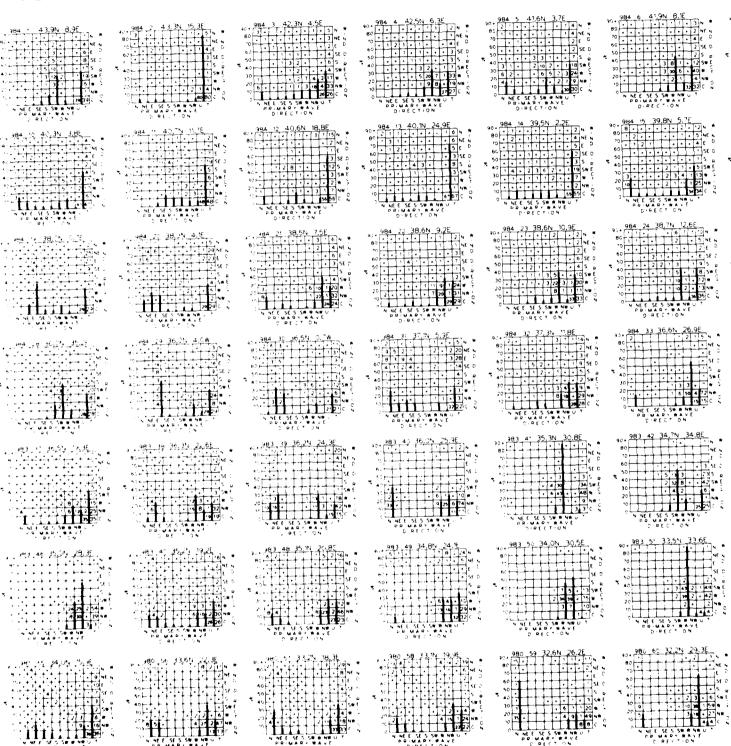
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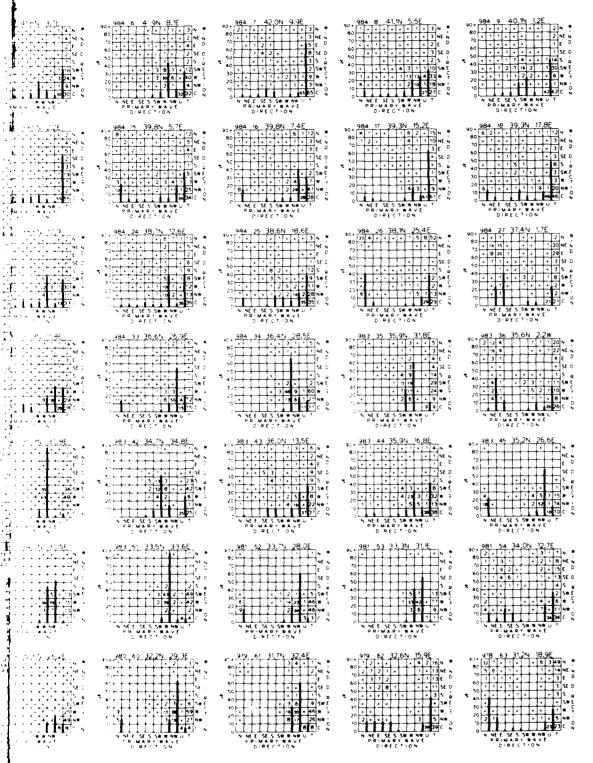


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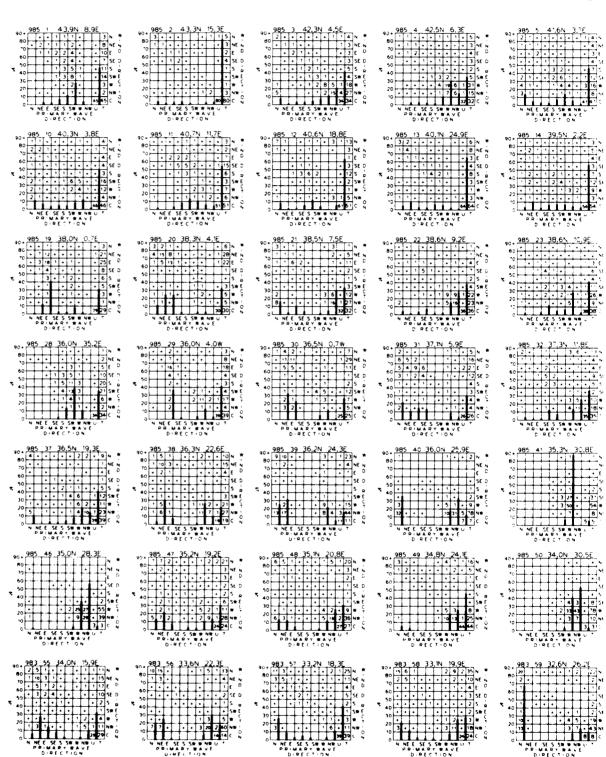


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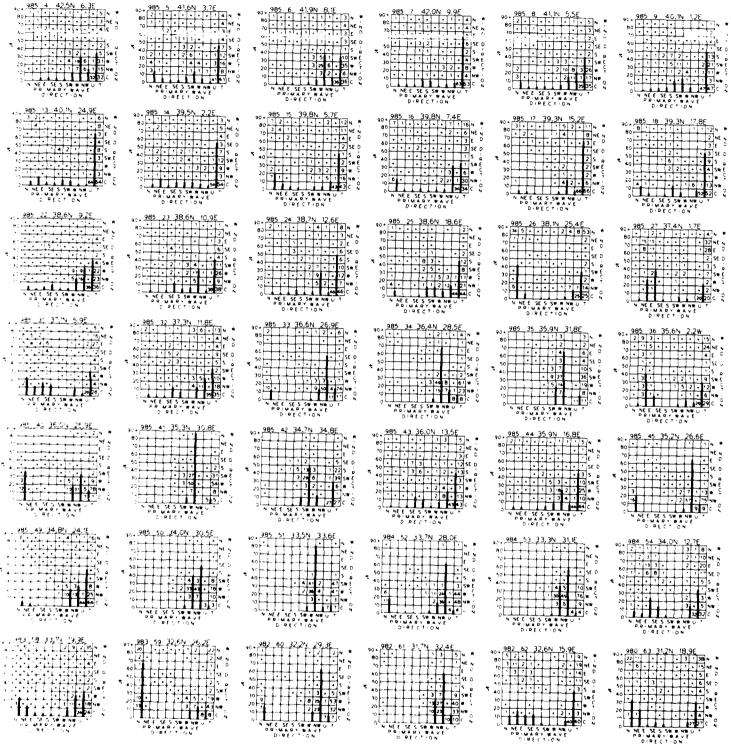
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PRIMARY WAVE DIRECTION AND WIND DIRECT



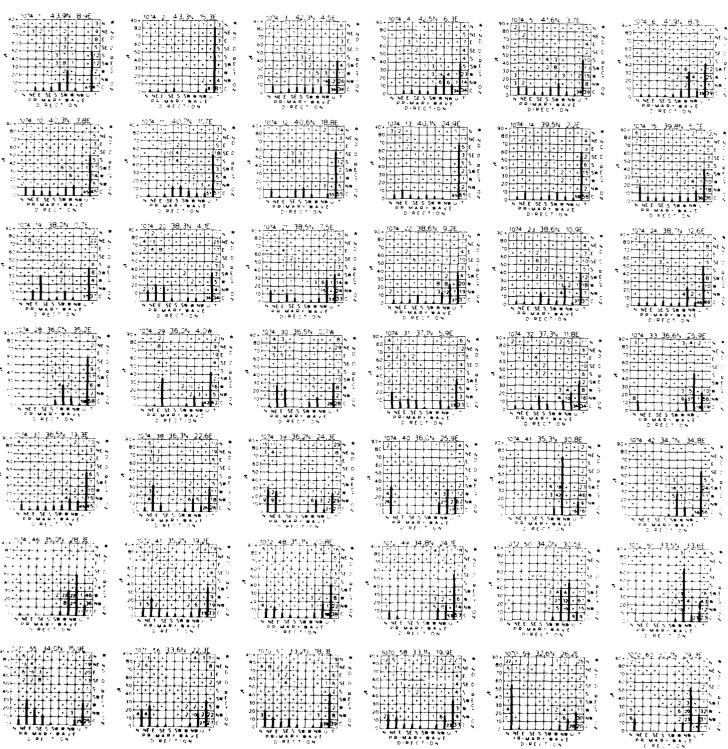
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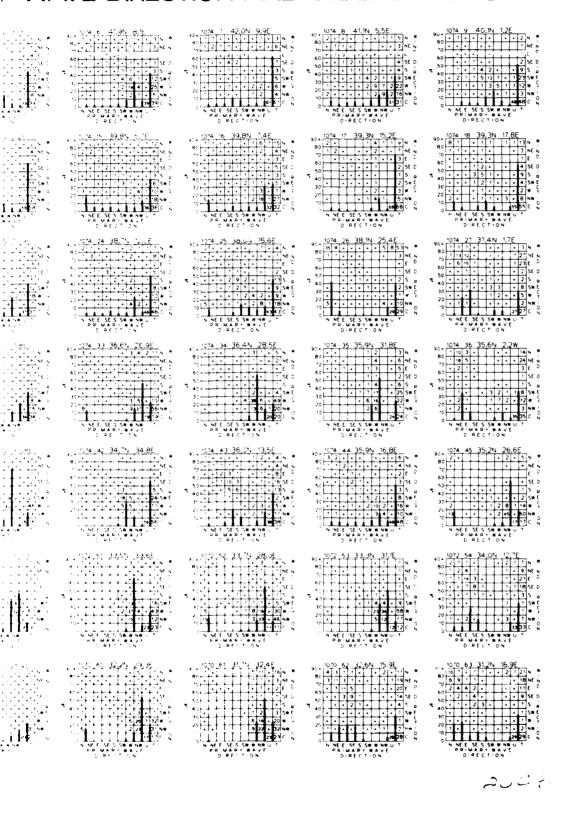


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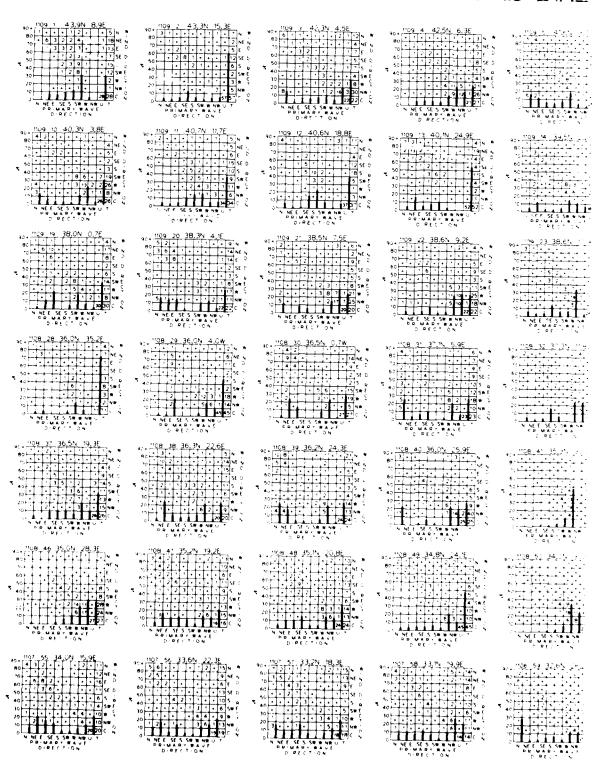
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WAVE DIRECTION AND WIND DIRECTION

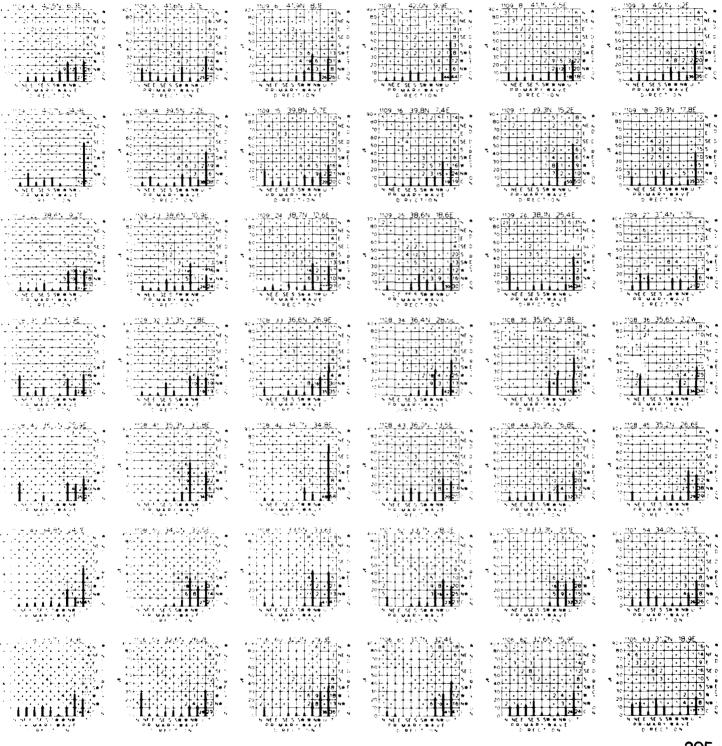


PRIMARY WAVE DIRECTION AND WIND DIRECTION



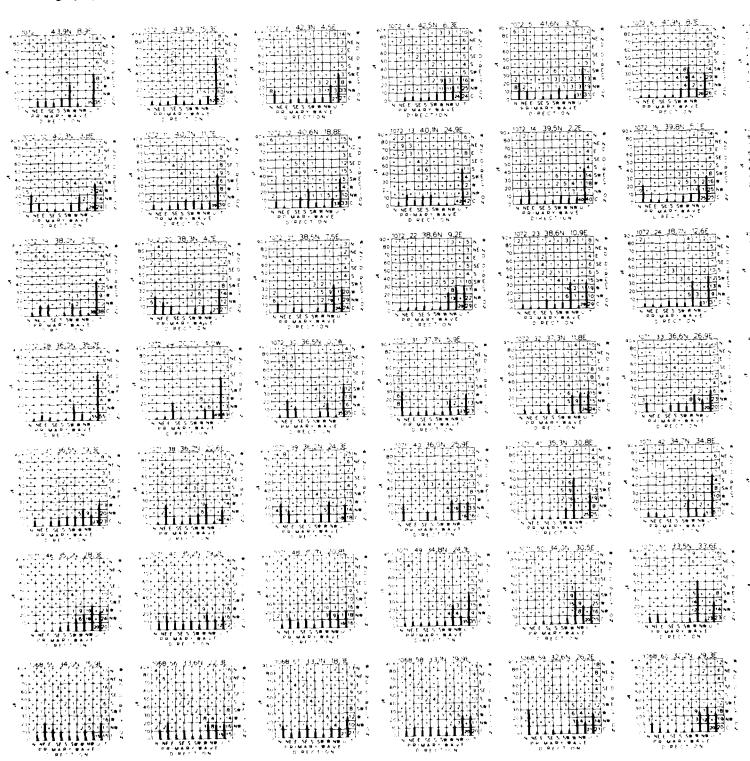
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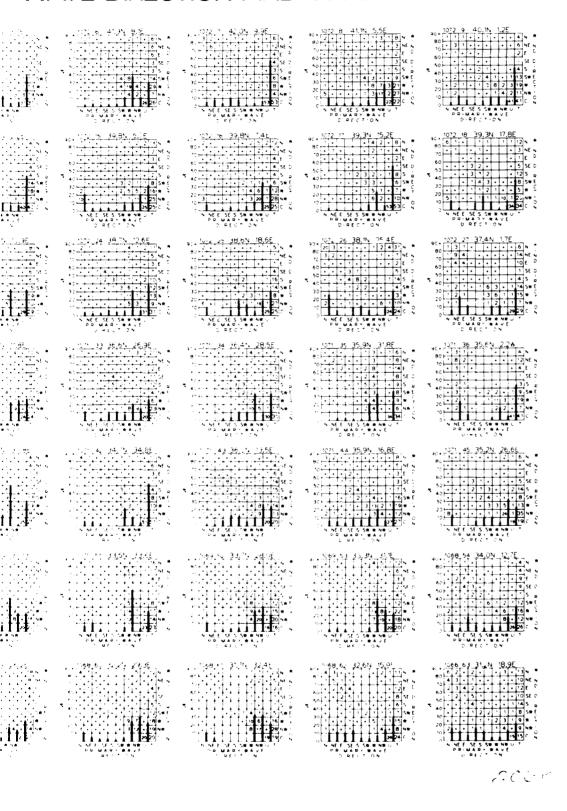


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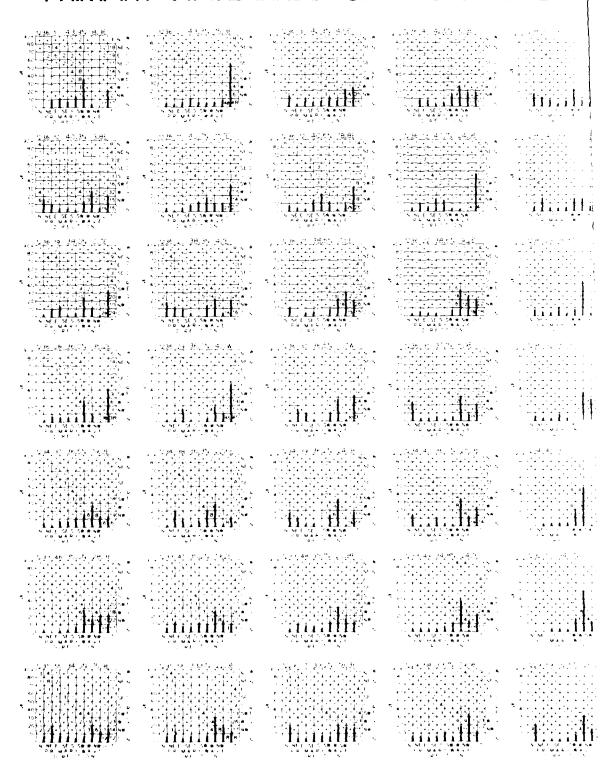
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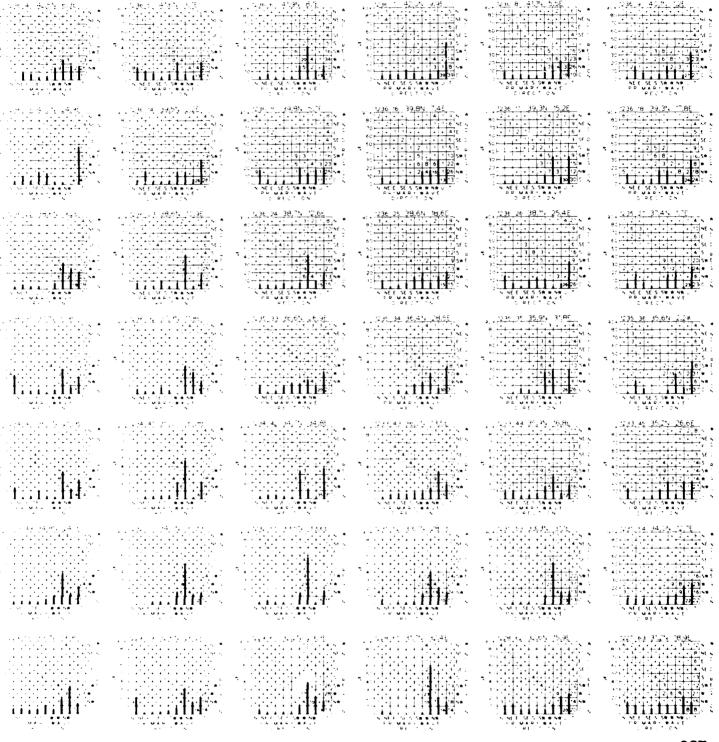


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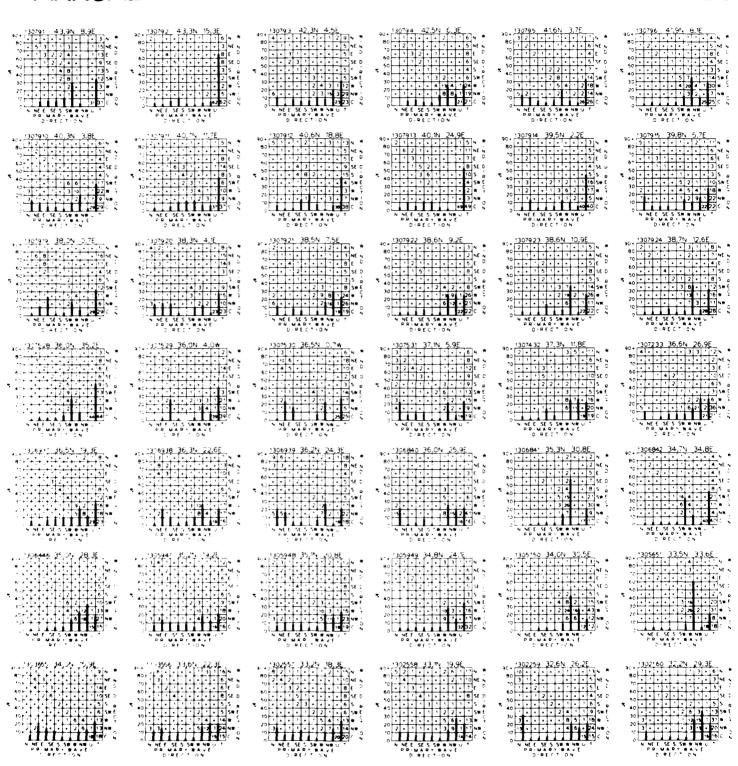
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DECEMBER

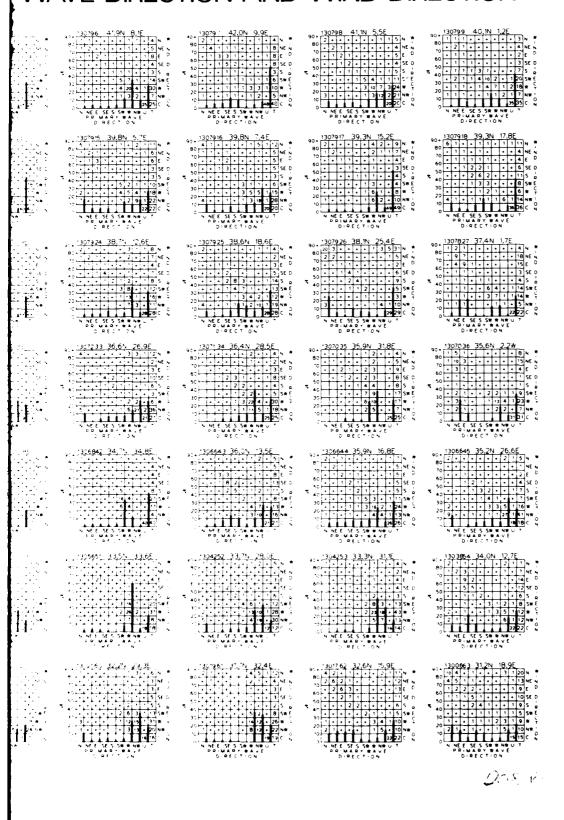


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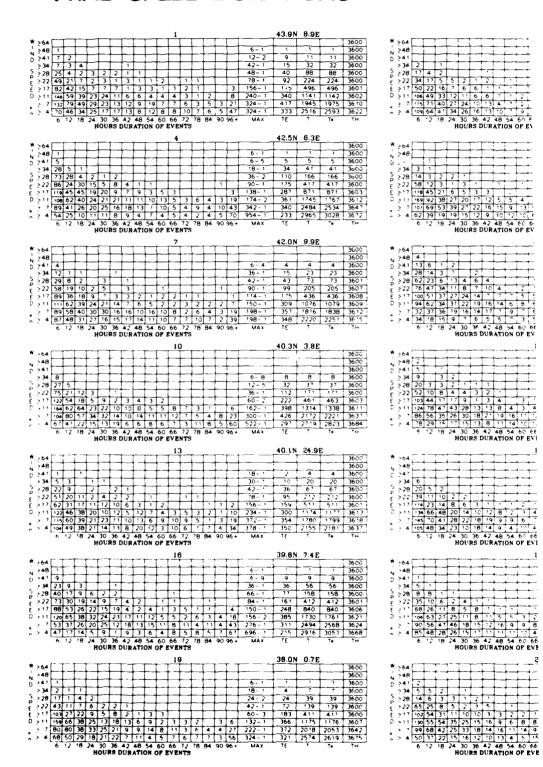
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WAVE DIRECTION AND WIND DIRECTION



WIND SPEED DURATIONS



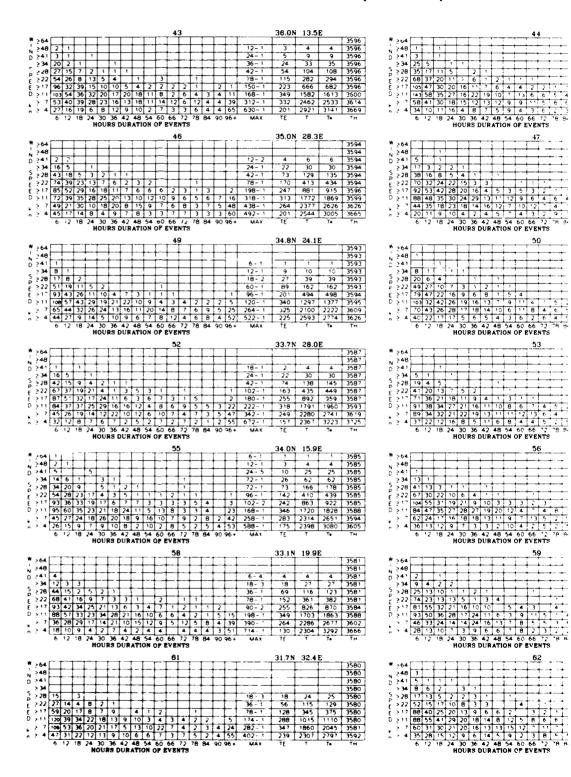
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2 2 2 68 37 20 11 7 6 1 2 1 1 1 66-1 155 370 1 1 1 3 1 08-1 259 811	373 3596 F > 22 74 44 22 10		1 156-1 176 470 485 3596 5 216-1 249 942 974 3597
43 58 35 27 16 22 19 10 1 13 6 6 5 4 2 16 234-1 389 748 58 4 30 18 15 12 13 12 9 9 1 5 8 6 3 45 384 295 2480		3 26 19 16 11 6 9 9 8 5 3 3 2 19 21 11 12 14 8 13 5 3 3 4 4	
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28 38 6 8 5 4 1 1 4 48 1 73 148 22 70 32 24 22 15 3 3 1 1 1 1 72 44	148 3593 3 28 39 15 7 2		42-1 67 121 121 3593 66-2 162 384 384 3595
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79 47 27 16 9 6 8 1 5 4 114-1 198 552 123 32 42 26 9 16 13 7 9 11 4 1 5 7 4 12 180-1 306 1370	1444 3596 0 511 103 54 34 1	5 11 2 3 1 1 1	66-1 136 321 341 3591 2 114-2 284 958 1000 3591
43 26 28 1 6 14 12 6 1 8 4 6 5 9 39 330 1 314 2180 4 4 22 1 1 5 6 5 4 3 6 2 6 4 5 2 58 648 1 202 2568	3005 3646 5 4 45 43 19 19	16 11 12 5 8 9 6 6 13 8 8	
6 '2 '8 24 30 36 47 48 54 60 66 72 '8 84 90 96+ WAX TE THOURS DURATION OF EVENTS		30 36 42 48 54 60 66 72 78 84 90 9 HOURS DURATION OF EVENTS	6+ MAX TE T To TH
53 33.3N 31.	3587 ₩ ≥64	54	34.0N 12.7E
18-1 1 3	3 3587 N 248 1 3 1		6-1 1 1 3585 24-1 5 11 11 3585
44 5 24-1 7 11 18 18 18 18 18 18 18 18 18 18 18 18	11 3587 > 34 10 5 1 54 3587 > 28 15 11 12 2		36-1 17 29 30 3585 54-1 42 96 102 3585
	205 3587 533 3587 537 538 538 538 538 538 538 538 538 538 538		78-1 106 267 285 3595 90-1 188 596 627 3585
38 34 22 21 6 11 10 8 6 7 4 5 2 9 186 1 289 127 83 34 32 2 22 1 13 1 1 1 12 13 6 4 7 3 29 276 1 326 2036		+-+	13 162 - 1 326 1461 1544 3590 37 438 - 1 308 2200 2437 3597
£ 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TE T	7980 3655 A 2 4 48 31 15 14 6 12 18 24	30 36 42 48 54 60 66 72 78 84 90 9	62 498-1 241 2450 2926 3626 6+ MAX TE T T# TH
HOURS DURATION OF EVENTS 56 33.6N 22		HOURS DURATION OF EVENTS 57	33.2N 18.3E
^4 4	3585 W >64 3585 > 48		12-1 2 2 3581
-4. · · · · · · · · · · · · · · · · · · ·	1 3585 5 241 5 3 5 3 15 3585 34 13 2 2 3		12-3 8 11 11 3581 30-1 21 40 40 3581
29 41 13 3 4 42 1 60 92 22 67 36 22 10 6 4 1 1 66 1 142 313	99 3585 6 28 30 19 6 2		66-1 64 140 151 3581 72-4 153 413 431 3581
265 782 194 55 31 19 21 9 10 3 3 3 2 3 1 1 96-1 265 782 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	830 3587 E > 17 64 45 37 2		2 108-1 232 842 904 3582 17 150-1 322 1726 1895 3588
6 2 24 1 6 18 8 3 1 9 7 13 5 2 11 7 42 282 1 275 276 4 36 13 2 9 7 3 3 7 10 4 2 5 2 5 2 60 546 1 175 245	2616 3629 > 7 39 30 15 10	3 19 10 12 10 8 13 9 7 7 4 4	
5 12 18 24 30 36 42 48 54 60 66 72 18 84 90 96+ MAX TE T HOURS DURATION OF EVENTS	Te TH 6 12 18 24	30 36 42 48 54 60 66 72 78 84 90 9 HOURS DURATION OF EVENTS	
59 32.6N 26.	2E # >64	60	32.2N 29.3E
, 40 , 10 , 10 , 10 , 10 , 10 , 10 , 10 , 1	3580 N 248 5 3580 0 241 1		3580 24-1 4 4 3580
. 14 3 4 2 2 2 2 17 31 24 2 17 31 66 1 54 120	31 3580 234 4 3	+,+++++++++++++++++++++++++++++++++++	36-1 8 16 18 3580 54-1 41 75 85 3580
722 74 23 13 13 5 1 3 4 1 1 78 - 1 131 308 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	358 3581 . > 22 61 24 9 7		54-2 112 235 268 3580 90-1 221 611 684 3580
93 50 36 28 17 24 16 3 9 11 5 1 4 4 20 258 1 32 1644 46 33 24 4 4 24 16 3 7 8 5 5 3 8 1 39 4 38 1 260 2160	1845 3597 D 211 103 55 28 2	2 12 16 11 13 6 10 4 6 1 2 2	16 210-1 307 1399 1568 3580 33 288-1 299 2053 2397 3606
· 4 28 3 19 1 3 9 6 6 2 8 2 3 2 2 3 49 480 · 1 158 2118	3204 3712 - 4 49 19 17 9	9 12 3 1 10 7 5 3 2 3	57 474-1 206 2254 3033 3681
HOURS DURATION OF EVENTS		30 36 42 48 54 50 66 72 78 84 90 9 HOURS DURATION OF EVENTS	
62 32.6N 15	3578	63	31.2N 18.9E
-41.5.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1	3 3578 N 48 1 1 1 3 2 1 3 2 1 3 2		6-1 1 1 3575 12-2 5 7 3575
· 28 (대한 제공 2 전 대학 대학 대학 대학 대학 대학 대학 대학 대학 대학 대학 대학 대학		151-1-1-1-1-1-1-1-1	30-2 18 38 38 3575 48-1 41 98 106 3575
72 1 1 3 3 3 4 1 7 3 1 3 3 3 4 3 1 7 3 1 96 1 220 692	. 1 338 3578	A 3 4 1 1 1 1 1 5 5 18 14 6 3 3 2 2 2 2	78-1 106 270 298 3575
(60, 31, 30, 71, 20, 16, 13, 13, 15, 12, 7, 11, 7, 13, 2, 13, 12, 22, 1, 15, 24, 20, 20, 20, 20, 20, 20, 20, 20, 20, 20	1714 3582 0 211 79 53 43 2 2515 3584 27 48 28 26 26 26	5 18 14 6 3 3 2 2 2 2 7 2 19 11 10 4 11 3 4 2 2 11 16 18 14 9 11 2 15 9 6 6 6	13 186~1 323 1517 1736 3583 34 540~1 272 2090 2510 3590
98 55 47 29 20 18 48 81 22 5 8 6 6 8 3 3 11 272 1377 1377 1478 1478 1478 1478 1478 1478 1478 14	79 16 3594 n 2 4 29 21 5 7 To TH 6 12 18 24	5 6 8 3 3 6 2 3 5 4 1 1 3 3 3 6 7 78 84 90 9	55 552-1 163 2313 31 84 3636
HOURS DURATION OF EVENTS		HOURS DURATION OF EVENTS	

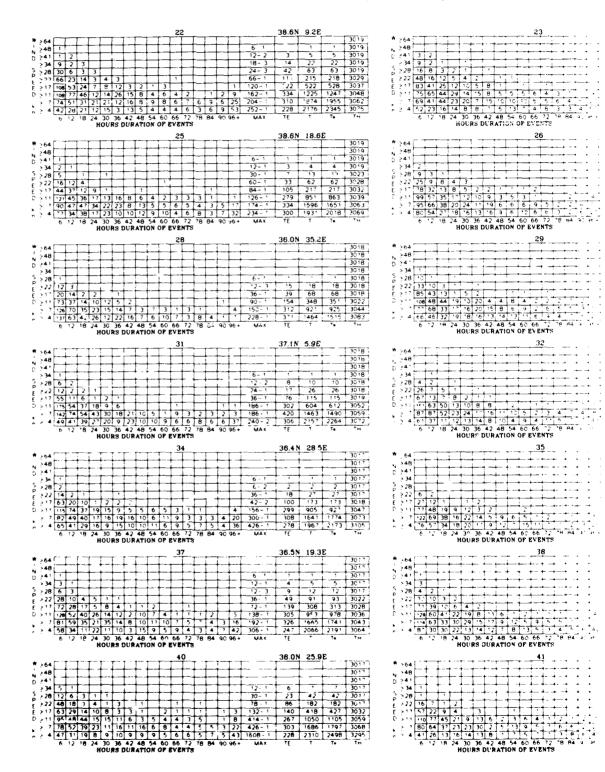
SPRING

WIN

1 43.9N 8.9E	2 43.3N 15.3E
* >64	W >64
248 3019 2 241 1 1 2 2 3019	0 >41
5 28 4 3 1 12-1 3 4 4 3019 5 28 4 3 1 12-3 7 10 10 3019	2 34 1
F > 22 28 6 2 16-2 36 46 46 3019	E > 22 13 3 1 1 36-1 17 25 25 3019
2 17 59 13 10 6 1 2 3 2 2 3 1 2 2 91 156 157 3019 2 1 1 87 55 27 12 6 8 7 4 2 3 2 2 1 1 120 1 216 599 600 3023	0 > 11 68 28 12 9 6 2 1 3 3 2 72 2 131 300 301 3030
2 7 19 62 52 25 16 10 9 11 12 5 4 3 2 5 1 6 126 1 342 1250 1287 3033 2 4 94 40 22 23 21 15 14 9 11 3 5 7 5 4 2 30 228 1 305 1782 1827 3052	> 7 93 57 24 15 14 5 5 4 2 4 3 3 2 114 1 231 683 688 3038 > 4 109 58 16 14 17 10 4 10 3 3 4 1 1 1 7 138 1 258 863 868 3043
6 12 '3 24 30 36 42 48 54 60 66 72 '78 84 30 96+ MAX TE T To TH HOURS DURATION OF EVENTS	6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96 * MAX TE T TO TH HOURS DURATION OF EVENTS
4 42.5N 6.2E	5 41.6N 3.7E
* ·64 ·48 3 3 3 3 3019	* >64 >48 1 6-1 3019
0 24 1 3 7 7 3022	N >41 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
2 34 14 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2 34 3 3 3 3019 5 28 7 3 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
22 63 27 9 9 3 4 1 2 1 1 90-1 120 269 269 3033	E 227 28 6 2 1 1 42 1 37 53 53 3019 E 217 73 24 6 2 1 1 1 90-1 108 174 174 3019
2 211 104 63 36 15 11 15 12 9 3 5 6 2 4 2 1 13 (38-1 30) 1204 1206 3049	D > 11 144 92 37 20 11 5 4 3 4 2 1 1 162-1 323 739 751 3022
2 4 50 29 19 16 18 11 8 2 15 5 9 3 3 28 264 1 314 1862 1878 3073 1 4 50 29 19 16 10 10 14 6 6 7 7 6 4 2 5 46 408 1 237 2206 2250 3083	2 7 104 79 68 33 31 12 15 17 9 5 8 7 4 3 : 6 216-1 396 1560 1595 3026 2 5 4 73 40 26 26 29 11 11 9 10 7 7 8 3 7 6 31 324-1 304 1993 2059 3035
6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TE T TO TH HOURS DURATION OP EVENTS	6 12 18 24 30 36 42 48 54 50 66 72 78 84 90 96+ MAX TE T TO THE HOURS DURATION OP EVENTS
7 42.0N_9.9E	8 41.1N 5.5E
3019 248	W 264 2 1 1 12-1 3 4 4 3019
6-1 3019	D 241 3 5 13 13 3019
5 > 28 10 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	\$ > 28 25 12 7 5 2 1 1 1 48-1 56 133 133 3021
222 18 4 3 1 2 1 42-1 29 56 56 3019 E 11 46 12 9 1 4 1 1 1 1 48-1 7 142 142 31.0	2 22 48 23 10 6 4 4 3 3 3 1 2 120 1 107 311 311 3027 E > 1 9 42 70 13 10 0 1 4 5 4 1 1 1 1 7 162 1 206 623 624 3032
0 21 84 51 17 6 12 6 4 1 4 2 2 1 90-1 190 494 497 3033	0 3 11 92 52 35 24 21 12 10 7 6 7 6 4 4 5 3 13 216-2 301 1416 1422 3047
2 4 132 70 40 25 1: 13 B 9 B 7 6 3 5 2 2 12 162 1 353 1358 1374 3049	n > 4 57 23 17 10 8 7 12 5 8 5 6 3 6 7 4 52 492-1 230 2264 2364 3099
6 12 18 24 30 36 42 48 54 60 66 72 78 84 9C 77: MAX TE T To TH HOURS DURATION OF BY ENTS	6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX 7E T T# TH HOURS DURATION OF EVENTS
10 +0.3N 3.8E	# >64 11 40.7N 11.7E
* 264 248	>48
0 :41 30:9	0 241 2 34
S 28 5 1 12-1 6 7 7 3019	28 3 2 2 1 18-2 7 13 13 3019
E > 12 66 20 10 4 1 2 36 2 103 169 169 3019	E > 17 67 14 9 4 2 4 1 1 1 1 60-1 96 183 183 3020
2 3 1 1 13 70 40 17 10 5 4 2 1 3 1 1 78 1 326 6 7 6 7 9 30 20 3 7 14 1 7 2 1 3 1 2 3 1 1 1 1 1 3 2 6 6 7 6 7 9 30 20 3 7 14 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	D > 11 111 54 24 17 6 7 5 7 5
4 99 55 28 32 16 14 15 12 8 6 7 4 8 6 5 22 360 1 337 1870 1932 3037	6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TE 7 TH
Hours duration op events	HOURS DURATION OF EVENTS
* -64 13 40.1N 24.9E 3019	14 39.5N 2.2E * >64
y 48 3019 1 41	N 248 3019 D 241
3019	> 34 36 19
6:1 1 3019 6:22 14 2 12 12 12 12 13 3019	F > 22 (3 5 2 2 29 29 30 19)
E > 17 55 22 4 1	E > 17 51 18 11 1 1 1 48 - 1 83 137 137 30 9 0 > 11 11 62 32 11 9 6 5 1 1 1 1 90 - 1 239 529 530 30 19
7 7 7 8 3 3 3 2 4 1 9 1 4 1 0 1 1 4 3 1 1 1 1 1 7 1 80 - 1 3 2 4 1 0 7 2 1 0 8 5 3 0 4 4	2 7 119 86 36 24 25 14 10 8 8 3 3 3 3 4 1 1 1 132-1 344 1097 1133 3030
6 12 18 24 30 36 47 48 54 60 66 72 78 84 90 96+ MAX 7E T TA TH	6 12 18 24 30 36 42 48 54 60 66 72 78 88 90 96+ MAX 7E 7 Th
HOURS DURATION OF EVENTS 16 39.8N 7.4E	HOURS DUNATION OF EVENTS 17 39.3N 15.2E
# ,64 3019 248	W 264 3019
0 241 3 3 3 3 3 3 3019	0 241
2 34 11 1	\$ 28 1 1 1 6-1 1 3019 \$ 28 1 1 1 1 2-1 2 3 3 3019
E > 22 39 16 11 9 2 2 2 7 1 54 1 83 193 193 3019 E > 17 66 22 16 11 11 5 3 5 2 4 2 72 2 147 430 434 3025	E > 22 12 2 3 18-3 17 25 25 3019 E > 17 26 10 6 3 3 3 3 3 3 3 3 3 3 3 3 3 4 3 3 3 3 3
D > 11 100 70 38 13 17 13 14 2 9 7 4 2 1 1 8 174 - 1 308 1103 1115 3038	D > 1 84 26 19 11 7 1 4 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
7 86 65 40 19 15 15 19 12 8 4 4 4 10 8 5 21 216 1 335 1814 1898 3060 2 4 56 37 23 12 10 9 9 10 4 5 4 6 6 6 6 49 300 1 252 2213 2373 3099	2 7 120 55 33 29 10 9 8 2 6 2 3 3 3 1 1 210 1 286 934 937 3046 2 4 110 53 33 19 9 15 4 13 9 3 8 3 2 2 2 2 12 288 3 16 1330 1334 3050
6 12 18 24 30 36 42 48 54 50 66 72 78 84 90 96 + MAX TE T T+ TH HOURS DURATION OF EVENTS	6 12 19 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TE T IN THE HOURS DURATION OF EVENTS
19 36.0N 0.7E	* >64 38.3N 4.1E
* >64 N > 19	>48
0 41 3019 3019 3019 3019	0 >41 1
28 8 2 3 3020	5 > 28 10 5 1 2 1 1 42 - 1 19 10 41 30 19
6 > 22 23 9 5 4 1 3 3 36 3 45 95 95 3021 6 > 17 77 25 13 7 4 4 2 1 72 1 33 284 265 3021	F > 17 66 29 17 9 5 2 4 1 1 78-1 133 289 293 3025
0 > 11 11763 50 19 16 7 7 11 5 3 1 1 2 174 1 298 882 885 3055 2 11864 35 29 19 26 18 11 10 11 6 5 5 5 2 2 13 186 1 370 1636 1664 3063	0 211 10 65 30 31 16 12 9 1 5 5 3 1 1 1 1 1 1 174 - 294 921 935 3054 2 7 98 59 42 29 21 22 21 11 8 5 6 4 6 4 2 17 186 - 1 365 165 165 1737 3065
. 4 62 47 23 18 17 17 6 5 14 12 13 11 7 3 5 32 318-1 292 2060 2139 3091	2 4 67 36 29 18 15 16 13 10 6 15 4 5 9 4 9 36 258-1 292 2079 2187 3079
6 12 18 24 30 36 42 48 54 60 66 72 79 84 90 96 4 MAX TE T TO THE THE HOURS DURATION OF SVENTS	6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TE T THE HOURS DURATION OF EVENTS

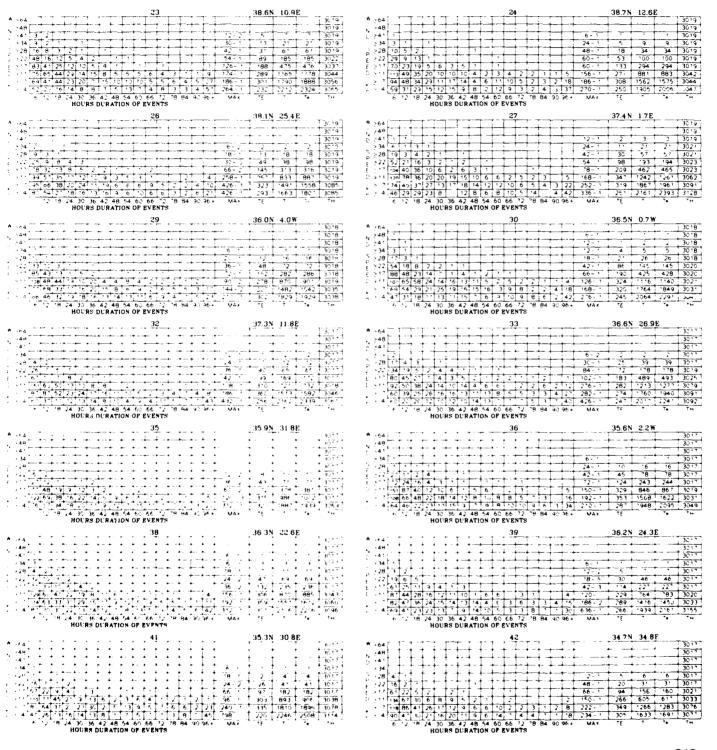
WIND SPEED DURATIONS

		3		42.3N 4.5E	
43 3N 15 3E	₩ ≥64	TTTTT	1 1 1 1	42.31 4.32	3019
3019	>48 1	1 1 1 1	6-1	1 7 1	1 3019
3019	0 241 4 3	 	12-3	7 10	10 3019
6-1 1 1 3319	>34 15 1 1 2 1		30 - 1	21 34	34 3019
18-1 3 5 5 3019	2 > 28 34 7 5 4 1	1 2	48-	54 112	112 3023
36-1 17 25 25 3019		3 1 1 2	1 1 96-1	121 316	316 3027
42-1 41 83 83 3020	F : X Y Y Y X X X X X X	7 5 2 2 2 2 2	1 2 102-1	207 613	614 3031
72-2 131 300 301 3030		18 11 5 3 6 5 3 13 8 6 7 10 3 8	2 1 14 234~1		1351 3052
4-1 231 683 688 3038			5 6 32 240-1 2 6 47 372-1		2009 3071 2269 3072
138- 258 863 868 3043 4 36+ MAX TE T T# TH		8 7 5 10 12 1 7 2 48 54 60 66 72 78		TE T	7* TH
. 30 + MHY - 15 14 10	HOURS DU	RATION OF EVENTS	04 90 90 7 MAA	12	,
41 6N 37F		6		41.9N 8.1E	
41.6N 3.7E	W >64			71.5% 0.15	3019
6-1 3019	. >48		† † † † † † † † † † † † † † † † † † †		3019
6-1 1 3019	5 341		6-1	1 1 1	1 3019
6-3 3 3 3019	> 34 4 2		12-2	6 8	8 3019
12-3 10 13 13 3019	> 28 29 7 3		18-3	39 52	52 3019
42- 3" 53 53 3619	E >22 57 14 16 6 1 1	`	60-1	98 193	193 3026
90-1 108 174 174 3019	E : 1 1 2 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	1 5	1 96-1	162 409	409 3034
		15 4 8 3 2 1 2 16 13 9 6 9 3 3	1 2 7 138-1 6 3 17 246-1	267 959 308 1606	960 3049 1609 3072
5 216-1 396 1560 1595 3026 5 3 324-1 304 1993 2059 3035	76 61 35 20 15 16	16 13 9 6 9 3 3 9 6 9 6 12 4 7			1609 3072 2076 3095
1.96+ MAX TE T TH TH	6 12 18 24 30 36 4	9 6 9 6 12 4 7 2 48 54 60 66 72 78	84 90 96+ MAX	TE T	T# TH
	HOURS DE	RATION OF EVENTS	G. 70 70		
41.1N 5.5E		9		40.1N 1.2E	
30.9	# ≥64				3019
3 4 4 3019	>48	+ + +		↓	3019
2-5 8 13 3 3019	5 241	++++++	+++	1 . 1 . 1	3019
33 24 47 47 3019	5 34	+++++	6-1	1 1	1 3019
48- 56 133 33 3021	> 28 5	+++++	18-1	6 B	8 3019
2 162-1 206 623 624 3032	E ≥ 22 21 2 2 1 1 ≥ 17 67 14 11 1	++++++	30-1	26 36	36 3019 141 3019
13 216-2 301 1416 1422 3047		₂┆┊╽┈╽╸ ┼╷┼╶├┈	1 2 150-1	320 685	694 3044
33 420 285 2009 2068 3082	70 66 26 24 20	9 8 6 2 6 2 4	3 3 8 174-1		1451 3049
4 402-1 000 2264 2364 3099	2 > 4 103 57 47 76 20 12	13 17 12 7 7 5 3	6 2 21 192-1		1838 3054
NOTE TO A TO SEE THE S	0 12 18 24 30 36 4	2 48 54 60 66 72 78	84 90 96+ MAX	TE T	Te TH
	HOURS DO	RATION OF EVENTS			
- 40.7N 11.7E	*>64[]	12		40.6N 18.8E	3019
3019	>48	+ + + + + + + + + + + + + + + + + + + +	++-i-+	+ $ +$	3019
30'9		+++++	 	+++	3019
30:9	5 > 34	+++++	6-1	+ - + - +	1 3019
9- 7 3 13 3019	S > 28 2	- - - - - - - - -	18-1	3 5	5 3019
36 - 2 31 61 61 3019	€ 222 20 1 1	, , , , , , , , , , , , , , , , , , , 	18-1	22 25	25 3019
* * * * * * * * * * * * * * * * * * * *					103 3019
60 - 96 83 83 3020	E > 17 42 17 5 3		24 - 3	67 103	.03 30.9
90 239 609 613 3020	2 > 11 109 36 23 12 6 9	3 2 1 1 1	60-1	202 438	446 3024
90 239 609 613 3020 9 90 - 332 267 279 3045	04 69 45 26 16 10	9 11 3 7 2 1 2	1 4 120-1	202 438 310 1016	446 3024 1056 3036
# 180 239 609 613 3020 # 180 332 1267 1279 3045 354 304 1653 1692 3064	2 2 11 109 36 23 12 6 9 10 10 10 10 10 10 10 10 10 10 10 10 10	9 11 3 7 2 1 2	60-1 1 4 120-1 2 4 15 192-1	202 438 310 1016 316 1526	446 3024 1056 3036 1577 3051
92 239 609 613 3020 9 90- 332 267 279 3045	3 1 1 100 36 23 12 6 9 100 69 45 26 16 10 12 14 87 65 31 23 16 12 16 12 16 12 16 12 18 24 30 36 4	9 11 3 7 2 1 2	60-1 1 4 120-1 2 4 15 192-1	202 438 310 1016	446 3024 1056 3036
22 739 609 613 3022 4 96 332 267 1279 3045 314 304 663 1692 3664 46 War 76 78 78	3 1 1 100 36 23 12 6 9 100 69 45 26 16 10 12 14 87 65 31 23 16 12 16 12 16 12 16 12 18 24 30 36 4	9 11 3 7 2 1 2 15 11 12 5 4 5 9 2 48 54 60 66 72 78	60-1 1 4 120-1 2 4 15 192-1	202 438 310 1016 316 1526 TE T	446 3024 1056 3036 1577 3051
# 180 239 609 613 3020 # 180 332 1267 1279 3045 354 304 1653 1692 3064	9 11 00 36 23 12 6 9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	9 11 3 7 2 1 2 15 11 12 5 4 5 9 2 48 54 60 66 72 78 RATION OF EVENTS	60-1 1 4 120-1 2 4 15 192-1	202 438 310 1016 316 1526	446 3024 1056 3036 1577 3051 Te TH
39 5N 2.2E	0 31 00 36 23 12 6 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	9 11 3 7 2 1 2 15 11 12 5 4 5 9 2 48 54 60 66 72 78 RATION OF EVENTS	1 4 120-1 2 4 15 192-1 84 90 96+ MAX	202 438 310 1016 316 1526 TE T	446 3024 1056 3036 1577 3051 Te TH
39 50 613 3025 90 312 766 1279 3064 314 304 663 692 3664 45 WAL TE TO TO TO TO TO TO TO TO TO TO TO TO TO	0 11 000 36 23 12 6 0 10 10 10 10 10 10 10 10 10 10 10 10 1	9 11 3 7 2 1 2 15 11 12 5 4 5 9 2 48 54 60 66 72 78 RATION OF EVENTS	60-1 1 4 120-1 2 4 15 192-1 84 90 96+ MAX	202 438 310 1016 316 1526 TE 39.8N 5.7E	446 3024 1056 3036 1577 3051 Te TH
39 50 609 613 3025 97: 332 765 7279 7048 314 304 767 769 2064 77 39:5N 2.2E 39:5N 2.2E 30:19 30:19 30:19 30:19	9 36 31 23 12 6 6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	9 11 3 7 2 1 2 15 11 12 5 4 5 9 2 48 54 60 66 72 78 RATION OF EVENTS	60-1 1 4 120-1 2 4 15 192-1 84 90 96+ MAX	202 438 310 1016 316 1526 TE T 39.8N 5.7E	446 3024 1056 3036 1577 3051 Te TH 3019 1 3019 14 3019
39 609 613 3026 96: 332 26: 279 3648 314 304 663 692 3664 4: MAI 77 79 39.5N 2.2E 30.79 30.79 30.79 30.79 30.79	0 211 000 36 23 12 6 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	9 11 3 7 2 1 2 15 11 12 5 4 5 9 2 48 54 60 66 72 78 RATION OF EVENTS	60-1 1 4 120-1 2 4 15 192-1 84 90 96+ MAX	202 438 310 1016 316 1526 TE 7 39.8N 5.7E	446 3024 1056 3036 1577 3051 Te TH 3019 1 3019 1 3019 14 3019 45 3019
39 50 69 613 3025 97 312 32 36 379 3045 314 304 653 692 3664 77 78 3079 39.5N 2.2E 5679 30.79 30.79 30.79 30.79 76 76 9	0 211 000 36 73 12 6 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	9 11 3 1 2 1 2 15 11 12 5 4 5 9 2 48 54 60 66 72 78 RATION OF EVENTS	60-1 1 4 120-1 2 4 15 192-1 84 90 96+ MAX 6-1 6-1 12-4 30-1 47-2	202 438 310 1016 316 1526 TE T 39.8N 5.7E	446 3024 1056 3036 1577 3051 Te TH 3019 1 3019 1 3019 14 3019 14 3019 142 3019
39 509 609 613 3020 9 9: 332 762 1279 1945 314 304 653 692 3664 45 WAY 77 79 74 39.5N 2.2E 3079 1019 1019 1019 1019 1019 1019 1019 1	0 211 000 36 23 12 6 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	9 11 3 2 1 2 1 5 1 1 2 5 1 1 2 5 1 1 2 5 1 1 2 5 1 1 2 5 1 1 2 5 1 1 2 1 2	60-1 2 4 15 192-1 84 90 96+ MAX 6-1 6-1 12-4 30-1 42-2 1 90-1	202 438 310 1016 1316 1526 7E 7 39.8N 5.7E 1 1 1 3 3 3 10 14 26 45 73 142 142 380	446 3024 1056 3036 1577 3051 Te TH 3019 1 3019 14 3019 45 3019 45 3019 383 3019
39 5N 2.2E 39 5N 2.2E 39 5N 2.2E 39 5N 2.2E 50 79 60 9 10 10 10 10 10 10 10 10 10 10 10 10 10	0 211 000 36 73 12 6 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	9 11 3 1 2 1 2 2 2 2 4 5 4 6 0 66 7 2 7 8 RATION OF EVENTS 15 2 48 54 60 1 2 2 4 5 5 9 9 2 2 4 8 5 4 6 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	60-1 1 4 120-1 2 4 15 192-1 84 90 96+ MAX 6-1 6-3 12-4 130-1 3 6 196-1	202 438 310 1016 316 1526 TE 7 39.8N 5.7E 1 1 1 3 3 3 10 142 380 142 380 290 1026	446 3024 1056 3036 1577 3051 Te TH 3019 1 3019 1 3019 3 3019 14 3019 45 3019 142 3019 142 3019 1038 3026
39 509 609 613 3020 9 9: 332 762 1279 1945 314 304 653 692 3664 45 WAY 77 79 74 39.5N 2.2E 3079 1019 1019 1019 1019 1019 1019 1019 1	0 211 009 36 73 12 6 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	9 11 3 2 1 2 1 5 1 1 5 1 1 2 5 1 1 2 5 1 1 2 5 1 1 2 5 1 1 2 5 1 1 2 5 1 1 2 5 1 1 2 5 1 1 2 5 1 1 2 5 1 1 2 5 1 1 2 5 1 1 1 1	60-1 1 4 190-1 2 4 15 192-1 84 90 96+ MAX 6-1 6-3 1 12-4 30-1 42-2 31 6 198-1 3 6 198-1 5 3 19 264-1	202 438 310 1016 316 1526 TE T 39.8N 5.7E 1 1 3 3 3 10 1016 31 126 1 1 2 1 1 2 2 1 3 3 3 1 1 1 2 1 1 3 3 3 3 3 1 2 1 1 3 4 2 3 1 1 4 2 380 2 90 1026 3 12 1730	446 3024 1056 3036 1577 3051 Tr TH 3019 1 3019 1 3019 14 3019 45 3019 45 3019 142 3019 142 3019 143 3019 140 3019 140 3019 141 3019 142 3019 143 3019 144 3019 145 3019 146 3019 147 3019 148 3019 149 3019 140 30
39 509 609 613 3020 97 332 756 1279 1048 314 304 1673 1692 3564 76 3079 39.5N 2.2E 39.5N 2.7E 30.79 30.79 30.79 30.79 30.79 44 93 12 137 379 44 93 12 137 379 47 27 29 526 536 3019 32 344 197 239 529 536 3019	# 364 # 364 # 364 # 364 # 365 # 364 # 365 # 364 # 364 # 364 # 364 # 364 # 364 # 364 # 364 # 365 # 366 #	9 11 3 1 2 1 2 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1	60-1 1 4 120-1 194 15 192-1 84 90 96+ MAX 6-1 6-3 12-4 1 30-1 3 6 198-1 5 3 19 284-1 5 3 19 284-1	202 438 310 1016 316 1526 7£ 7 39.8N 5.7E 1 1 1 3 3 3 1C 14 26 45 73 142 380 290 1026 312 1730	446 3024 1056 3036 1577 3051 Te TH 3019 1 3019 1 3019 3 3019 14 3019 45 3019 142 3019 142 3019 1038 3026
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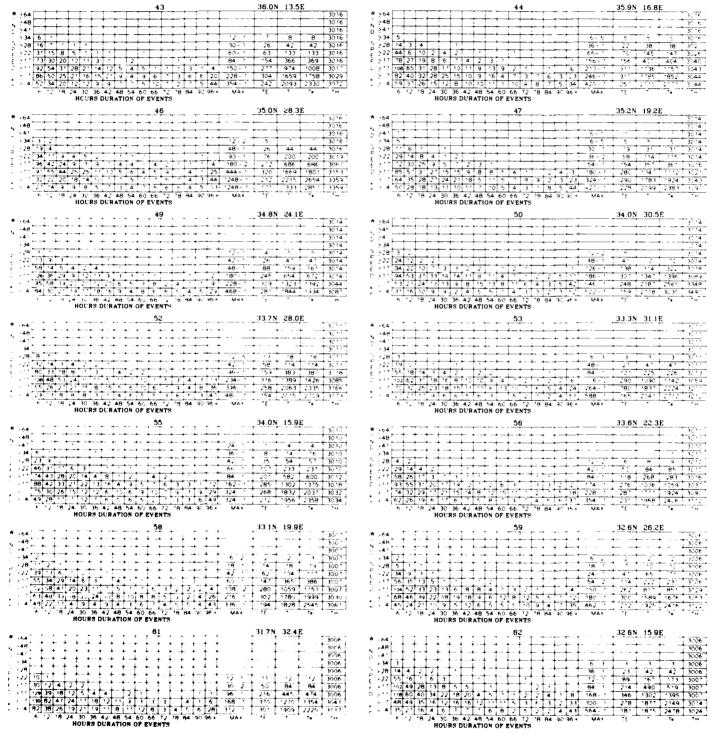
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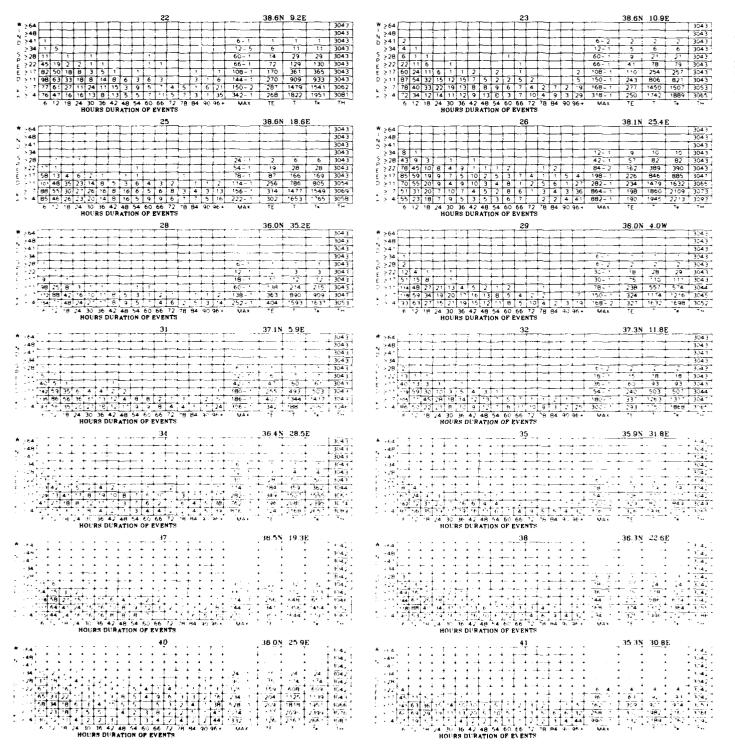
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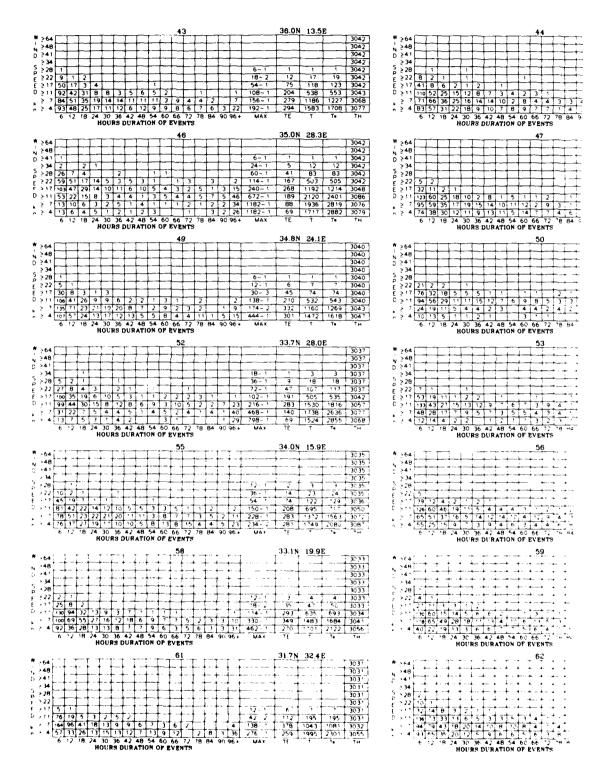
2 43.3N 15.3E	3 42.3N 4.5E
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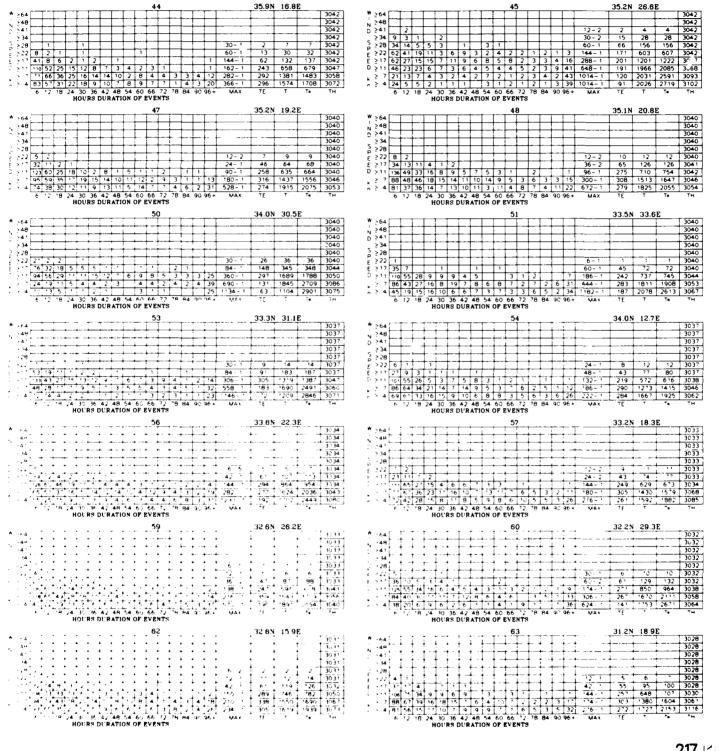
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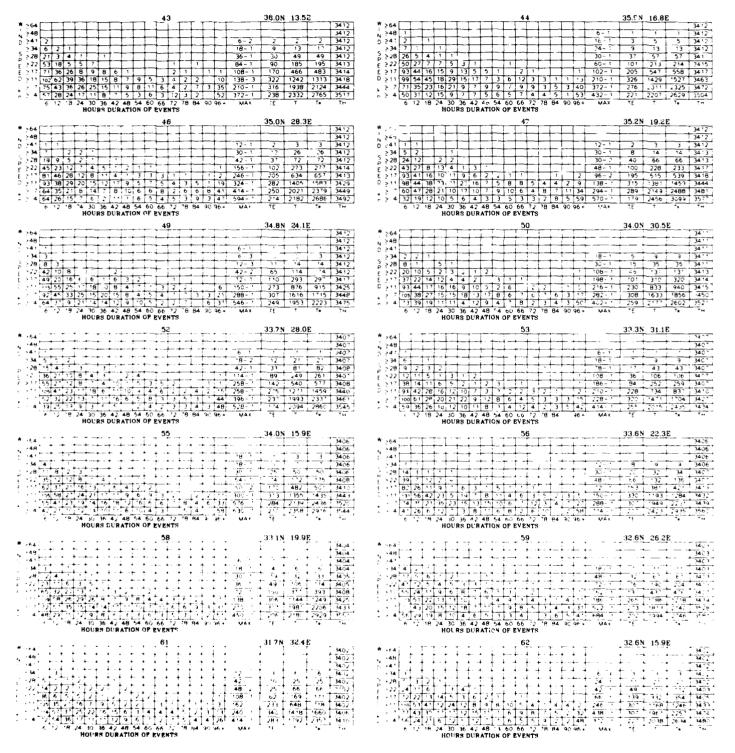
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WIND SPEED DURATIONS (Cont'd)

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WIND SPEED DURATIONS (Cont'd)

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WIND SPEED INTERVALS

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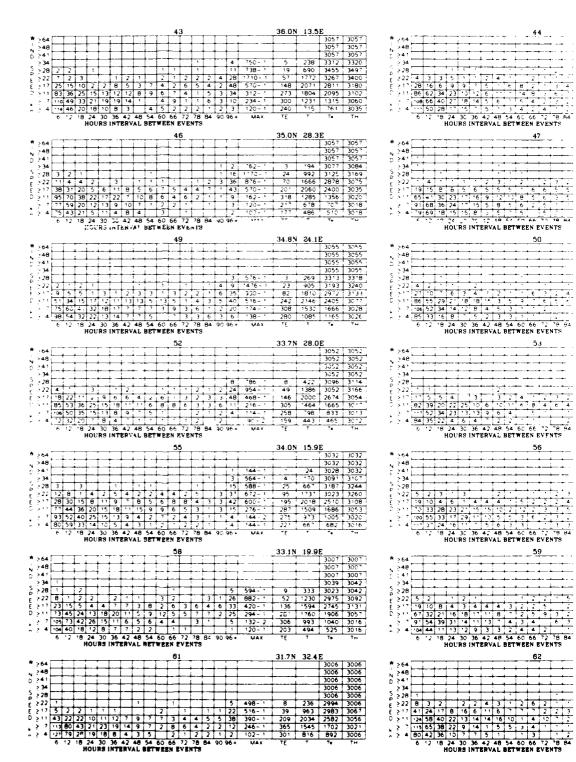
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ार रामियार सिप्ती भारतिकारमध्या स्थापना किया है है है है है स्थापन हुए उन्नी राज है उन्नी में प्रमान है है से	ু ১ প্ৰায়ং প্ৰিল্ডেইফাট্ৰপ্ৰিয়াৰ বিভাগৰ বিভাগৰ প্ৰায়েশ কৰিব বিভাগৰ প্ৰায়েশ কৰিব বিভাগৰ বিভাগৰ বিভাগৰ বিভাগ
ी अब अभिने क्यांक्टी की नामित्र के लिए हैं कि कि कि कि कि कि कि कि कि कि कि कि कि	
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िर्देश के प्रश्निक प्राप्त कराये हैं कि किस कर है जिसे किया कर है है है है है है है है है है है है है	्रिक्त के के क्षेत्र के अभिनेत्र के अभिनेत्र के किया है। इस किया किया के अपनेत्र के अपनेत्र के अपनेत्र के अपने अपनेत्र के अपनेत्र के अपनेत्र के अपनेत्र के
चित्र के प्रतिकृतिक के प्रतिकृतिक के प्रतिकृतिक के प्रतिकृतिक के प्रतिकृतिक के प्रतिकृतिक के प्रतिकृतिक के प्र - विकास सुनिक्षित के प्रतिकृतिक के प्रतिकृ	्रिक्ष के प्राप्त के प्राप्त के प्राप्त के अपने के किया है। उस प्राप्त के प्राप्त के प्राप्त के अपने किया है। अपने के प्राप्त के किया के प्राप्त के किया के प्राप्त के अपने किया किया किया है। किया के प्राप्त के किया किया अपने किया किया किया किया किया किया किया किया
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ार पर हुए अंदेरिको रहारहो हो कि सिंही से कि कि कि लिए हो पर किया किया अबेट पर है एक कि उन्हार है देवेंगर है है	32 16 7 6 12 6 5 9 9 6 5 6 3 9 38 456 1 209 2076 2530 3°C
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ုံး လူ့ မောက် ဆိုကြားသည့် ကောင်ကောက်ကြောင်းသည်။ မောက်သည်။ မောက်သည် မိန်းသည်။ မောက်သည် မောက်သည်။ မြောက်သည်။ မြေ	4 19 5 7 2 7 2 1 1 1 1 4 1 3 4 1 4 3 2 1 1 4 1 90 1 27 1 860 889 3054
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୍ର ନାର୍ମ୍ଭ କରିଥିଲେ । ଏହି ବର୍ଷ ବର୍ଷ ବର୍ଷ କରିଥିଲେ । ଏହି ଅନୁକ୍ର ବର୍ଷ କରିଥିଲେ । ଏହି ଅନୁକ୍ରି ଅନୁକ୍ରି ଅନୁକ୍ରି ଅନୁକ୍ର ପ୍ରାୟ ନ୍ୟୁ କର୍ଷ କରିଥିଲେ । ଏହି ଜଣ୍ଡ କରିଥିଲେ । ଏହି ଜଣ୍ଡ ଅନୁକ୍ରି ଅନୁକ୍ର ଅନୁକ୍ର ଅନୁକ୍ର ଅନୁକ୍ର ଅନୁକ୍ର ଅନୁକ୍ର ଅନୁକ୍ର	1 9 1 6 3 4 6 7 2 4 8 1 6 7 1 3 1 3 1 3 1 3 1 4 1 1 2 1 1 1 1 6 6 1 3 1 1 1 1 1 1 1 1 1 1 1 1		
ાં કરેડી કેમાં હોય અને હો પોલે ફહા કરા કેટલો છે. જે તેને જો જો મોટી કે પોલે કરો કરો છે. જે કો મોટી કો જો હો કે જો કરો કો માટે કરો હોય કે માટે કરો કરો કરો કરો હોય કરો કરો હોય કરો કરો હોય કરો કરો છે. જે જો હો કો જો હો કે જો	6 12 18 24 30 36 42 48 54 60 66 12 78 94 40 44 40 44		
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्डा हो बोबनी सिर्ण प्रोप्ति ने निर्णा के लिया जिस है जो है है है है है है है है है है है है है	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		
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ાં ભાગો પહોંચનો લાગે કો તેવા કે કોંગ કે કોંગ કે ફાર્યકાર તેવારો જાતના કરતી હતા કોંગ હતા. તે જીવના કોંગના કરતી કોંગની માટે માર્ચકાર કોંગની તેવા માટે કોંગની કોંગની કોંગ કોંગ કોંગ કોંગ કોંગના કરતી છે. માટે કોંગના ફાઈ સહ્યુ ક	ে ১৮০ নিৰ্দিষ্ট কৰি কুটাৰ শ্ৰীৰ কৰিব কৰি নিৰ্দেশ কৰিব কৰিব কৰিব কৰিব কৰিব কৰিব কৰিব কৰিব		
and the first of t	그는 그 교육화원 한 경우 한 나는 나는 하는 하는 하는 하는 하는 사람들이 눈을 가는 수 있는 그 사람들이 하는 하는 사람들이 느낌들이 느낌들이 느낌들이 느낌들이 느낌들이 느낌들이 느낌들이 느낌		
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into 14. Note il Biologico il ricologico il Aliano il principali il Adio Halono il compositore di Adagai Milita Il Califa il Malifario il Aliano il ricologico il Anglia di Anglia di Anglia di Anglia di Anglia di Anglia di A	6 48 498 62 78 367 348 69 2308 346 69 2308 346 69 2308 346 69 2308 346 69 2308 346 69 2308 346 69 2308 346 69 2308 346 69 2308 346 69 2308 346 69 2308 346 69 2308 346 69 2308 346 69 2308 346 69 2308 348 69 2308 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2308 348 69 2008 348 69 2008 348 69 2008 348 69 2008 348 69 2008 348 69 2008 69 2008 348 69 2008 348 69 2008 348 69 2008 348 69 2008 348 69 2008 348 69 2008 348 69 2008 348 69 2008 348 69 2008 348 69 2008 69 2008 348 69 2008 348 69 2008 348 69 2008 348 69 2000 348 69 2000 348 69 2000 348 69 2000 348 69 2000 348 69 2000 348 69 2000		
ાં પ્રમુખ્ય કર્યા હતું. તે મુખ્ય માર્ગ કર્યા છે. જે મુખ્ય કરી કરાયું કર્યો છે કે કે કે કર્યા કર્યા કર્યો છે. જે	and the contract of the contra		
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65 98 61 8E	36 35.6N 2.2W 1
65 98	36 35 6N 2 2W 1 A 10 35 6N 2 2W 1 A 10 36 58 3
65 98 CLBE	36 35.6N 2.2W 16.5B 36.5B 16.5B
65 98 CLBE	36 35.6N 2.2W 16.5B 36.5B 16.5B
(6) (8) (1) HE	36 35.6N 2.2W 1
65 98 61 8E	36 35.6N 2.2W 1
(6) (8) (1) HE	36 35.6N 2.2W 1
(6) (8) (1) HE	36 35.6N 2.2W 1 A 10 35.6N 2.2W 1 A 10 35.6S 36.5S 3
(6) 4N 22 6E	36 35.6N 2.2W 1
(6.48 d. 8E) (6.48 d. 64 d. 6	36 35.6N 2.2W 1
65 4N CL BE 10 10 10 10 10 10 10 1	36 35.6N 2.2W 1
(6) 4N 22 6E	36 35.6N 2.2W 1
65 48 CL RE 10	36 35.6N 2.2W 1
## 10 BE 10 10 10 10 10 10 10 1	36 35.6N 2.2W 1
(6) 4N 22 6E	36 35.6N 2.2W 1

43 36.0N 13.5E	44
1 2 SEA- 2 2 736 3656 248 2 SEA- 2 2 736 3656	3656 * 48
() 241 2 SEA- 2 2 736 3693	3695
> 34 5 > 28 2 1 1 1 1 1 17 SEA - 1 23 1637 3909	3940 3958 5 28 4 1
£ 22 10 6 4 6 2 3 3 1 1 3 1 1 3 1 36 714-1 81 1805 3390	3584
E > 17 31 9 17 7 6 7 5 5 4 5 3 5 1 2 3 48 582 1 158 2095 3012 1 89 45 30 25 12 16 13 15 6 9 10 3 7 5 2 26 198 7 313 1837 2137	3493 E > 17 36 8 7 8 7 9 7 9 6 7 9 7 9 8 7 9 9 8 7 9 9 8 7 9 9 8 7 9 9 8 7 9 9 9 9
7 104 60 40 28 17 13 15 9 4 3 2 6 2 1 6 156-1 310 1124 1325	3417 > 198 58 24 32 13 11 6 5 4 5 4
6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TE T Ta	7H 6 12 18 24 36 36 42 48 54 66 66
HOURS INTERVAL BETWEEN EVENTS	HOURS INTERVAL BETWEEN EV
# >64 35.0N 28.3E	Taran 47
2 SEA-2 2 736 3656 248 2 SEA-2 2 736 3656	3656
3 SEA-1 3 786 3644 34 1 2 SEA-2 8 1192 4047	3647
34 1 1 1 5EA-2 8 1792 4047 5 28 3 3 1 2 1 1 1 15 SEA-1 26 1495 3695	4073 376 5 28 3 2 2
= > 22 16 6 8 3 1 3 1 3 1 2 1 1 2 2 2 2 3 38 1434 - 1 88 1846 3472 = > 1 49 27 14 5 9 6 3 3 8 3 8 2 3 3 2 51 600 - 1 196 2132 2899	3697 - 22 9 7 6 7 1 5 2
0 2 2 9 3 3 9 24 15 11 12 13 7 4 7 5 7 7 3 4 3 0 228 1 286 1734 1886	3452 > 1 8 49 41 28 14 6 8 9 4 6 6 6
95 47 27 17 15 10 12 6 4 3 3 5 2 1 2 9 162 1 257 995 1077 6 4 84 47 2 17 15 5 9 6 3 4 3 5 1 3 162 1 223 772 813	34 19 > 7 124 5 1 39 17 16 10 10 6 3 3 3
6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 96+ MAX TE T To	34 19 -> 4 \(\frac{132}{34} \) 3 9 10 \(\frac{7}{2} \) 4 \(\frac{7}{2} \) 18 24 30 36 42 48 54 60 66 \(\frac{7}{2} \).
HOURS INTERVAL BETWEEN EVENTS	HOURS INTERVAL BETWEEN EVI
49 34.8 iv 24.1 b	3656 * >64 50
N 248 2 2 736 3656	3656 ≥48
2 SEA 1 2 656 3758 234 3 SEA 3 943 4132	3759 4135 234
28 1 8 SEA- 1 9 1268 3975	3989 € ≥20
22 11 8 3 1 1 2 1 1 1 2 2 362 1 53 1308 3566 2 17 17 9 4 4 2 6 3 3 4 3 5 3 3 3 1 720 1 97 1524 3222	3680 E 22 3 2 2 2 2 3 3 3 3 3 3 3 3 3 3 3 3
\$ 11 74 31 32 8 13 15 8 10 9 4 6 5 7 1 4 39 342 1 265 2140 2570	3472 0 21 52 24 22 11 9 3 10 10 9 7 5 5
35 46 35 25 16 13 11 6 6 8 4 3 10 3 14 3 2 1 301 1507 1748	3427 > 7 95 44 34 19 20 29 17 5 7 17 7 6 3427 > 4 109 55 25 26 10 9 12 6 4 3
F 1, 18 24 30 36 42 48 54 60 66 2 78 84 90 96 4 MAK TE TO HOURS INTERVAL BETWEEN EVENTS	TH 6 12 18 24 30 36 42 48 54 60 66 12
	HOURS INTERVAL BETWEEN EVE
* -64 SEA 368 3482	3482 * >64
48 SEA 368 3482	3482 248 3482 244
34 5 SEA-1 9 550 3658	36 79 > 34
28 2 2 1 10 35 5 22 8 8 4 1 2 5 2 2 4 5 31 666 74 468 3307	3656 3568 5 22 4
6 4 6 2 4 2 3 34 486 1 129 629 2904	3480 E 21" 14 2 1 3 2 3 2 1 3 3 3
85 4 1 25 20 14 1 1 5 5 1 2 4 3 4 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3436 5 22 19 5 13 12 6 7 9 1 4 5 3422 > 7 68 1 28 22 1 15 1 9 8 12 2 2
· 4 66 38 22 11 2 9 4 6 5 1 1 1 3 4 62-1 185 646 692	3414 -> 4 83 11 29 15 11 16 1 1 9 2 2 3
6 12 18 24 30 36 42 48 54 60 66 72 78 84 90 964 MAX TE T TO HOURS INTERVAL BETWEEN EVENTS	6 12 18 24 30 36 42 48 54 60 66 72 HOURS INTERVAL BETWEEN EVE
55 34.0N 15.9E	56
13481 1481 1481	348
0 141	3520 0 241
3517 34 1 3799	3806
35.17 37.34 3.26 3.27 3.27 3.27 3.27 3.27 3.27 3.27 3.27	3806 3844 5 28 2 3/28 5 22 2 3/28 5 22 2 3/28
34 34 37 37 38 38 38 38 38 38 38 38 38 38 38 38 38	3806 3844 2 28 2
351 3799 3799 3799 3799 3799 3799 3799 379	3806 3 14
351 3799 3799 3799 3799 3799 3799 3799 379	3866 3844 5 28 2
35.17 379 379 379 379 379 379 379 379 379 37	1806
351 3799 3799 3799 3799 3799 3799 3799 379	3866 3844 5 28 2
35.1 3.7 4 4 4 4 2 5 3 2 3 2 4 2 5 5 5 5 6 5 4 6 5 5 7 5 1046 3555 1055 1055 1056 3554 1055 1056 1055 1056 1055 1056 1055 1056 1055 1056 1055 1056 1055 1056 1055 1056 1055 1056 1055 1056 1055 1056 1056	1806
35.17 34 34 35 37 37 37 37 37 37 37 37 37	1806
35.17 34.1 34.1 35.17 37.9	1806
35.7 3 799 3799 3799 3799 3799 3799 3799 3	3806
35 379	1806
35 1	1806
35.1 3.7 4 4 4 4 4 2 5 3 2 3 2 4 2 5 5 5 540 - 5 2 2 2 3 3 3 1695 203 1 6 2 2 8 4 2 8 19 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1806
35 1 3 4 4 4 4 7 5 3 7 3 2 4 2 5 5 540 5 5 7 2 9 7 1 1 1 1 4 0 1 3 6 6 6 7 2 4 1 1 1 1 4 0 1 3 6 6 6 7 2 4 1 1 1 1 1 4 0 1 3 6 6 7 3 4 1 1 1 1 1 4 1 1 1 1 1 1 1 1 1 1 1 1	1806
35 379	1806
1	18066
35 1 1 1 1 1 1 1 1 1	1806b
35 379	1806
35 379	1806
35 1	1866
35.17 379 379 379 379 379 379 379 379 379 37	1806

1551

4 3 35.9N 16.8E 1.5(4 1.7 1.7 1.5(4 1.7 1.7 1.5	45 35.2N 28.6E 248
47 35.2N 19.2E 44 56 156 165 165 165 165 165 165 165 165	## 36.4 2 35.1N 20.8E N 248 2 56.4 2 736 3656
50 34.0N 30.5E 4P	33.5N 33.6E 34.8
33.9N 311E	54 34.0N 12.7E 3481 3481 3481 448
56 33.6N 22.3E 4an 3481 3481 44 30 3.6N 22.3E 3481 3481 3481 3481 44 4 3.5 6 5 7 5 7 6 3 6 5 3 3 6 1 702 14 703 3673 3658 44 5 6 7 7 5 7 6 3 6 5 3 3 6 1 702 14 703 3673 3658 48 4 30 7 2 5 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7	57 33.2N 18.3E 34.79 34.79 34.79 34.79 34.79 34.79 35.64 35.79 35.64 35.79 35.62 36.71 35.63 35.83 35.72 35.82 35.72 36.72
Second Second	N 164
82 32.6N 15.9E 34.71 34.77 34.71 34.71 34.71 34.71 34.71 34.77 3	# 764

ANNUAL

40.00 0.00	2 43.00 45.00
# `64 13079 13079	₩ ≥64
13076 13079	>48
3079	0.00-0 13074 13079
34 2 1 1 1 1 1 2 2 1 1 99.25 1 14 1312 13013 13079 5 28 3 2 1 2 5 4 3 8 11 4 7 1 79.50 1 51 2832 12912 13079	234
\$\frac{28}{5}\frac{28}{20}\frac{10}{10}\frac{5}{5}\frac{8}{16}\frac{15}{15}\frac{8}{16}\frac{32}{32}\frac{29}{10}\frac{10}{6}\frac{1}{10}\frac{67}{10}\frac{50}{176}\frac{5609}{5609}\frac{12625}{12625}\frac{13079}{13079}	> > 27 14 3 1 1 1 6 3 5 6 17 19 11 7 1 1 1 1 75 50 - 1 94 4 237 1 28 20 130 29
50.75-1 414 8364 12002 13079	$\epsilon > 17[22] 6[9] 4[28[21] 11[17[37]33[13] 5[1] [36.75-1] 206[5751[12452]13679]$
25.00-1 941 8375 10160 13079	0 > 11 (1/ 50 48 34 (09 73 51 34 75 31 8 2 40.75 - 1 626 8210 11237 13079
7 433 249 163 104 229 108 5 30 31 4 12.50 - 1 1408 6737 7421 13079	2 7 185 113 118 90 218 100 72 28 66 19 1 2 75 - 1 1014 8030 9457 13079 3 4 254 161 129 100 2227 100 65 32 52 10 16 25 - 2 1132 734 8455 130 9
25 5 75 1 2 3 4 5 10 20 30 60 90 180 360 50 MAX TE T TO TH	25 5 75 1 2 3 4 5 10 20 30 60 90 180 360 30 MAX TE T To TH
DAYS INTERVAL BETWEEN EVENTS	DAYS INTERVAL BETWEEN EVENTS
4 42.5N 6.3E	5 41.6N 3.7E
0.00-0 13079 13079	₩ >64
>48 3.30-0 13075 13079	N ≥48 2.00-0 13077 3079
2 4 7 1 105.00 1 6 971 73049 13079 34 7 5 1 5 4 3 9 15 5 8 2 9 00 - 1 75 3834 12937 3079	0.00-0 13073 13079 234 1 1 1 1 1 64 00 6 52 13059 13079
28 32 11 22 7 16 20 13 14 48 43 8 6 96 75 1 246 6895 12594 7079 22 (16 43) 37 26 63 49 43 3 92 50 4 3 52 50 544 845 8 6 8454 11738 13679 22 (16 43) 37 56 63 49 43 3 92 50 4 3 52 50 544 845 11738 13679 24 52 50 544 845 1	\$ \$28 4 1 1 1 4 1
52.50 544 8543 11738 13079	£ >22 21 6 9 9 19 7 9 10 38 30 15 5 1 1 105.00 - 1 179 598 12694 13079
17 279 13 59 44 135 89 55 49 78 32 1 2 36 25 - 1 886 8495 10304 13079	E > 17 75 44 38 36 68 48 39 35 85 34 12 3 47 75 - 1 517 8485 11958 13079
33, 96 39 22 26 08 50 34 43 5 2 23.50 - 1 186 6667 7449 13079 44 1252 139 78 163 58 36 11 12 1 10.25 - 1 1197 4360 4681 13079	D > 11 373 2 144 83 23 1 16 7 1 53 58 8 2 29 25 - 1 1353 8422 9383 13079 27 575 30 18 13 12 13 62 35 17 20 9 75 - 1 154 1 5526 5954 13679
4 80 38 85 69 110 34 70 7 8	5 4 515 243 151 79 137 37 26 8 9 7 75 - 1 1205 3705 3949 3079
25 5 75 1 2 3 4 5 10 20 30 60 90 180 360 30 MAX TE T TO TH	.25 .5 75 1 2 3 4 5 10 20 30 60 90 180 360 C MAX TE T T. T.
DAYS INTERVAL BETWEEN EVENTS	DAYS INTERVAL BETWEEN EVENTS
7 42.0N 9.9E	8 41.1N 5.5E
# 64 48	# >64 248 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
A 478 13067 13079	N 241 4 5 1 3 4 1 1 1 1 5 4 3 2 86.25 1 35 1946 12983 13079
34 1 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2	> 34 14 8 2 1 10 4 5 3 16 22 6 9 1 1 95.25 - 1 102 4776 12790 13079
28 9 1 4 1 2 5 5 6 11 8 5 6 1 1 1 75 00 1 62 2973 12927 13079	> 28 45 29 13 13 23 19 16 14 59 29 9 7 40,75 - 1 276 6242 12324 13079
22 13 8 6 7 15 11 10 15 35 34 11 2 1 76.00-1 168 5371 12650 13079	E > 22 109 48 37 22 71 44 49 38 81 36 7 3 3 3 25 - 1 545 8034 11319 13079
22 3 8 6 7 55 10 75 35 34 17 5 7 76 00 168 5371 2650 33079 151 251 2650 13079 151 2650 15079 151 2650 15079 151 2650 15079 151 2650 151 26	E 3 17 (45) (25) (6) (7) (7) (43) (7) (22) 4 (25) (6) (7) (9) (6) (46) (9805) (30.79) (9) (11) (42) (95) (26) (8) (8) (9) (9) (9) (9) (9) (9) (9) (9) (9) (9
-, > 1;3:4):77[:38[87[222]96[53]40[60[8]	> 7 410 197 101 86 157 57 22 7 9 9 9 25 - 1 246 3653 3941 3079
A 420 214 36 102 200 85 47 24 37 3 12.00 - 1 1268 6044 6696 13079	- ~ 4 (310 48 78 65 120 44 15 7 2 1) 1 1 6.25 - 1 789 (2665 2890 13079
75 - 75 ' 2 3 4 5 10 20 30 60 90 180 360 \$ MAX TE T TO THE DAYS INTERVAL BETWEEN EVENTS	.25 .5 .75 1 2 3 4 5 10 20 30 60 90 80 360 C MAR TE T TO THE DAYS INTERVAL BETWEEN EVENTS
10 40.3N 3.8E	# >64
0.00-0 13077 3079	248 1 1 3075 3079
0 00 - 0 13079	0 241
34 54 75 5 350 13063 13079 28 4 1 2 2 4 9 6 3 45.75 33 1758 13009 13079	2 34 1 1 2 4 1 3 59 5-1 2 83 3040 13679 5 28 3 1 2 2 1 3 2 6 2 7 53 50-1 39 2328 12964 13679
28 4 1 2 2 1 4 9 6 3 45.75 1 33 1758 13009 13079 F 22 27 8 7 20 18 15 8 42 38 7 4 1 96 50 1 202 5831 12725 13079	2 28 3 1 2 2 1 3 2 6 2 7 5 53.50-1 39 2328 12964 130-9 5 222 15 8 7 7 15 7 9 15 34 3 1 1 8 44.75-1 167 5679 12679 13079
95 5 5 5 8 28 73 38 4 3 7 66 38 6 3	517 81 46 31 31 66 42 28 33 80 43 7 4 4 49 50 - 1 492 8772 11964 13073
23 50 - 1 278 8367 9430 13079	8.25-1 1095 8236 9695 13079
1 523 500 101 89 234 82 43 23 18	7 333 288 145 109 240 92 51 24 29 4 13 75 1 1305 633 682C 13079 4 1900 21 139 94 204 71 34 14 16 3 10 25 3 166 4876 5248 13079
25 5 75 1 2 3 4 5 10 20 30 60 90 180 360 00 MAK 7E 7 18 TH	25 5 75 1 2 3 4 5 10 20 30 60 90 180 360 c MAX TE THE TH
DAYS INTERVAL BETWEEN EVENTS	DAYS INTERVAL BETWEEN EVENTS
13 40.1N 24.9E	14 39.5N 2.2E
* .64 	# >64 ->48 ->48 ->48
248 0.00-0 13078 13079 241 74.25-1 299 13073 13079	1, 248 0 >41 0 >00 - 0
-34 63.25-1 5 617 13052 13079	> 34
6 · 28 7 1 2 1 1 1 1 4 7 3 6 2 85.75 - 1 37 2349 12973 13079	> 28 3 2 1 1 3 1 8 6 6 4 40 00 - 1 35 18:3 13004 130 9
E > 22 29 5 7 2 10 7 7 9 34 24 10 6 1 66 25 1 151 4916 12701 13079	$E \ge 22 \cdot 16 \cdot 6 \cdot 8 \cdot 6 \cdot 14 \cdot 5 \cdot 4 \cdot 6 \cdot 22 \cdot 17 \cdot 10 \cdot 8 \cdot 10 \cdot 10 \cdot 10 \cdot 10 \cdot 10 \cdot 10 $
2 7 55 3 1 23 16 34 29 25 20 75 44 1 3 4 1.00 - 1 362 7277 12087 13079 1 100 1 175 46 154 154 155 1 10 20 4 25 50 - 1 901 8761 10283 13079	E > 17 72 32 42 19 54 21 22 21 52 45 10 4 1 98.00-1 395 7495 12234 13079 0 > 11 229 45 13 42 46 90 71 41 83 24 4 1 31.50-1 988 8798 10348 13079
22.30 40 1023 13079 26 202 162 100 268 116 57 36 49 4 15.50 1255 7400 7993 13079	27 383 234 181 95 227 109 59 32 48 5 31.35 - 13.37 3 7246 7808 13079
4 360[238[17][108[276][106][33][30][30][1][11.00-7][1333 [6339][6786][13079]	4 468 288 55 102 196 96 34 19 24 9 50 - 1383 5585 5993 130 9 25 5 75 1 2 3 4 5 10 20 30 60 90 180 360 10 MAX TE T 10 TH
25 5 75 1 2 3 4 5 10 20 30 60 90 180 360 D MAK TE T TO THE DAYS INTERVAL BETWEEN EVENTS	25 5 75 1 2 3 4 5 10 20 30 60 90 180 360 to MAX TE T THE DAYS INTERVAL BETWEEN EVENTS
16 39.8N 7.4E	W 264 1 1 1 0.00-01 130-9 30-79
0.00-0 13073 13079	>46
4 3 1 1 83.75 1 12 845 13050 13079	0 > 41 0 0 0 0 C 13077 13079
2 34 6 3 2 2 1 2 3 10 9 5 7 1 1 100.50 1 52 334 12948 13079 2 2 8 23 1 7 5 12 13 11 8 32 23 10 8 1 1 1 101.75 161 5456 12685 13079	> 34 1 1 1 90 50 - 1 3 400 13065 130 0 5 28 2 1 1 1 3 3 3 1 4 1 90 25 - 1 19 1504 13024 13079
2 22 67 33 14 12 47 29 36 29 69 44 5 4 38.00 1 389 7456 12014 13079	> 22 9 3 2 3 4 8 7 5 14 19 10 5 1 1 86.10 90 408 12863 30 9
28.25 - 1 697 8533 10806 13079	E > 17 32 21 22 11 24 22 13 17 50 29 9 4 1 4 46 50 1 254 5742 72476 13019
14.25 - 1 1227 7002 7834 13079	D > 11 122 101 73 42 78 73 55 34 93 28 4 2 38 50-1 705 8190 11116 13079
- 1 44 723 146 80 166 68 34 12 10 7.75 2 1216 4466 4767 13079 4 1866 19 55 4 131 48 14 4 4 6 6 00 1 916 2920 3115 13079	7 300 170 122 71 196 11168 35
25 5 75 1 2 3 4 5 10 20 30 60 90 180 360 00 MAX TE T TO TH	25 5 75 1 2 3 4 5 10 20 30 60 90 180 360 V MAX TE 7 TH
Days interval between events	DAYS INTERVAL BETWEEN EVENTS
19 38.0N 0.7E	20 38.3N 4.1E W .64
48 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	>48
0.00-0 13078 13079	N 241 1 40 25 - 1 1 161 13075 13079
34/ / / / / / / / / / / / / / / / / / /	> 34 1 1 3 3 1 74.75~1 9 850 13037 13079
28 2 3 1 1 1 1 1 5 4 3 6 1 1 128.25 - 1 30 2492 12981 13079	28 5 1 2 2 1 3 1 12 7 11 8 1 74 75 1 54 3606 12927 130 9
222 15 16 9 1 13 6 10 6 22 31 16 9 52.50 1 154 5917 12704 13079 2 17 6 1 43 44 22 63 48 39 20 86 52 14 1 37.50 1 492 9059 11919 13079	22 25 16 9 7 18 11 21 16 48 42 13 3 51 50 1 22 9 6564 12548 13079 5 17 100 52 37 28 76 63 35 31 88 49 7 1 32 00 1 56 7 8689 11567 13079
0 > 11 313 170 114 83 210 124 67 39 80 8 1 21 75 - 1 1211 8276 9376 13079	D > 11 317 159 129 81 227 114 56 49 70 5 1 15.75 - 1 1207 7843 8652 13079
7 444 208 191 103 234 64 41 16 20 1 1 11.25 1 1440 5724 6199 13079	> 7 475 273 186 123 233 83 29 13 6 6 75 - 1 1427 5137 5466 13079
25 5 75 1 2 3 4 5 10 20 30 60 90 180 360 00 MAX TE T TO TH	25 5 25 1 2 3 4 5 10 20 30 60 90 180 360 \$5 MAX TE 7 TO THE
25 5 75 1 2 3 4 5 10 20 30 60 90 180 360 to MAX TE T To TH DAYS INTERVAL BETWEEN EVENTS	25 5 75 1 2 3 4 5 10 20 30 60 90 180 360 @ MAX TE 7 To The DAYS INTERVAL BETWEEN EVENTS

WIND SPEED INTERVALS

	Ď.	40.2N 4.5P
43.3N 15.3E	* 264!	42.3N 4.5E
0.00-0 13079 13079 0.00-0 13079 13079	1,148	32.50-1 2 134 13063 13079
130.9 130.9		71.00-1 21 936 13015 13079
0 00 0 13074 13079 0 00 0 13062 13079	34 18 1 9 2 10 4 2 2 19 22 2 7 1 2 2 3 1 3 1 3 1 3 1 3 1 3 1 3 1 3 1 3	
0.00-0 13062 13079 13.75-1 22 2118 12996 13079	234 18 11 9 2 10 4 2 2 19 22 2 7 1 2 2 28 57 28 11 13 42 14 14 17 50 31 10 10 1	66.25-1 109 3552 12823 13079 93.50-1 298 7181 12368 13079
13.75 1 22 2118 12996 13079 1 75 50 1 94 4237 12830 13079	5 5 28 5 7 28 11 13 42 14 14 17 50 31 10 10 10 1 1 1 1 1 1 1 1 1 1 1 1 1	40.75-1 595 8151 11362 13079
75 50-1 94 4237 12830 13079		
36, 75 - 1 206 5751 12452 13079	E > 17 227 102 67 56 156 90 67 48 73 20 2 1	36.00-1 909 8090 9863 13079
40 75-1 626 B210 11237 13079	2 5 1 1 375 207 125 101 213 102 46 29 31 2 1	23.50-1 1232 6220 6928 13079
21.75-1 1014 B030 9457 13079	> 7 388 248 160 90 164 56 22 10 13	9.75-1 1151 4149 4406 13079
16.25-2 1132 7324 8455 13079	4 351 220 124 68 123 36 16 11	9.75-1 956 3173 3333 13079
(C182 362 ± WAX TE T T+ TH	25 .5 .75 1 2 3 4 5 10 20 30 60 90 180 360	DOD MAX TE T TO TH
	DAYS INTERVAL BETWEEN EVENTS	
41.6N 3.7E	6	41.9N 8.1E
0.00-0 13079 13079	*>64	0.00-0 13079 13079
1,00 - 0 13077 (3079	348 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	0.00-0 13075 13079
		85.75-1 11 1077 13057 13079
	34 1 1 1 5 2 4 9 12 2 9 1	85.50-1 53 3205 12971 13079
75 00-1 31 2652 12978 13079	5 > 28 28 9 3 3 22 11 11 13 30 29 11 12	53.75-1 182 6149 12714 13079
175 AC = 1 179 1 5981 112694 113079	2 > 22 93 24 26 18 45 32 27 17 75 49 11 3	39.25-1 420 8078 12079 13079
47,75-1 517 8485 11958 13079	17 48 61 47 28 86 64 51 34 102 42 2	20 76 1 666 9602 11067 12070
29 25 - 1 1353 8423 9383 13019	2 > 11 304 108 105 82 184 103 60 44 74 8	14 75 - 1 1072 7534 8721 13079
2 75 1 1541 5526 5054 13070	7 4 10 232 37 92 202 81 36 23 27 2	12.75 - 1 1242 5459 5983 13079
75-1 205 3705 3949 13079	4 392 180 123 72 141 49 23 9 15 1	11 25 - 1 1005 3690 3986 13079
1:18::36(X MAX TE T To TH	.25 .5 75 1 2 3 4 5 10 20 30 60 90 180 360	
•	DAYS INTERVAL BETWEEN EVENTS	•
44 AN	0	40.1N 1.2E
41.1N 5.5E	* >64 md 2 d. d	0.00-0 13079 13079
139 25 - 1 6 690 13058 13079		0.00-0 13077 13079
86 25 36 946 12983 13079	· \ \fai\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	5.00-1 1 20 13073 13079
95.25-1 102 4776 12790 13079	- ', '4 - + '	44.00-1 7 536 13053 13079
40.75-1 276 6242 12324 13079	28 5 3 3 1 3 2 1 3 6 7 4 2	65.00-1 40 2046 12995 13079
31.25 1 545 8034 11319 13079	\$ \$22!29 \$2; 10' 6 11' 10 6 13 26 28 7 5 1 1	44.00 - 1 169 4446 12747 13079
15 50 1 010 BUAS 0805 13070	= > 17 97 41 397 17 54 39 27 31 55 45 12 5 T	36 25-1 462 7971 12089 13079
16 75 - 1 1231 5863 6511 13079	11 336 78 122 68 198 118 66 37 77 19	19.75 - 1 1219 8515 9748 13079
3 75 1046 7657 704 1770	7 471 305 175 113 322 109 42 10 20 2	112 75 . 1 1482 6181 6611 13079
6.25-	4 514 313 190 106 198 7 17 13 10 1	10.50-1 1430 4814 5107 13079
1.91.360 E VAY TE T Te TH	4 (4 11) log(106 108) 73 17 11 10 1	D 00 MAX TE T TO TH
	DAYS INTERVAL BETWEEN EVENTS	
40.7N 11.7E	12	40.6N 18.8E
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	A .64	0.00-0 13079 13079
* * * * * 6 25 - 21 * * * * * * * * * * * * * * * * * *	· · · · · · · · · · · · · · · · · · ·	0.00 - 0 13072 13079
5 25 3 3074 3074 3074 3074 3074 3074 3074 30	· * ;4 · * · † · † · † · † · † · † · † · † · †	22 25 - 1
54 5 2 83 306 30 4 53 5 39 2328 2964 3079	- 14 - 14 - 14 - 14 - 14 - 14 - 14 - 14	38.00 - 1 13 673 13020 13079
53 FC 39 2328 12964 13019	28 4	68.00 - 1 42 2868 12944 13079
44.15 = 1] 161 5619 12619 13019	, +22 15 6 7 2 13 21 12 14 28 20 14 6	40.75-1 158 5134 12703 13079
44.15 1 492 8172 11964 13074	22 15 6 7 2 13 21 12 14 28 20 14 6 5 5 1 5 28 24 10 5 1 42 35 27 65 39 12 3	48 50 - 1 393 7594 12107 13079
44.5: 16. 66.79 (26.79) (37.79)	57 28 24 10 51 42 35 27 65 39 12 3	48 50 - 1 393 7594 12107 13079 21.25 - 1 960 8363 10211 13079
44 15 1 6 56 79 126 79 13 13 17 14 15 15 15 15 15 15 15 15 15 15 15 15 15	5 28 24 12 51 42 35 27 55 39 12 3 15 13 81 58 11 54 13 32 55 28 1 15 13 24 11 92 12 15 04 53 30 42 3	48 50 - 1 393 7594 12107 13079 21.25 - 1 960 8363 10211 13079 13.50 - 1 1304 6821 7586 13079
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1 152 153 154	10 10 10 10 10 10 10 10
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271

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23	38.6N 10.9E	24	38.7N 12.6E
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28 1 8 7 1 7 7 1 0 33 23 7 8 1 67 5 - 1 22 65 37 27 19 42 30 23 25 68 2 7 7 1 42 75 - 1	156 5065 12701 13079 381 7290 12073 13079	28 18 8 4 6 13 4 9 7 24 17 4 9 1 2 22 44 34 23 13 46 26 19 25 49 30 7 6	56.75 - 1 322 6189 12227 13079
30 85 60 40 0 62 48 35 92 31 3	688 8007 10909 13079	E > 17 140 72 63 35 91 43 37 36 80 31 5 3	44,75-1 636 7786 11196 13079
390 233 137 90 178 66 26 15 23 2 1 1 50 1	1147 7019 7938 13079 1140 4612 5062 13079	0 > 11 311 164 134 78 159 101 56 31 61 13 1 > 7 322 239 138 87 184 73 40 21 28 1	28.50-1 1109 7281 8525 13079 10.25-1 1183 5266 5807 13079
4 44 183 103 61 121 42 23 5 10 1	892 3:44 3351 130 91	3 4 370 '84 101 76 136 60 26 16 15	10.00-1 984 3848 4160 13079
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48 1 23.5%	6 221 13062 13079	, ≥48	0.00-0 13077 13078
34 2 3 2 1 8 0 3 4 84.50	9 288 13040 13079 42 2410 12933 13079	0 241 2 1 2 1 3 2 4 1	71.75-1 17 154 13023 13078
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322 31 65 41 12 49 39 20 21 80 35 10 6 50 25 - 1	474 7907 11654 13079	E > 22 4 7 24 2 1 7 39 26 26 21 65 48 13 7 E > 17 164 99 65 28 116 81 68 52 95 30 7 1	54.75-1 344 8396 12329 13078
27, 75 1 252, 756, 92, 73, 200, 95, 66, 17, 53, 5 22, 75 1 22, 75 1	800 8315 10031 13079 1029 6601 7145 13079	E > 17 164 99 65 28 116 81 68 52 95 30 7 1 1	32.00-1 806 9194 11107 13078 11.00-1 1369 7309 8003 13078
> 12. 56 92 73 200 93 66 77 31 7 12.50 - 12.50	1029 4621 4961 13079	> 7 474 289 147 98 213 71 26 11 11	8.25-1 1339 4822 5120 13078
5 4 213 191 115 80 111 59 24 9 13 10,00-1	935 38 5 4103 13079	= > 4 451 244 114 74 138 33 16 5 6	B 25 - 1 108 3223 3387 13078
25 5 75 2 3 4 5 10 20 30 60 90 80 360 E MAX DAYS INTERVAL BETWEEN EVENTS	TE T Te TH	25 5 75 1 2 3 4 5 10 20 30 60 90 DAYS INTERVAL BETWEEN EVENTS	80 360 € MAX TE T TE TH
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12 1 4 14 5 16 1 15 6 35 32 1 7 2 7 3 50 1 1 2 1 38 19 62 38 29 32 88 4 9 4 36 36 36 36 36 36 36 36 36 36 36 36 36	191 6108 12697 13075	E > 22 37 20 17 3 15 28 19 10 50 42 12 6	56.50-1 259 7001 12516 3075
23 104 5 1 199 120 66 42 80 1 1 1	531 8502 11890 13075 1079 8481 9554 13075	2 3 1 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	28.50-1 649 8989 11520 13075 15.50-1 1284 7992 8744 13075
12 25 - 2 12 25 - 258 110 62 22 24 4 12 25 - 2	124 637 6938 3075	2 11 341 89 115 87 254 125 57 47 64 5 7 468 272 455 121 252 89 29 13 14	8 50-1 403 5406 5780 3075
- 4 1/4/39 44 98 25 79 39 9 15 10 20 30 60 90 180 360 30 MAX	1255 5234 5594 13075 TE T T# TH	, > 4 427 231 144 81 168 51 20 8 4	7.50-1 1134 3700 3874 13075 80 360 00 MAX E T T TH
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32	37.3N 11.8E	33	36.6N 26.9E
464 480 0.25 1	13074 13074	* >64 -48	0.00 - 0 13072 3072 0.00 - 0 13070 3072
4,	62 13068 3074	N 240 - + - + + + + + + + + + + + + + + + +	41.75-1 2 169 13064 3072
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4 419,214 95 65 135 45 4 8 6 6 25	1372 5505 6053 13074	318 172 122 76 179 60 24 14 18 4 355 140 110 66 13 36 19 4 4	8.00-2 983 4105 4434 13072 7.75-1 81 2881 3092 13072
28 5 2 4 4 4 1 2 5 1 32.25 29 5 2 4 1 4 1 2 8 4 1 33.25 20 7 8 15 3 49 8 2 1 90 36 9 6 6 0 60 0 60 360 0 MA 20 8 10 10 10 10 10 10 10 10 10 10 10 10 10	1021 3202 3422 13074	4 355 40 10 66 37 36 19 4 4 1 25 5 5 75 1 2 3 4 5 10 20 30 60 90 DAYS INTERVAL BETWEEN EVENTS	80 360 m MAX TE T To TH
DATS INTERVAL BET HEEN EVENTS	25 ON 21 OF	36	
35 36 37 38 39 39 30 30 30 30 30 30 30 30 30 30	35.9N 31.8E	* .64	35.6N 2.2W
48 2 00 7 241 3 00 7	3070 13076	, 248	0.00 - 0 13070 13070
3.00 c	13068 13070 2 82 13051 13070	0 -41 - 34 1 2 1 1	0.00 - C
	5 148 13018 13076	5 19 3 5 5 5 5 6 5 5 7 4 3 5 5	66.25-1 36 1481 12972 13070
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16 90 53 32 75 70 44 4 4 88 34 3	187 5366 12520 13076 646 7736 11102 13070	F > 17 69 41 43 19 42 30 31 18 72 40 9 5	50.50 - 1 419 7758 12011 3070 22.50 - 1 1108 8595 9740 13070
· 1 289 2 6 154 18 203 97 55 35 65 6 1 2 50 - 1	1198 7284 8386 13070	3 - 11 256 74 114 59 186 110 77 29 84 18 1 - 7 184 312 186 129 257 80 48 18 25 2	11 50~ 1 1441 6320 6809 13070
4 496 230 146 82 52 65 33 7 59 7	1230 4375 4795 13070 TE THE	, - 4 451 256 142 116 194 54 31 11 9	8.25-1 1264 4478 4788 1307C
299 2 16 154 18 223 27 25 35 65 6 2 2 50		25 5 75 1 2 3 4 5 10 20 30 60 90 DAYS INTERVAL BETWEEN EVENTS	80 360 @ WAT 12
38	36.3N 22.6E	39	36.2N 24.3E
>48 + + + + + + + + + + + + + + + + + + +	13069 13069	π (64)	0.00 - 0 13069 13069
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		>28 9 5 1 5 1 3 2 10 10 4 6 2 	65.75 - 1 58 3017 12909 13069 65.75 - 1 226 5269 12473 13069
22 93 19 11 5 24 23 11 7 45 22 9 2 1 80 00 1	572 8206 11642 13069	E +17 (05 56 36 1 283 56 51 27 81 38 6 2	31 75 - 1 558 8092 11397 13069
716 (69) 11 82 220 26 70 37 72 6	1209 7919 9077 13069	2 - 11 310 155 99 56 113 106 63 33 78 8	17.00 - 1 1081 7435 8445 13069
2 488 219 175 107 249 75 29 17 13 1 10.25 1 10.25 1 6.50		7 364 228 132 85 183 75 31 20 25 4 353 193 192 48 198 39 21 6 4	10.00-1 1143 4950 5340 13069
4 460 274 29 6 144 35 7 5 5 1 6 5 6 5 0 20 30 60 90 90 360 36 0 MAX	1 1643 [3127 [1332 [13069] 11	25 5 75 1 2 3 4 5 10 20 30 60 90	80 360 00 MAX TE T Te TH
DAYS INTERVAL BETWEEN EVENTS		DAYS INTERVAL BETWEEN EVENTS	
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	13068 13068 13067 13068	, ·4B	0.00-0 13068 13068 0.00-0 13068 13068
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449	1 3668 1 3068 1 3067 1 3068 1 3064 1 3368 1 3664 1 3368 2 3 1841 1 3000 1 3368 2 3 1841 1 3000 1 3368 3 3 3 3 6 7 7 1,7 14 7 1 3368	34 1 1 1 2 5 3 1 1 2 5 3 1 1 2 5 3 3 1 1 2 5 3 3 5 1 1 1 2 5 3 3 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.00-0 13068 13068 0.00-0 13068 13068 0.00-0 13067 13068 44.25-1 177 13063 1307 70:50-1 171 120 13020 13068 53.25-1 72 13385 12887 13068 34.75-1 349 6552 12362 13068
449	13068 13068 13067 13068 13064 13068 13064 13069 161 13050 13068 13068 13069 13068 131 6377 1277 13068 131 6377 1277 13068 131 6377 1277 13068 131 6377 1278 13068	5 28 5 1 2 4 5 3 5 7 5 6 5 6 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.00-0
.49	10068 13068 13067 13068 13068 13668 13068 13668 19108 13060 13068 1911 13067 13068 1313 6372 12142 13068 1313 6372 12142 13068 1368 7368 2390 13068 1267 5058 5542 13068	34 1 1 1 2 5 3 1 1 2 5 3 1 1 2 5 3 3 1 1 2 5 3 3 5 1 1 1 2 5 3 3 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0 .00 - 0 13068 13068 0.006 0.00 - 0 13068 13068 13068 0.00 - 0 13067 13068 1306

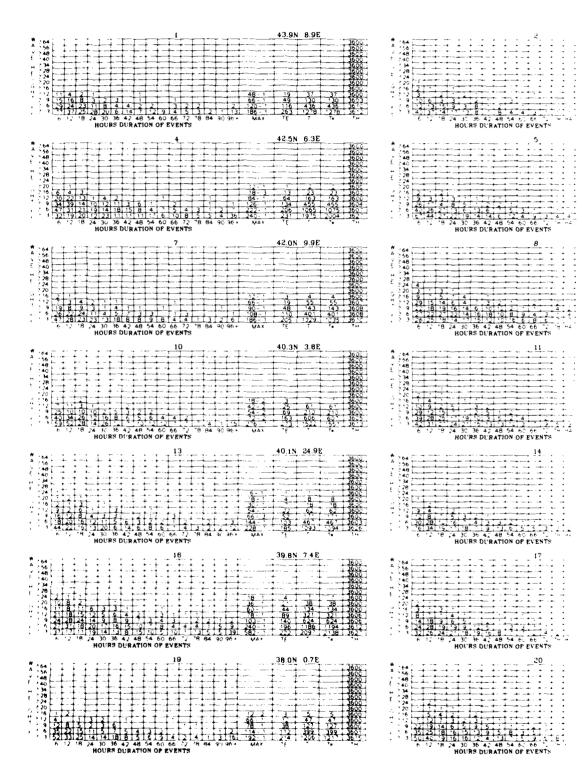
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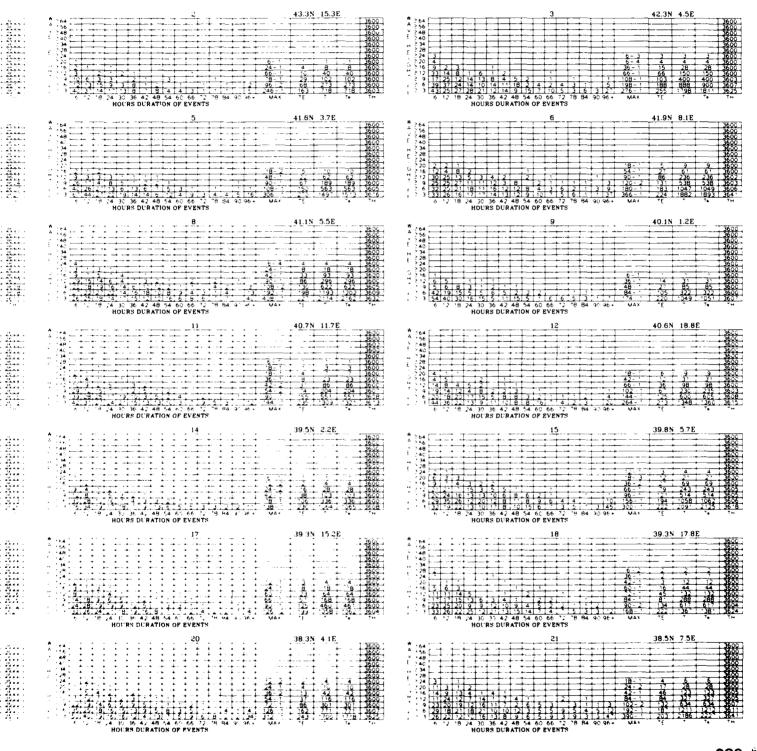
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49 34.8\ 24.1\ E	\$\begin{array}{c c c c c c c c c c c c c c c c c c c
52 33.7N 28.0E	53 33.3N 31.1E ***peak** **peak** ***peak** ***peak** ***peak** ***peak** **peak**
55 34.0N 15.9E	10
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0 1 285 6517 12313 13065	>22 115 36 36 18 5 46 37 27 86 40 2 2	59.75 - 1 496 7412 11396 13066
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	3 12 160 97 80 200 97 42 27 35 3 1	20.75 - 1 1054 5709 6310 13066
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59 45 4 4928 13066		
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35.2N 19.2E		35.1N 20.8E
1,305,311,305,4	" ⁶⁴	
3056 3053	>48	0.00-0 13059 13059
38 1304 13059	- 6 24 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.00 - 0 13050 13059
2999 1059	> 34 [[] 2 []] [] 2 [] [] [] [] []	55.00 - 1 16 840 13003 13059
15 1 90 3596 12815 13059	28 7 5 2 3 4 4 2 4 22 12 10 4 1	63.75-1 80 3543 12861 13059
296 5176 2266 3059	22 79 22 76 7 29 23 21 11 62 33 5	29.25 - 1 268 5203 12356 13059
5 = 11 607 7061 11213 13059 1	85,50,45,34,82,54,43,45,94,24,4,3	38.25 - 1 563 7633 11278 13059
	329 180 124 84 206 131 62 32 41 12 1	23.50-1 1202 7230 8147 13059
	179 180 124 64 206 131 62 32 4 2	
162 42*1 4556 13059	* 426 216 150 98 81 64 24 10 15	
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MAN TE TO THE THE	25 5 75 1 2 3 4 5 10 20 30 60 90 180 360 ¤	MAX TE T TO TH
	DAYS INTERVAL BETWEEN EVENTS	
34.0N 30.5E		33.5N 33.6E
	* .64	0 00 - 0 13056 13056
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4 15, 3029 130571	· · ; 34 +-+ + - · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · · ·	0.00 - 0 13047 13056
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	- P \$22 1214 13 1 1 1 1 2 1 8 1 2 1 5 1 8 1 6 1 3 1 1 1 1 1 1	61.75-1 76 3040 12835 13056
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5 1 1509 3763 4006 1305 T	× 370 241 194 86 229 84 34 25 24 1	11.00 1 1294 5748 6150 13050
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72 TH THE	25 5 75 7 2 3 4 5 10 20 30 60 30 80 360 7	MAX TE T TE TH
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33.3N_31.1E	54	34.0N 12.7E
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11042	48	9.00 - 0 13038
13039 13042	341	C 30 - 3 13027 13038
3 64 13022 3042	· · · · · · · · · · · · · · · · · · ·	21.50-1 10 415 12998 13038
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	2 5 1 15 4 1 14 14 16 5 4 5 2 9 3 7 5 9 3 7 4 1 7	
6032 1839 3042	E > 17 75 41 39 14 65 45 29 37 59 32 4 2	41.50-1 442 6567 11601 13038
7089 8360 3042	273 165 90 50 199 196 62 35 70 12	20 00-1 1062 7400 8634 13038
. 1069 1089 8360 13042 4289 4625 13042	> 382 24 142 130 196 5, 32 16 15	20 00 - 1 1062 7400 8634 13038 8.75 - 1 7204 4826 5306 13038
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33.6N 22.3E	2 29 24 120 120 126 15 15 15 15 15 15 15 1	20 30 - 1 1062 7400 8634 13038 8 25 - 1 1204 4826 5306 13038 5 15 1 1217 3095 1378 13038 MAY TE THE 33.2N 18.3E 5 00 - 0 13025 13025 13025 5 00 - 6 13023 13025
33.6N 22.3E 13.6N 22.3E 13.6N 22.3E 13.6N 23.6N 33.6N 99 34 14 1 1 1 0 0 0 0 5 3 2 1 6 5 4 4 28 2 6 1 2 6 2 4 5 1 C 20 30 60 90 180 360 a DAYS INTERVAL BETWEEN EVENTS 7 64 4 48 48 4 5 1 C 20 30 60 90 180 360 a	20 30 - 1 1062 7400 8634 13038 8 25 - 1 1204 4826 5306 13038 5 15 1 1217 3095 1378 13038 MAY TE THE 33.2N 18.3E 5 00 - 0 13025 13025 13025 5 00 - 6 13023 13025	
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33.6N 22.3E 13.6N 22.3E 13.6N 22.3E 13.6N 22.3E 13.6N 22.3E 13.3N 30.3N 13.3N 30.3N 13.3N 30.3N 13.3N 30.3N 13.3N 30.3N 13.3N 30.3N 13.3N 30.3N 13.3N 30.3N 13.3N 30.3N 13.3N 30.3N 13.3N 30.3N 14.3N 30.3N 30.3N 14.3N 30.3N 30.3N 14.3N 30.3N 30.3N 14.3N 30.3N 30.3N 30.3N 14.3N 30.3	99 34 14 1 1 1 0 0 0 0 5 3 2 6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	20 30 - 1 1062 7460 8634 13038 8 75 - 1 7204 4826 5306 13038 5 15 1 1017 3095 3378 13038 MAY TE THE THE TENT
33.6N 22.3E 33.6N 22.3E 33.6N 22.3E 33.6N 22.3E 33.6N 23.6 30.35 33.6N 30.35 33.6N 30.35 33.6N 30.35 33.6N 30.35 33.6N 30.35 33.6N 30.35 33.6N 30.35 33.6N 30.35 33.6N 30.35 33.6N 30.35 33.6N 30.35 33.6N 30.35 33.6N 30.35 33.6N 30.35 33.6N 30.35 33.6N 30.35 33.6N 30.35	97 A-1 (a.) (30) (98) (5) 32 (6) (5) (4) (4) (4) (4) (4) (4) (4) (4) (4) (4	20 30 - 1 1062 7400 8634 13038 8 25 - 1 1204 4826 5306 13038 5 15 1 1217 3095 1338 13038 MAY TE TH 33.2N 18.3E 0.07 - 0 13025 13025 0.07 - 0 13023 13025 5 25 - 1 3 24 13009 13025 6 50 - 1 1208 1208 13025 5 5 00 - 55 1720 12815 13025 54 75 - 739 4862 12277 13025 54 75 - 739 4862 12277 13025
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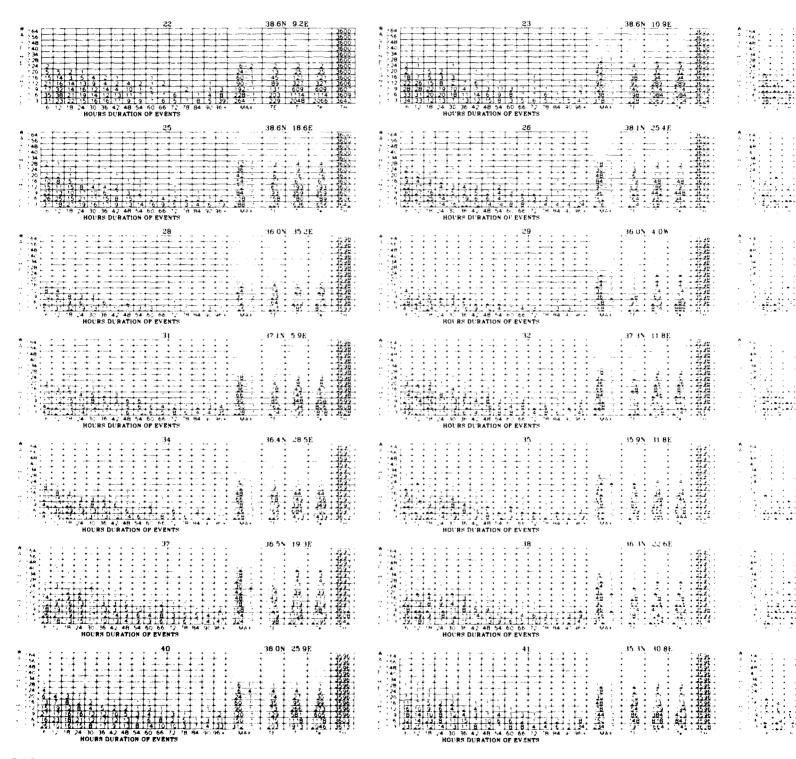


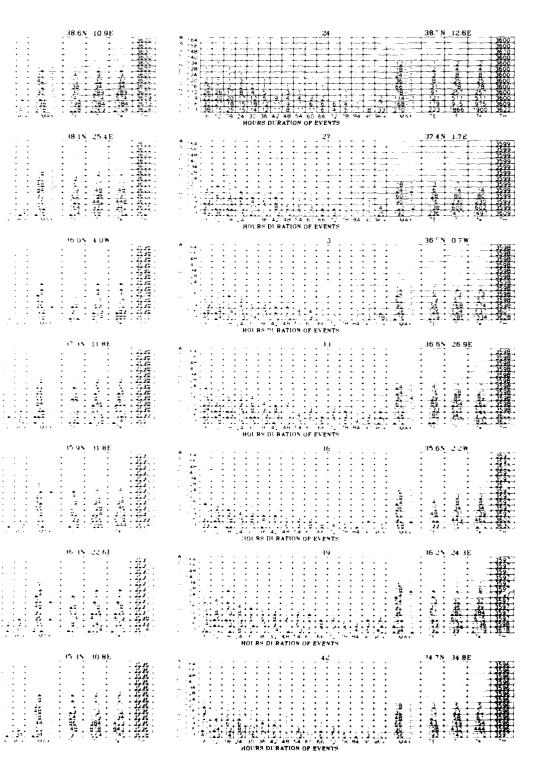
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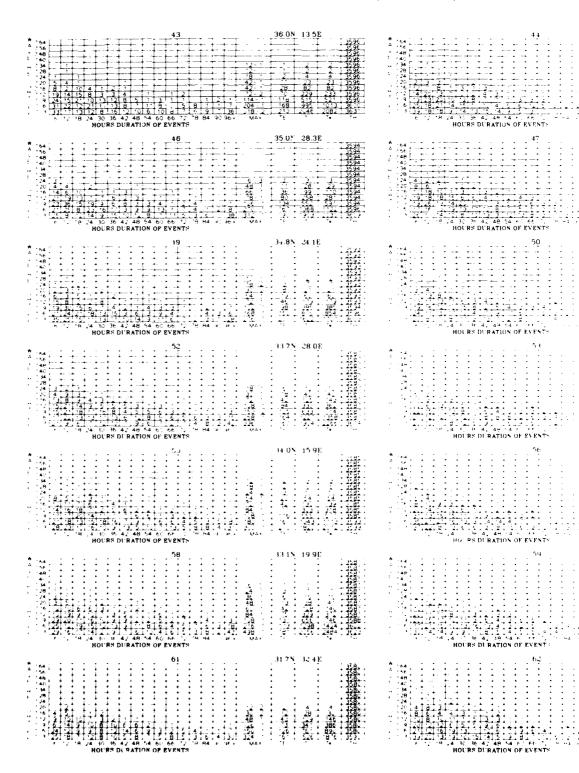
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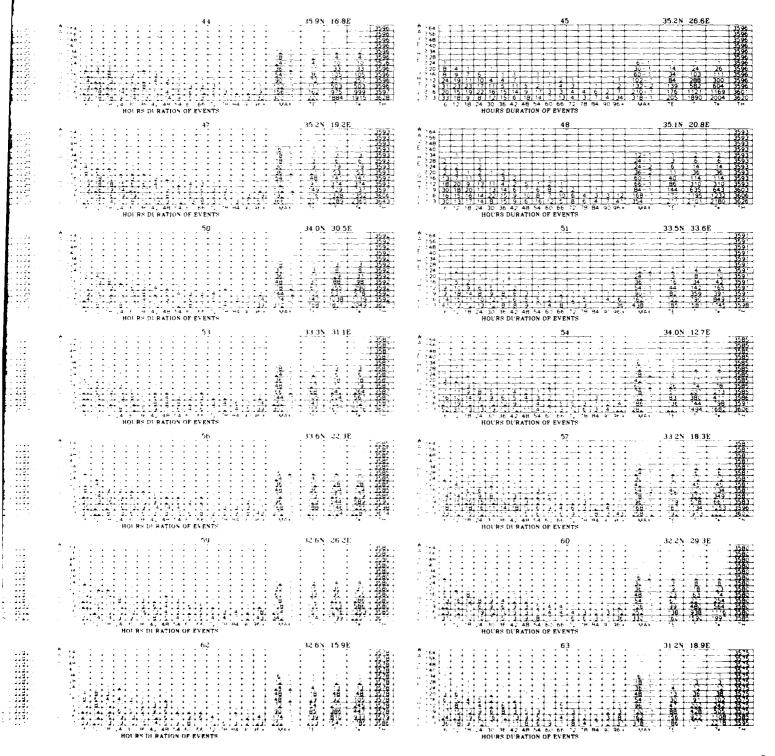


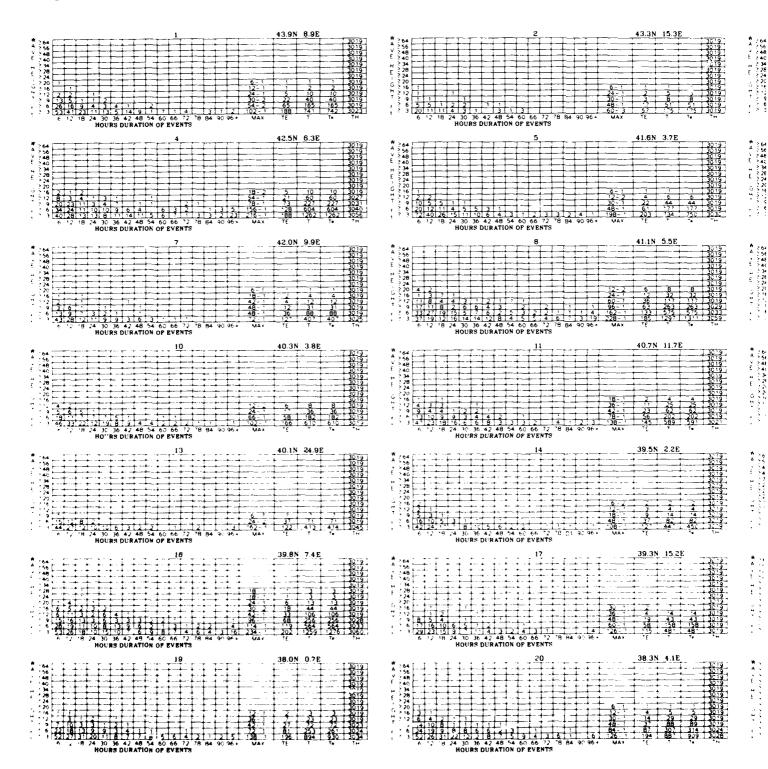
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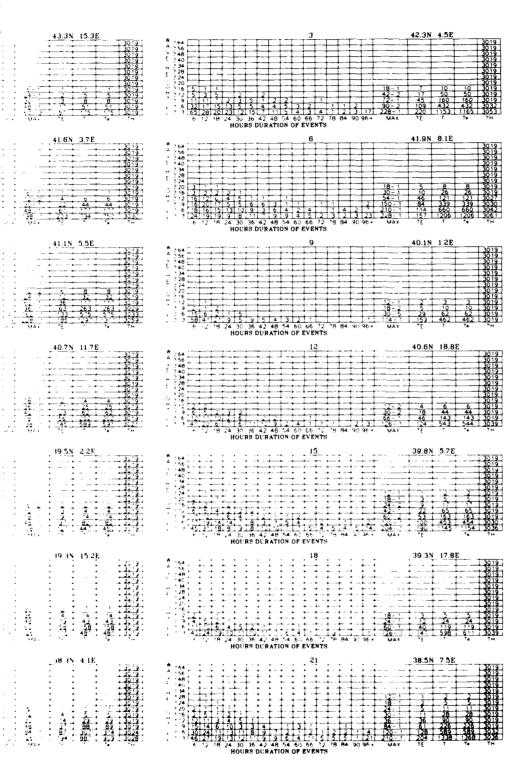
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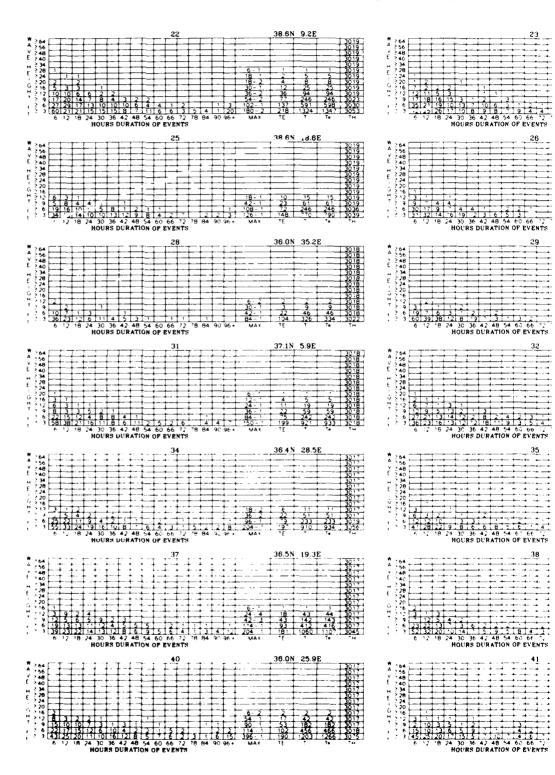




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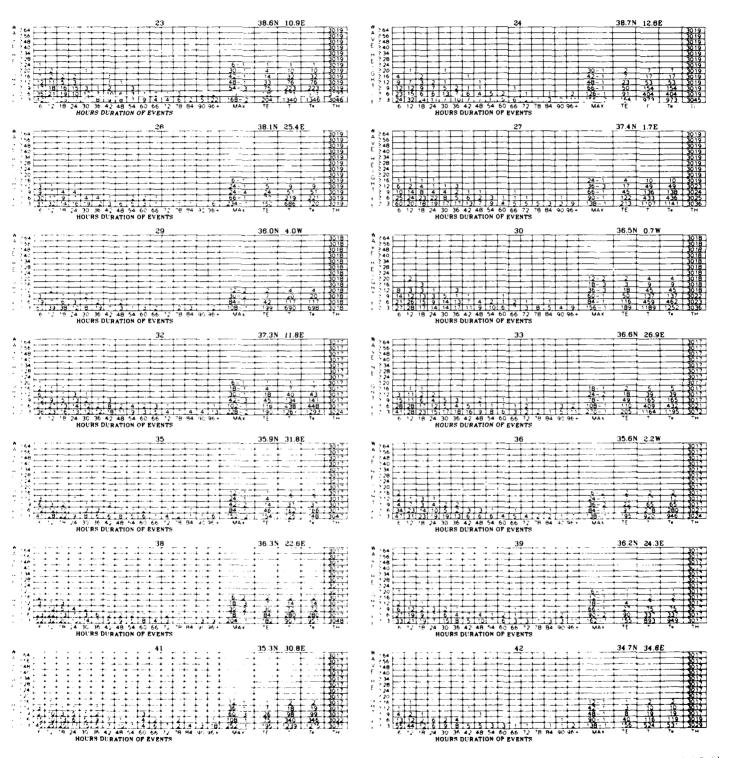


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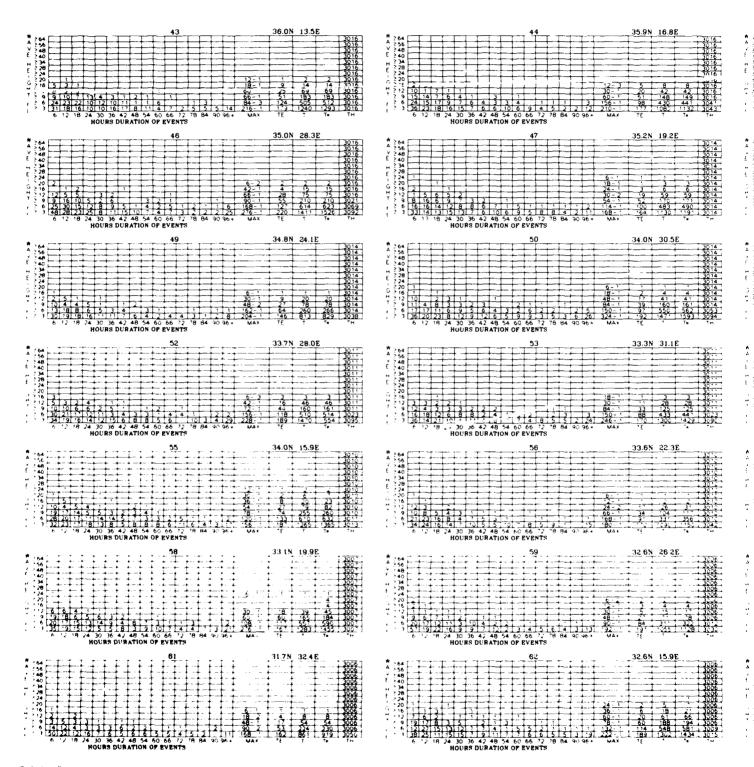
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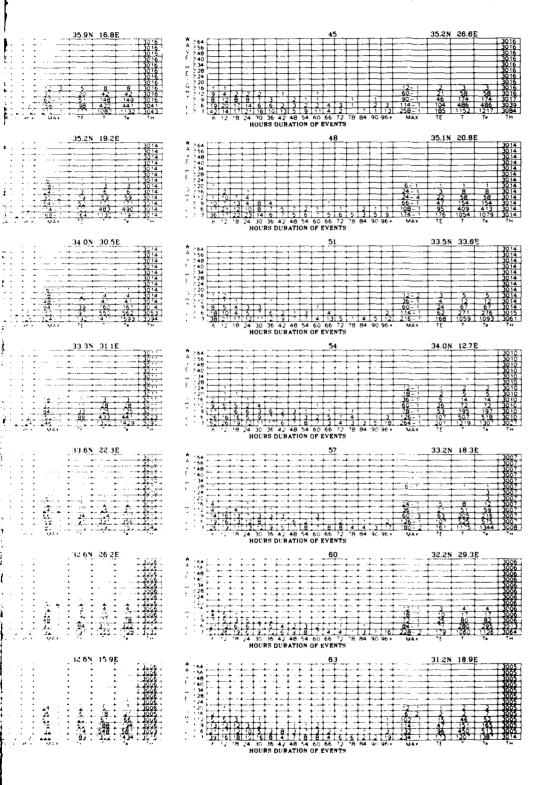
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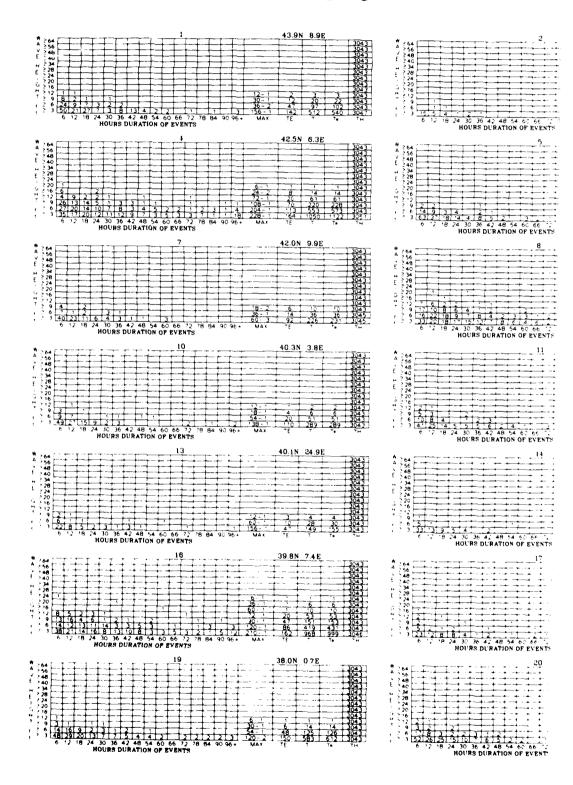
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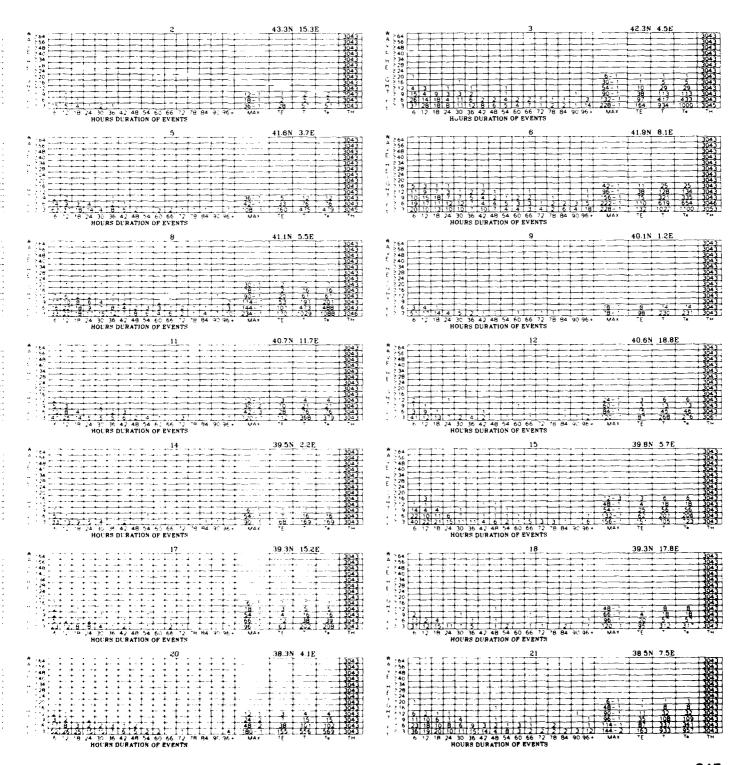


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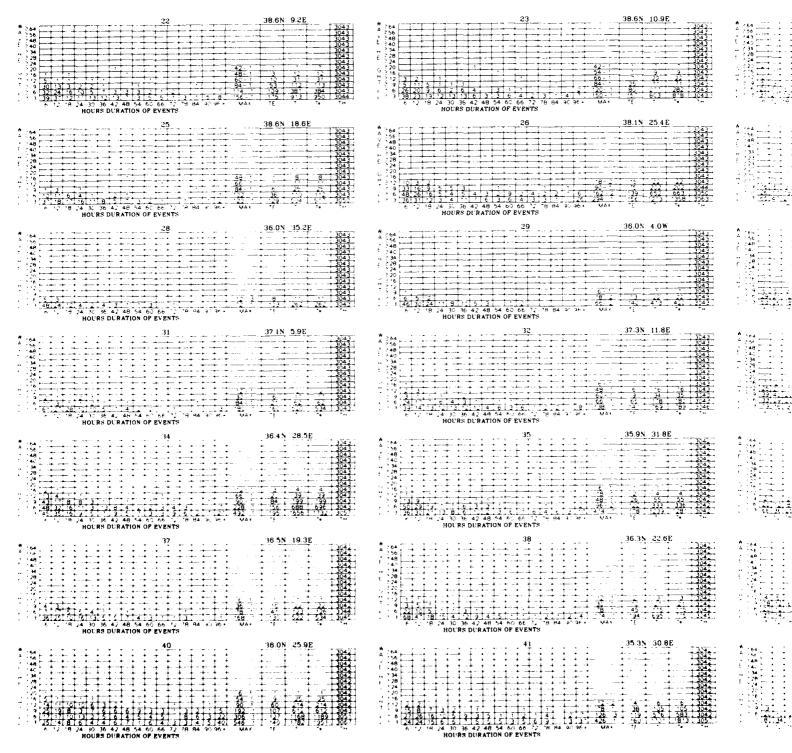


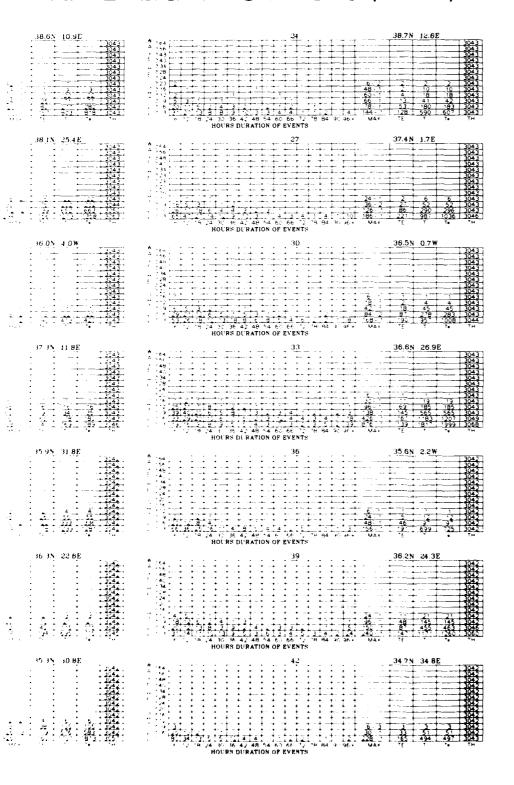
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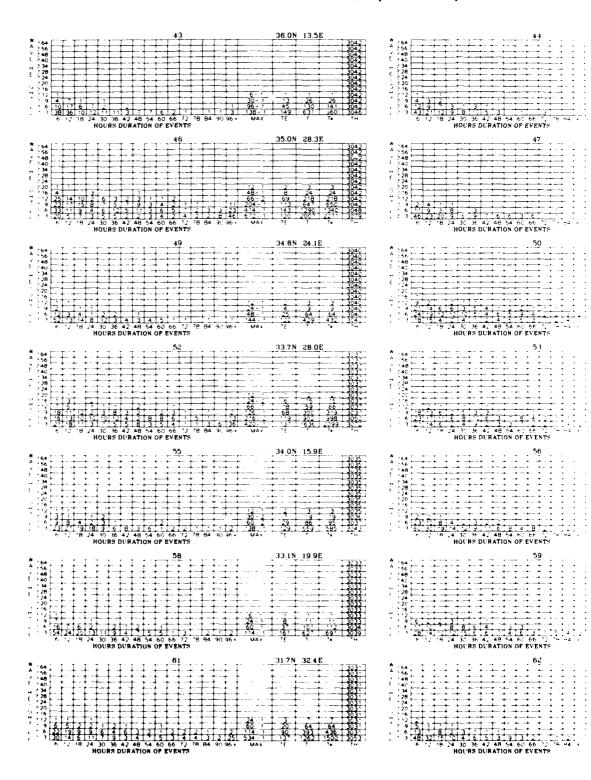
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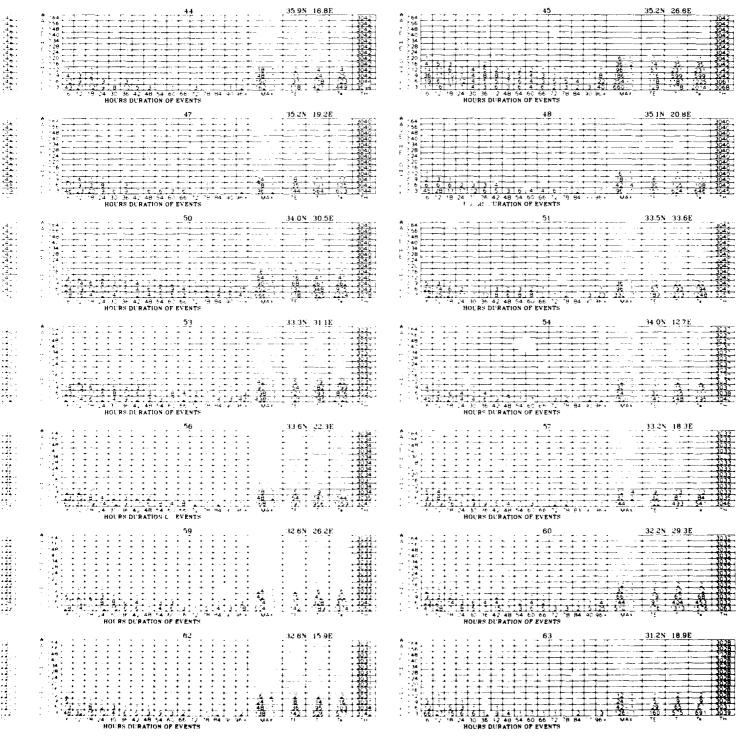


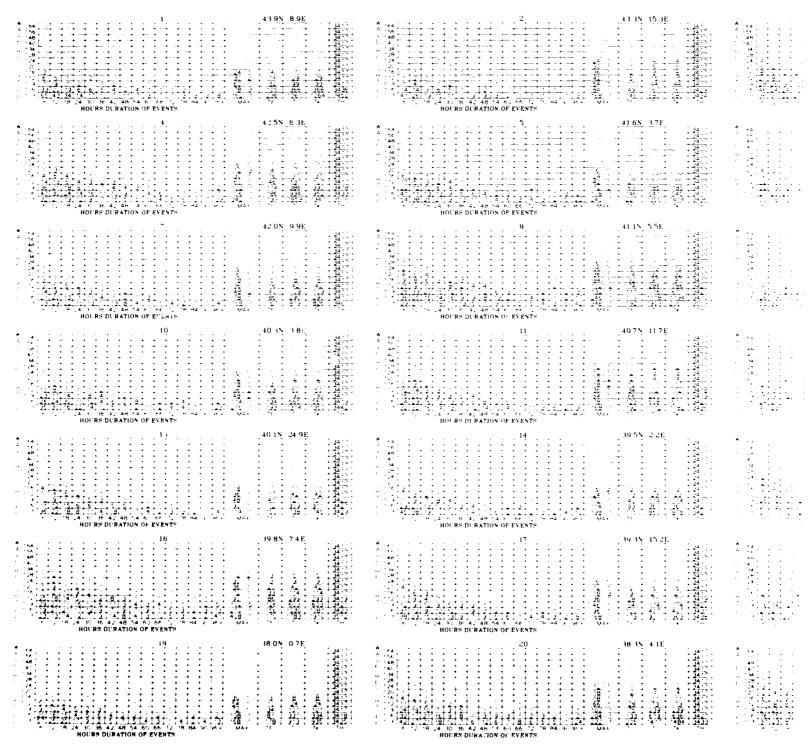
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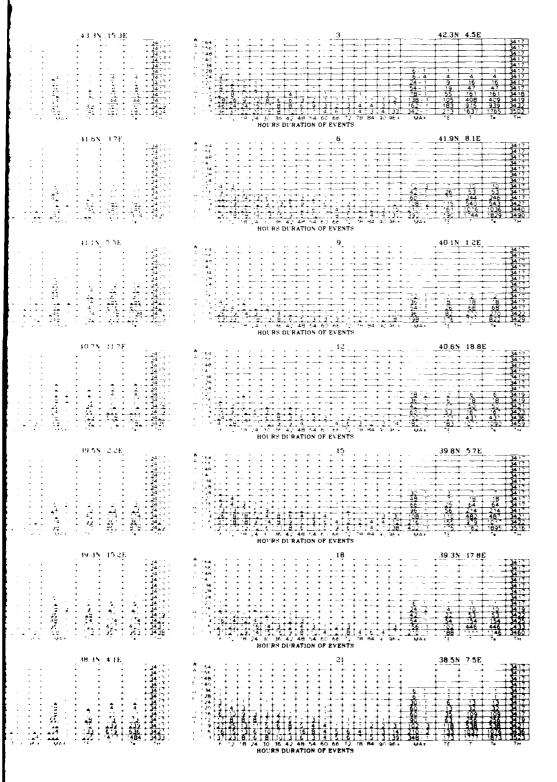
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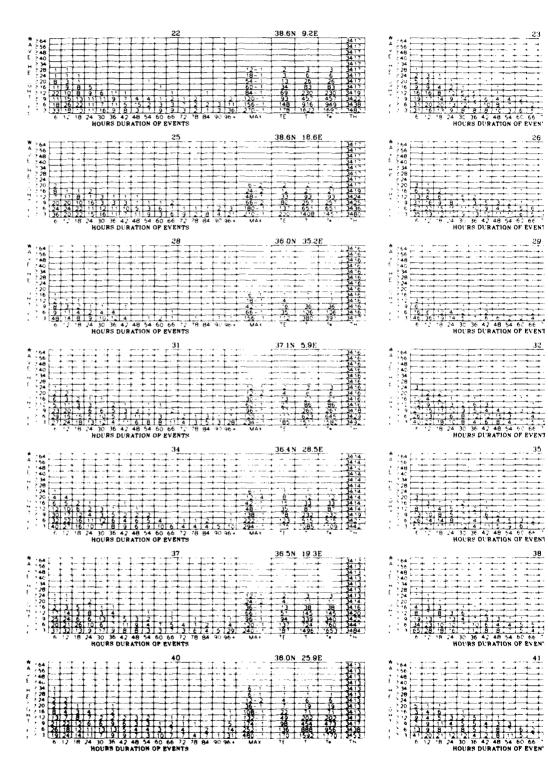




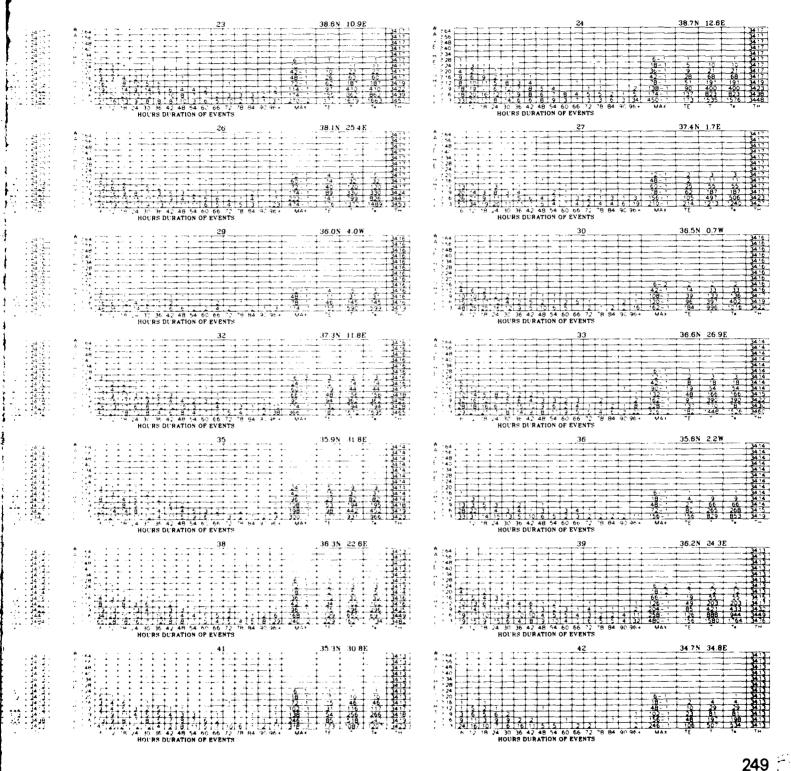
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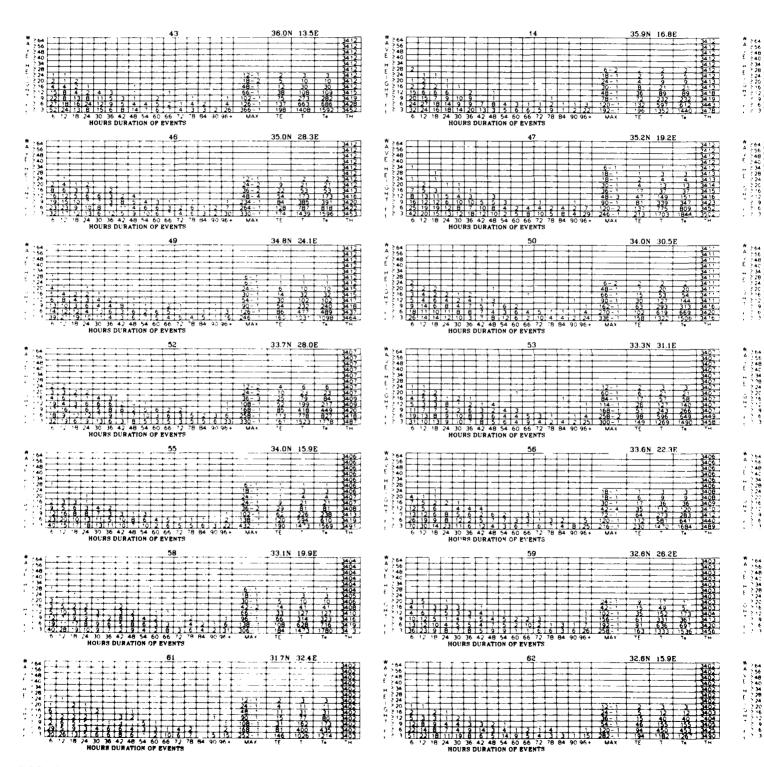


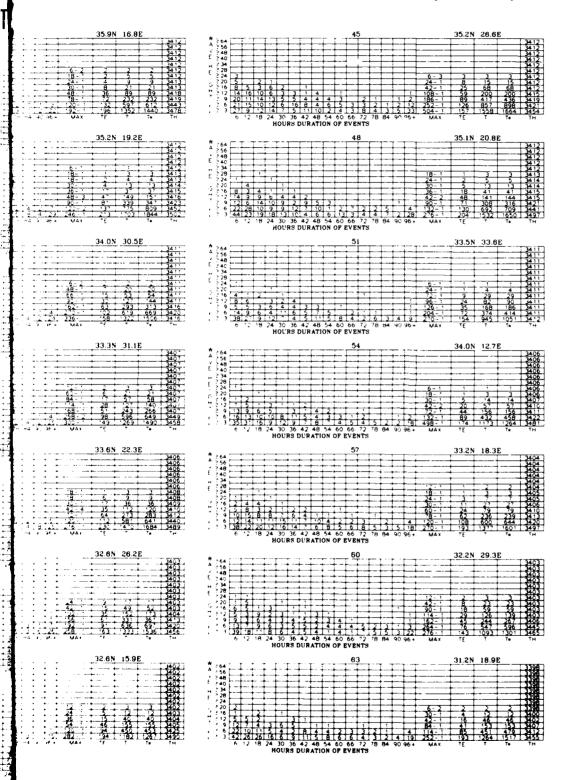
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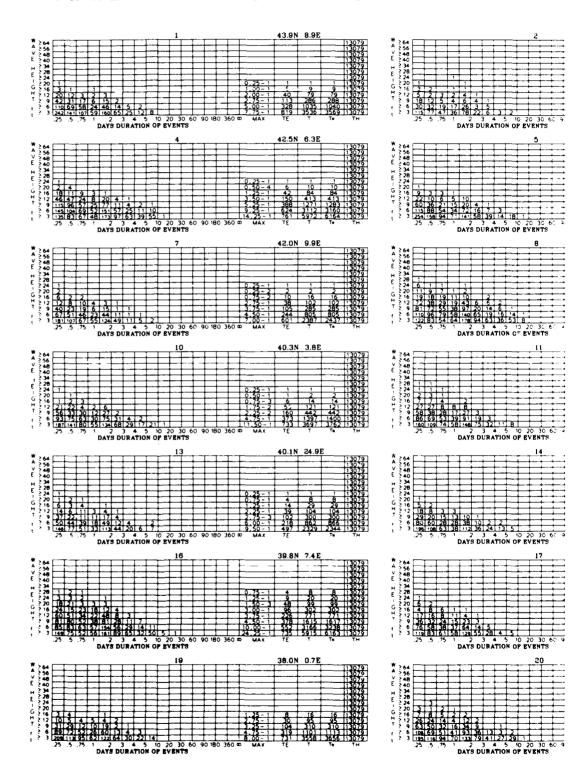
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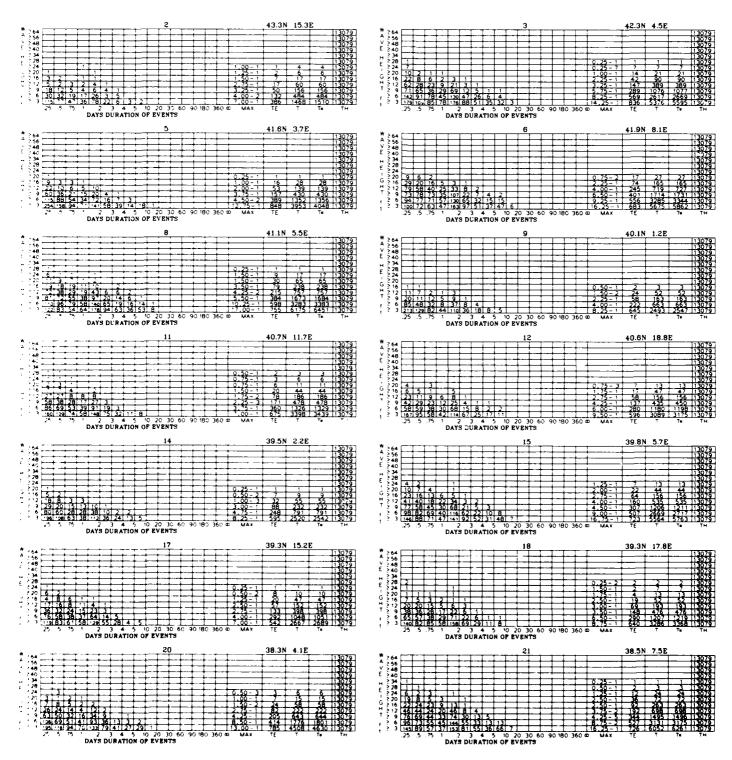


WAVE HEIGHT DURATIONS



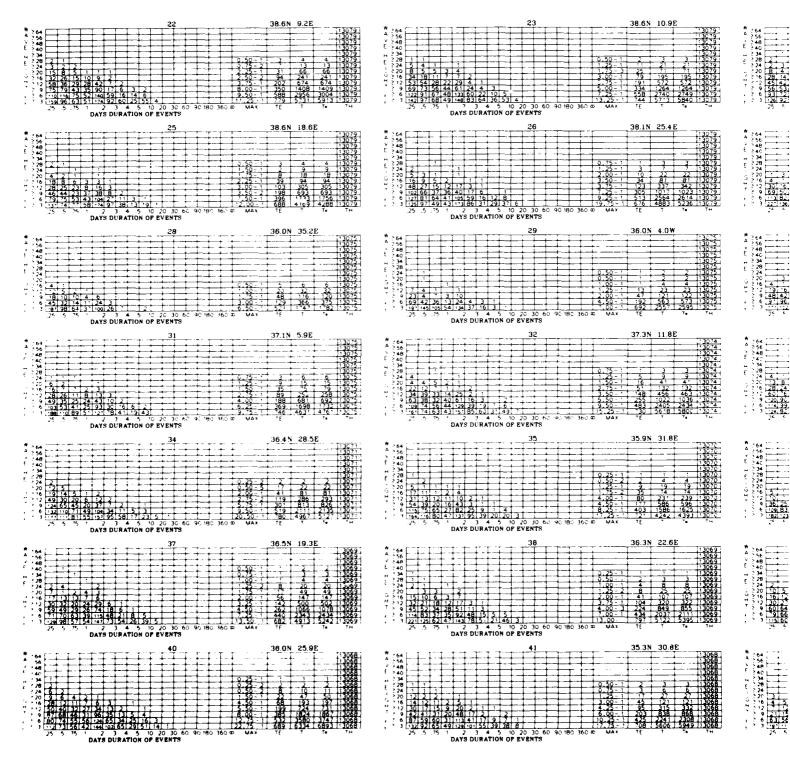
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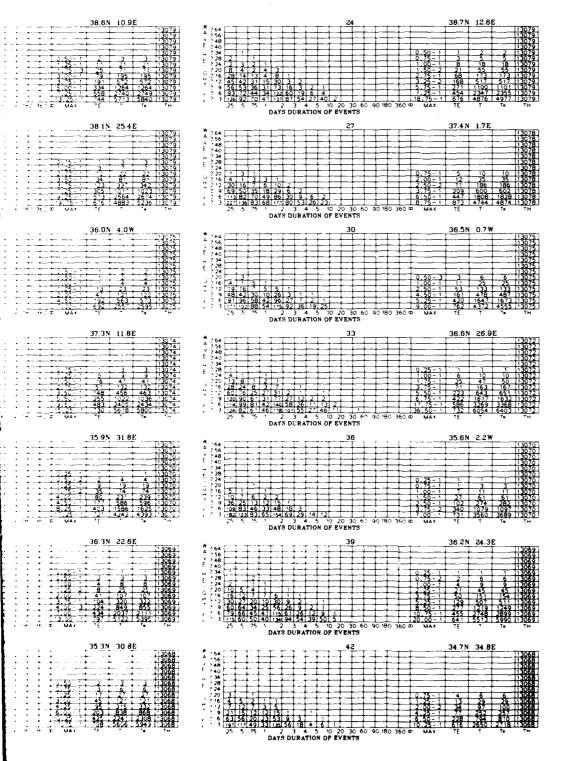
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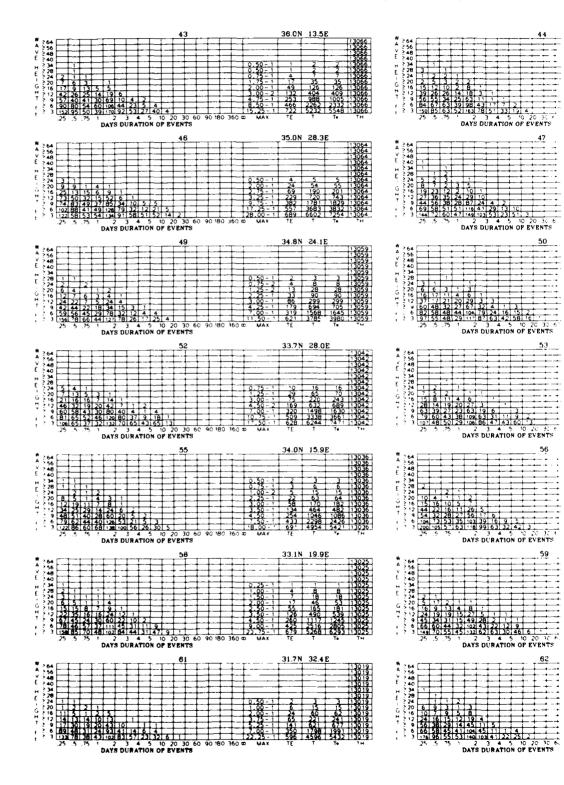


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WAVE HEIGH

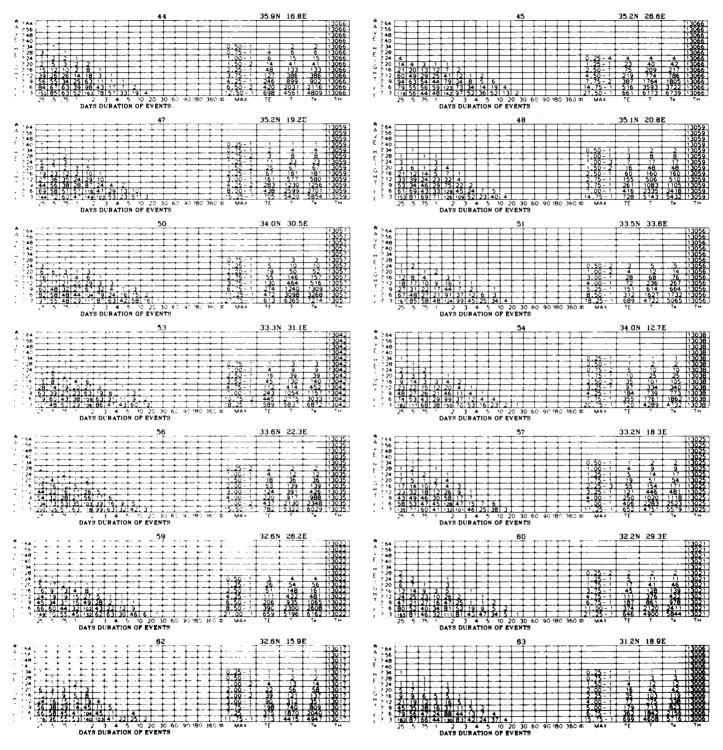




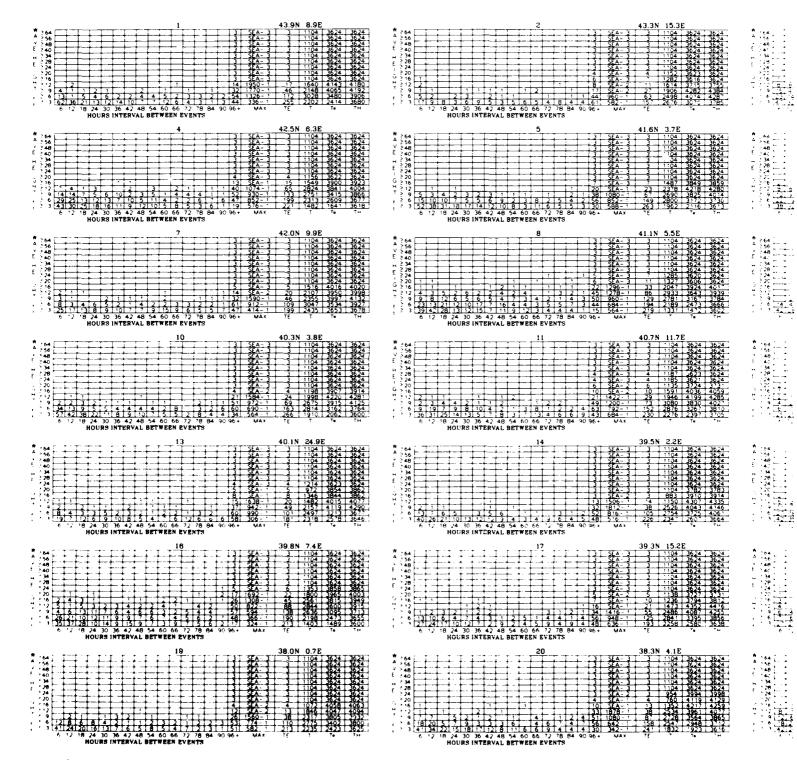


IS (Cont'd)

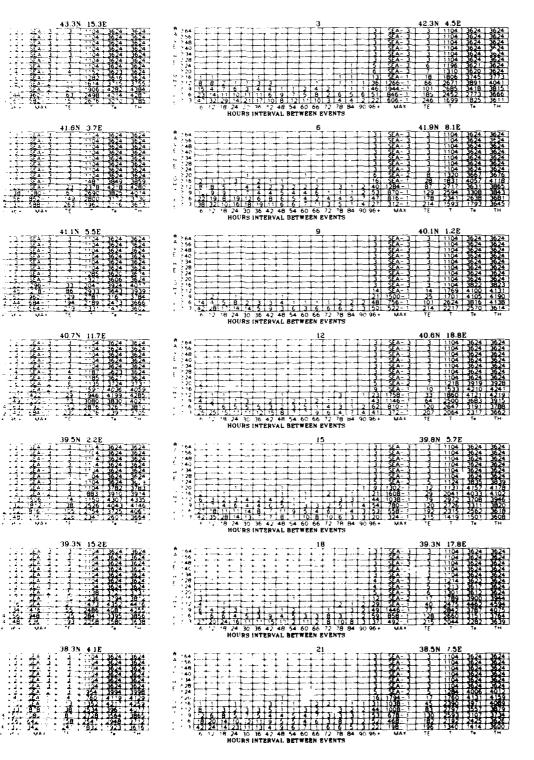
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WINTER

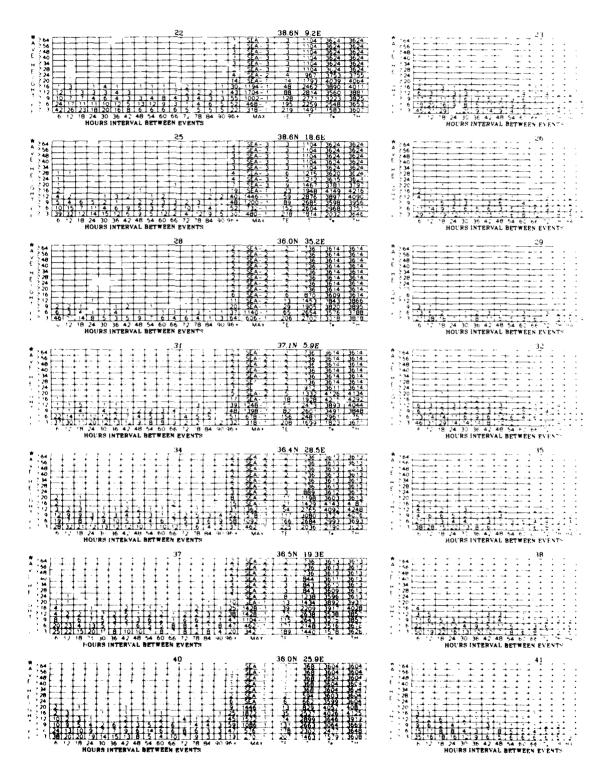


WAVE HEIGHT INTERVALS



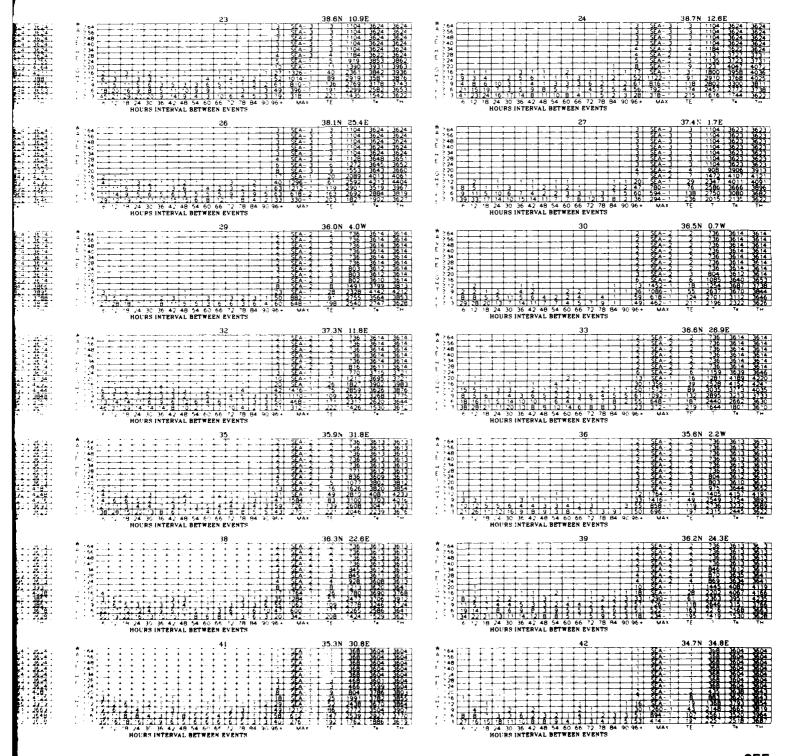
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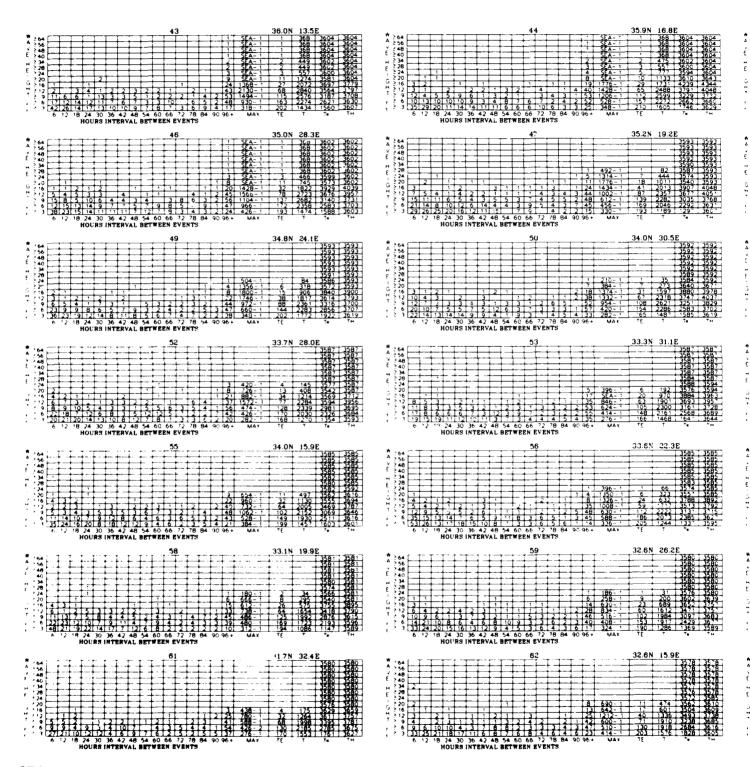


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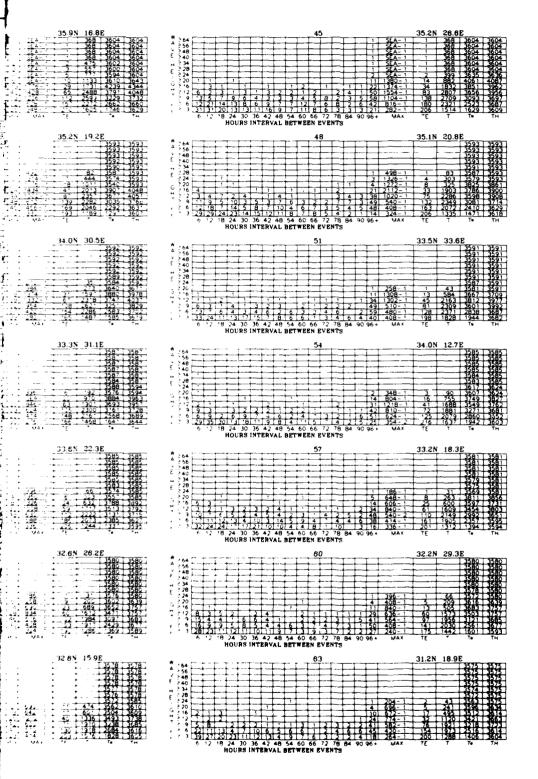
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WAVE H

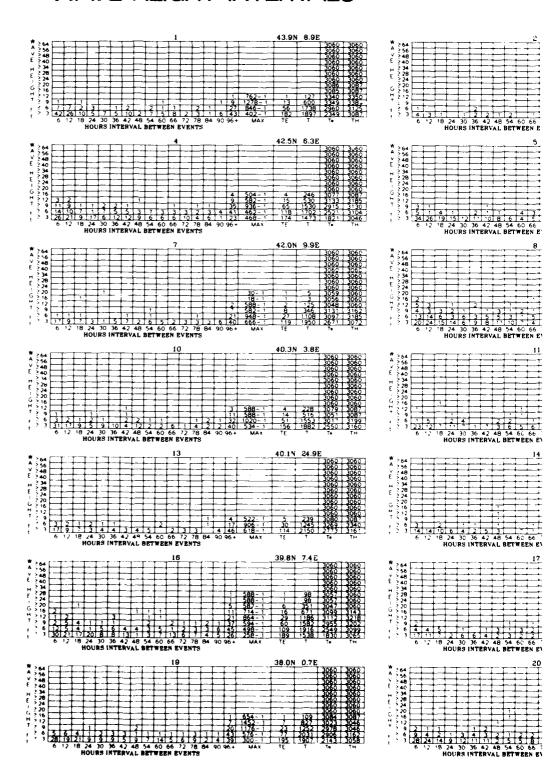


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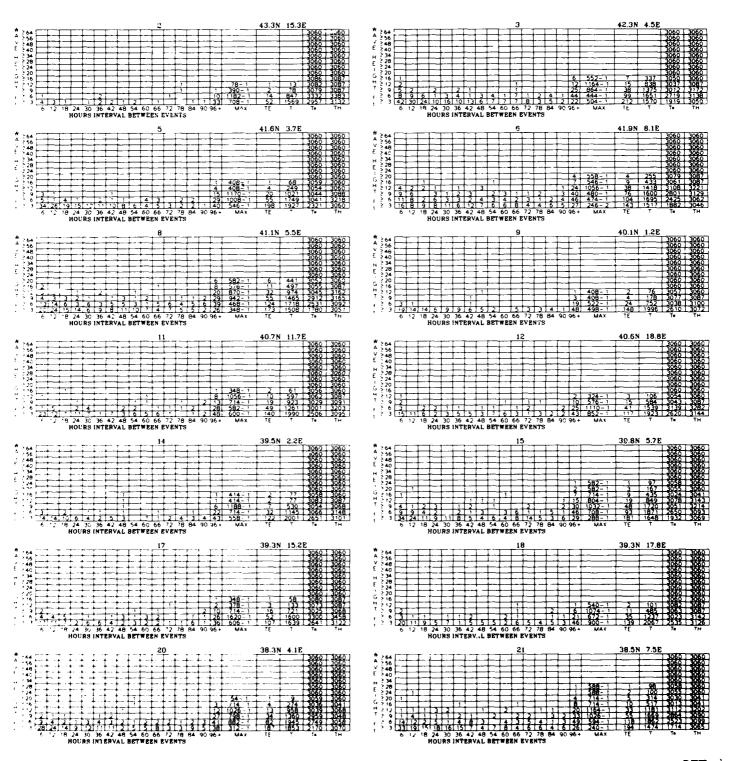


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WAVE HEIGHT INTERVALS

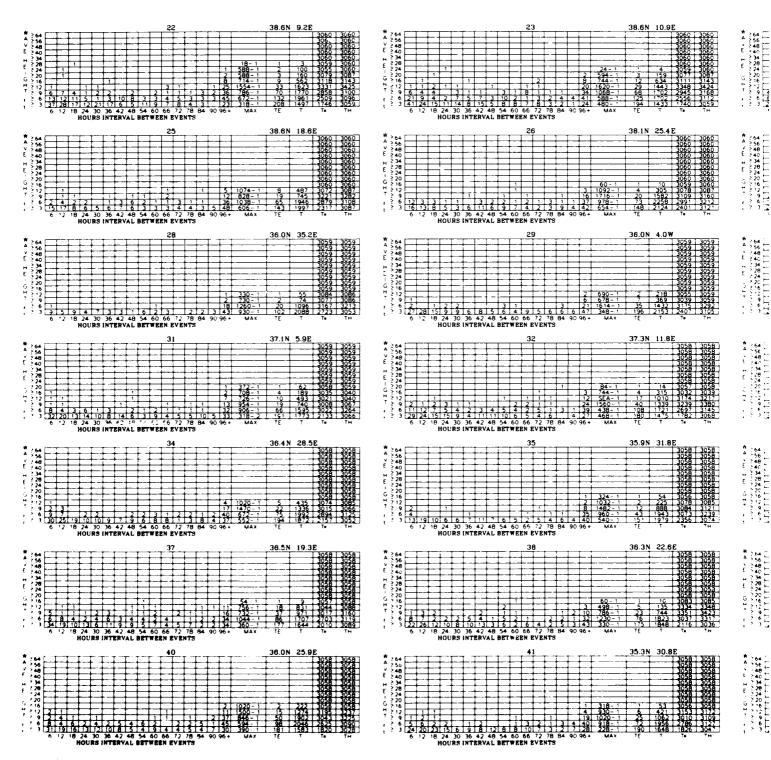


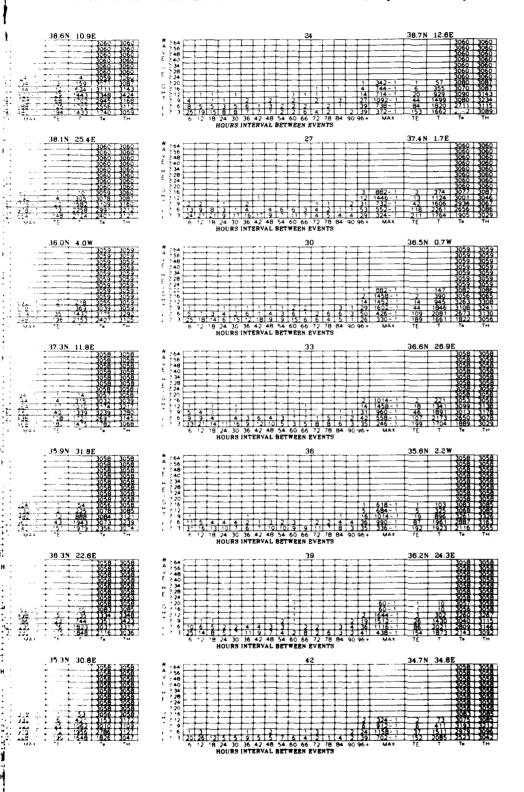
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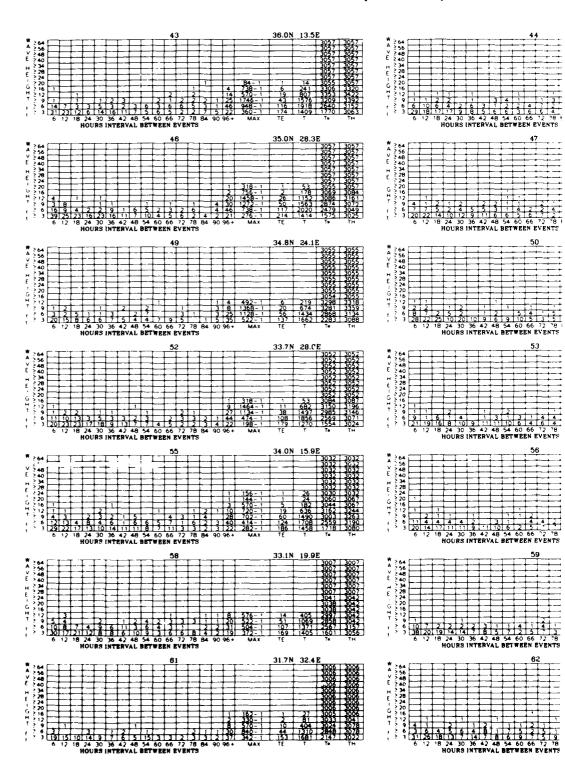


SPRING

WAVE HER

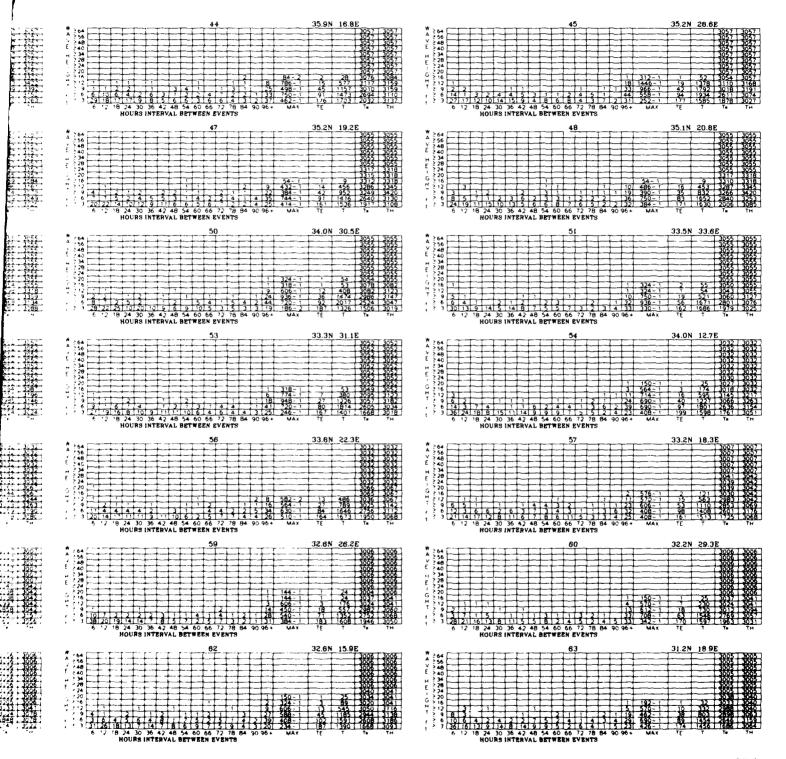




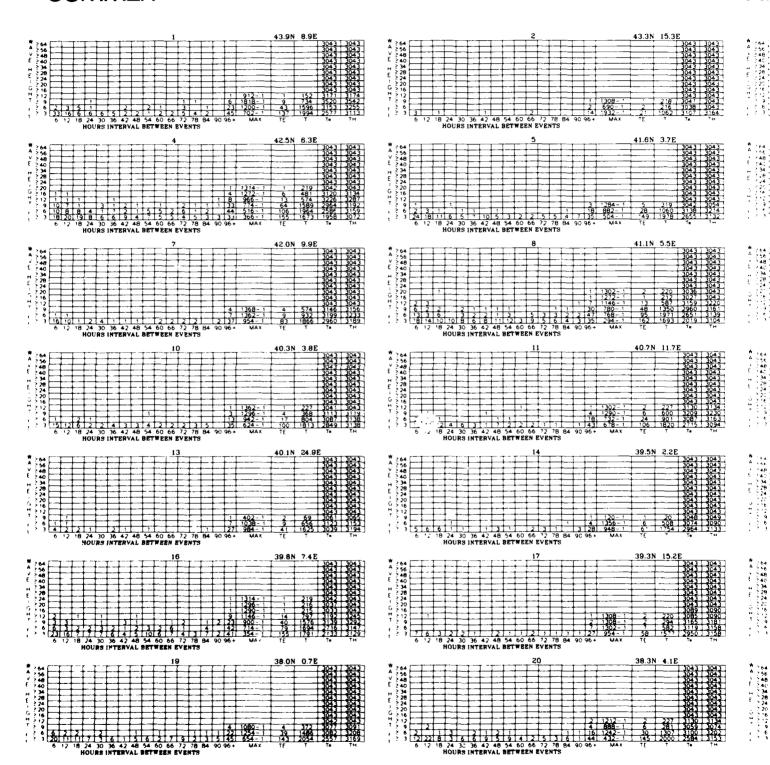


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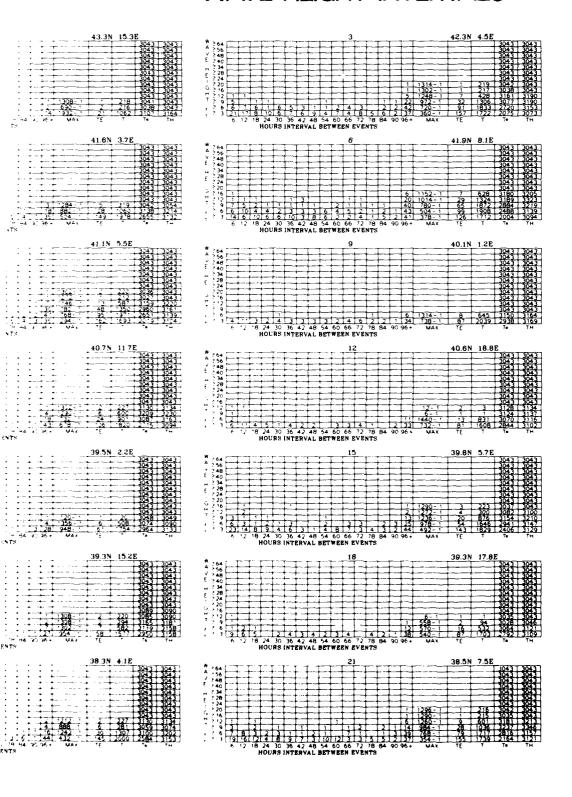
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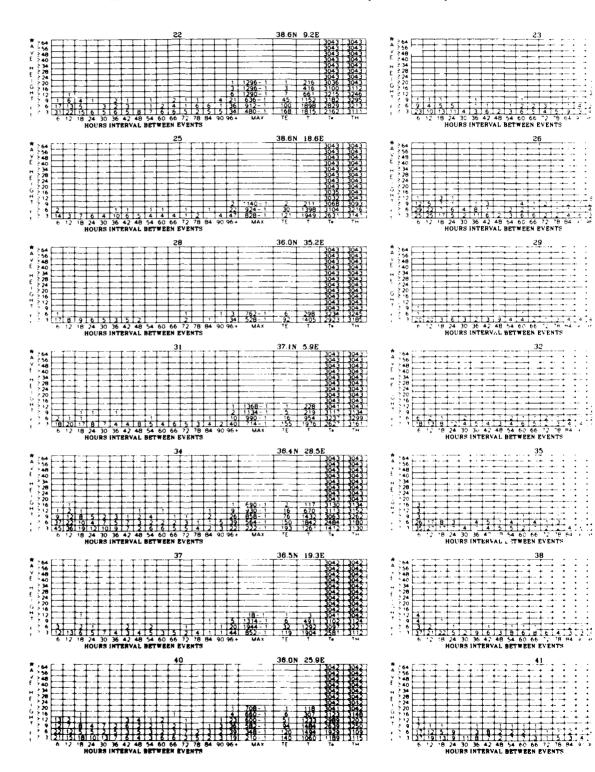


SUMMER



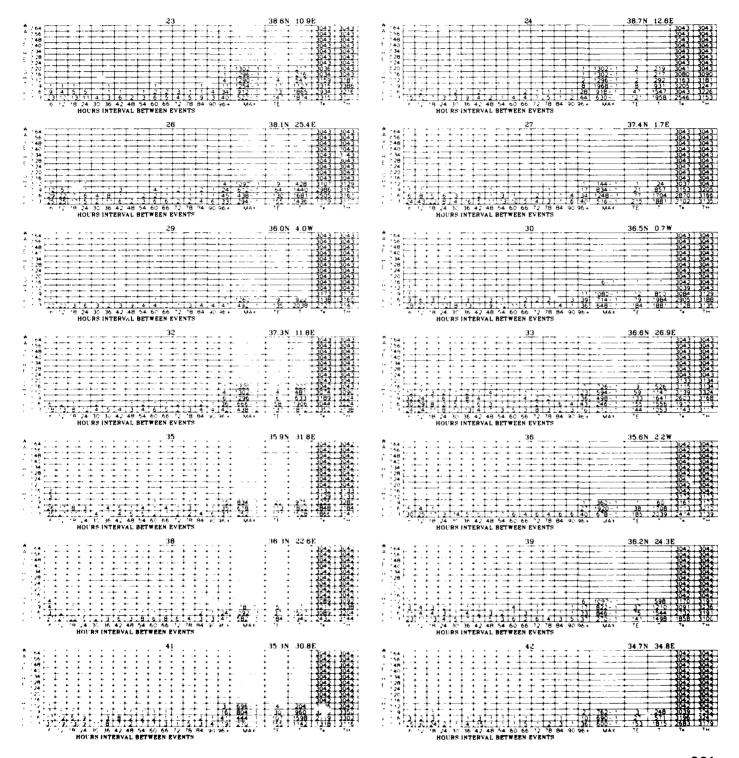
WAVE HEIGHT INTERVALS





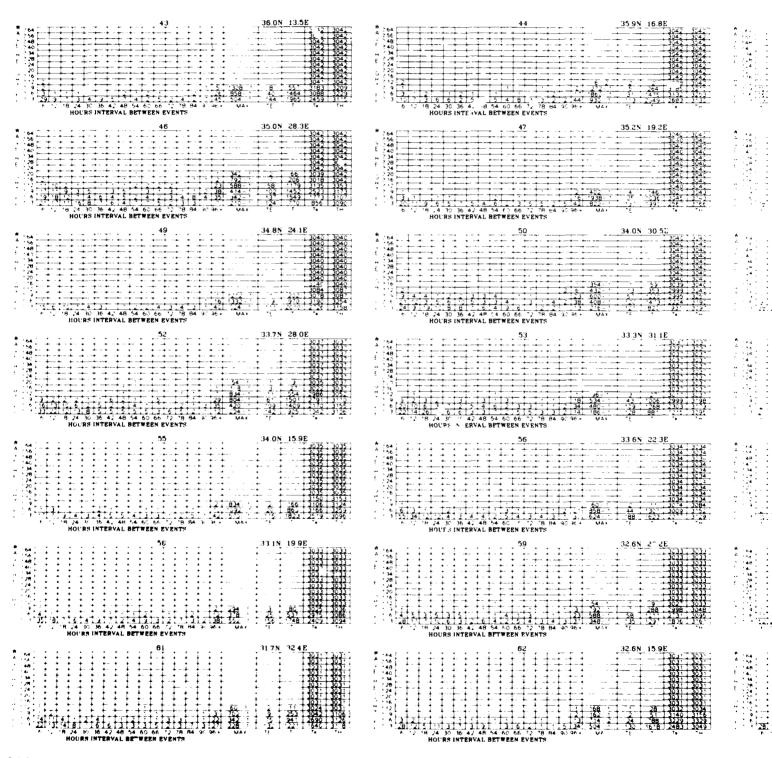
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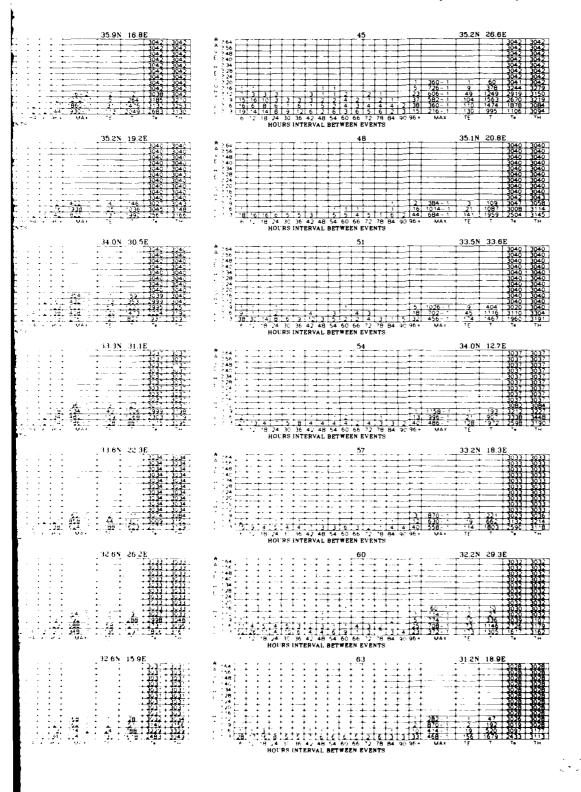
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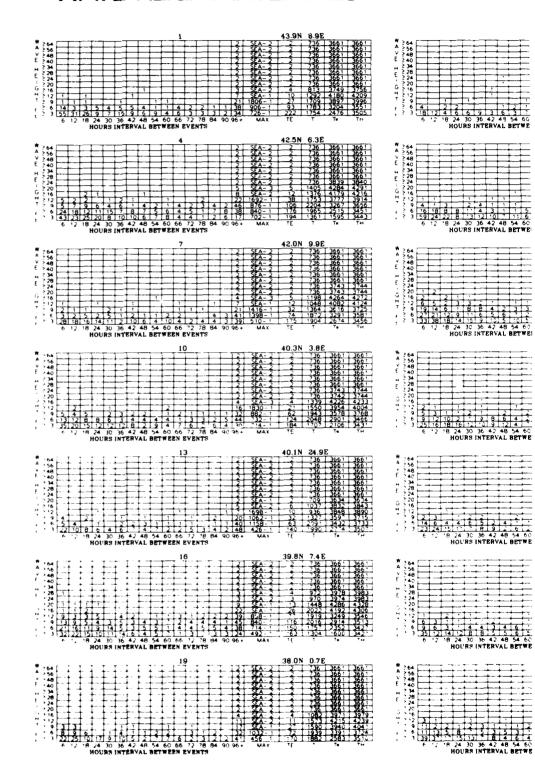
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WAVE HEIGH

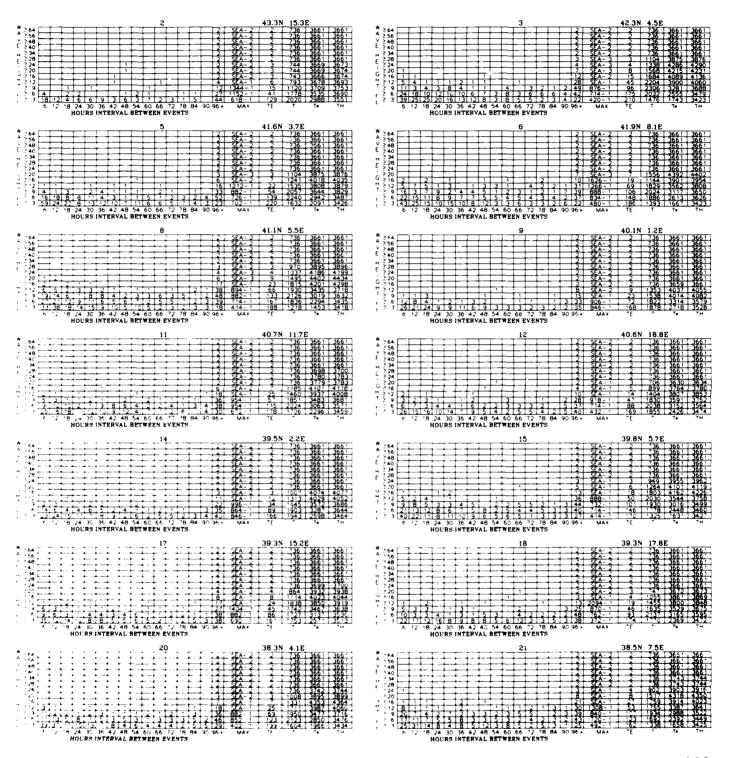




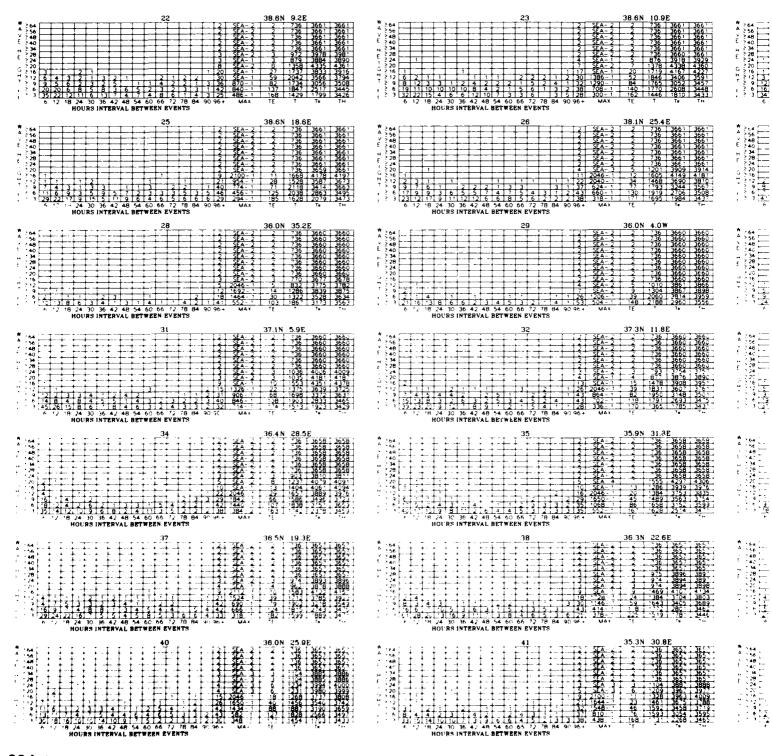
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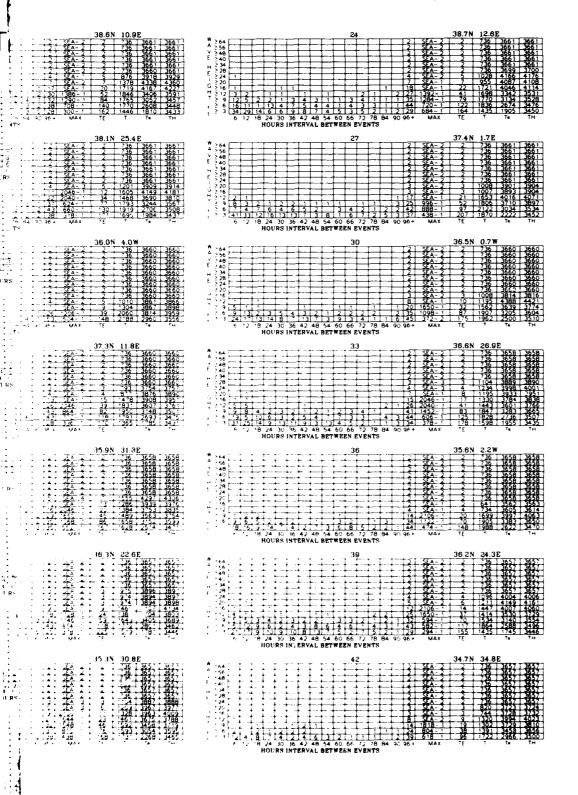


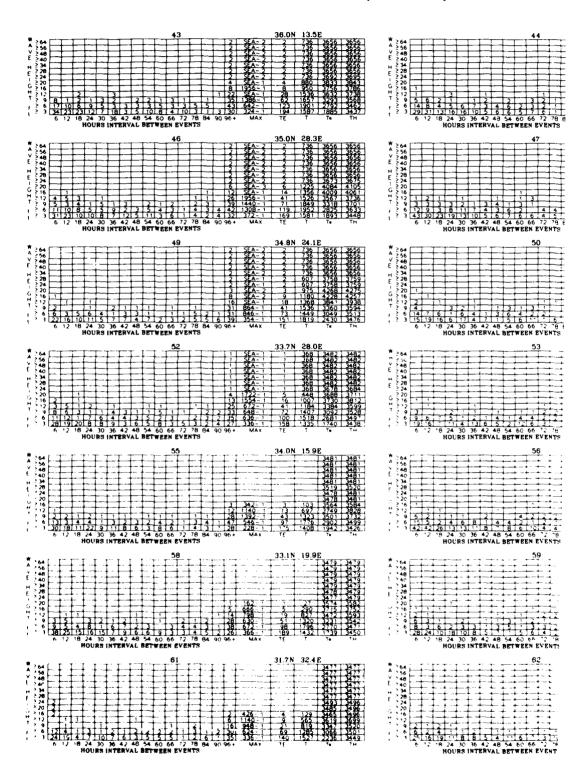
FALL

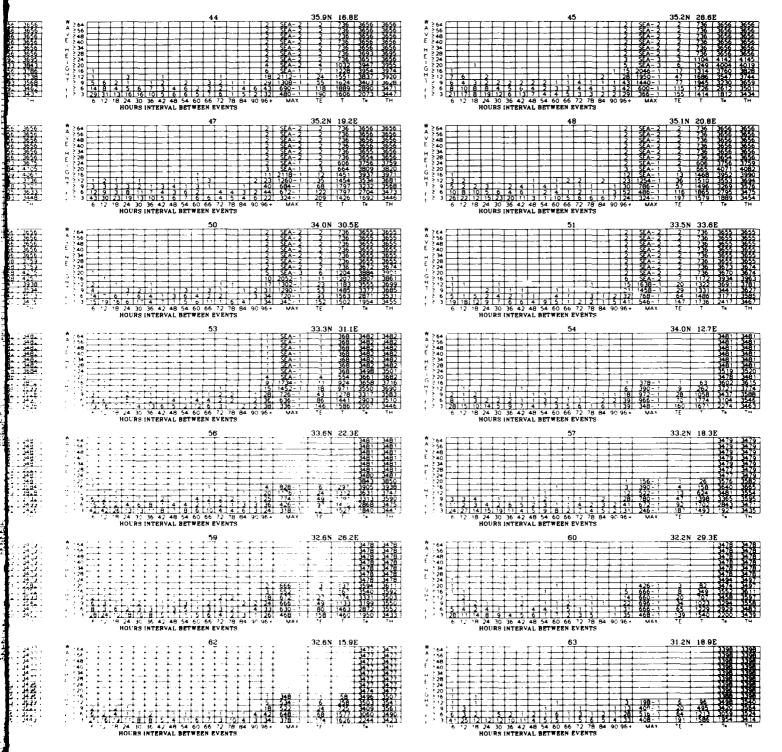


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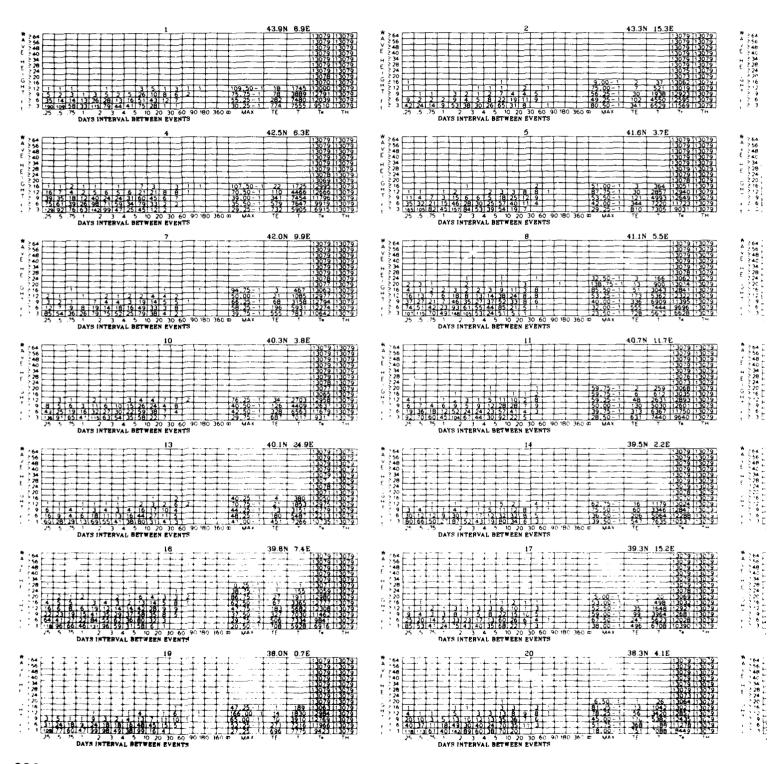




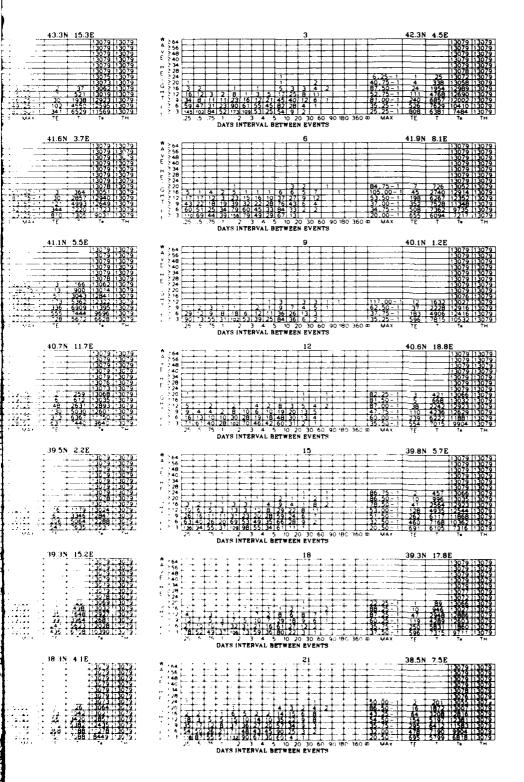


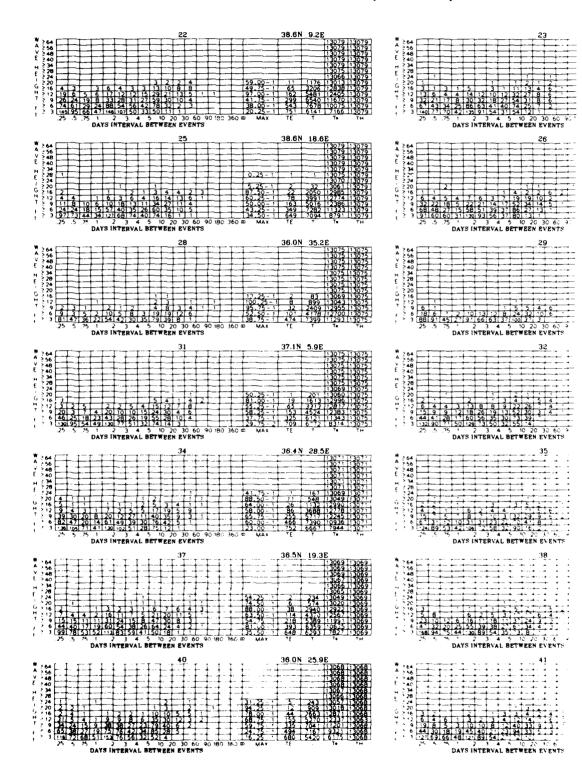


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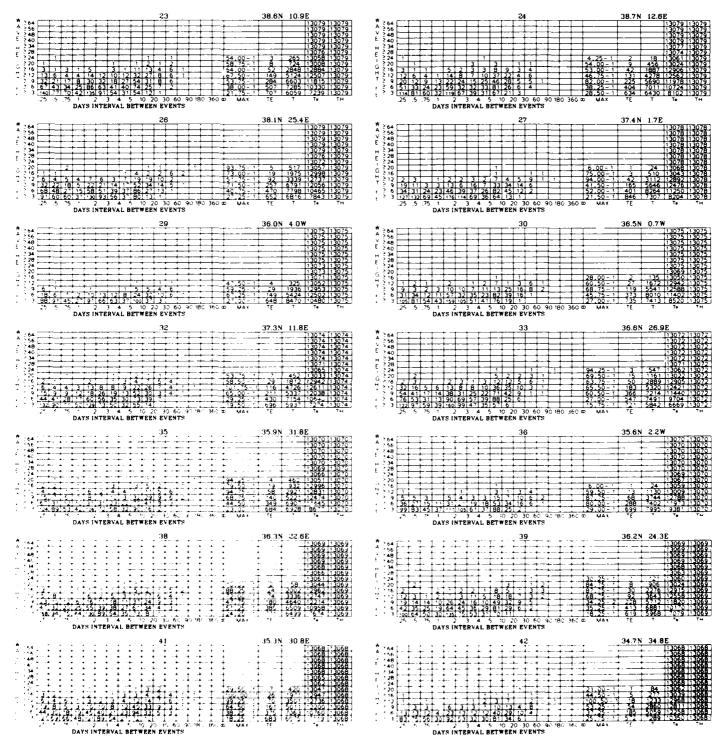
WAVE HEIGHT INTERVALS



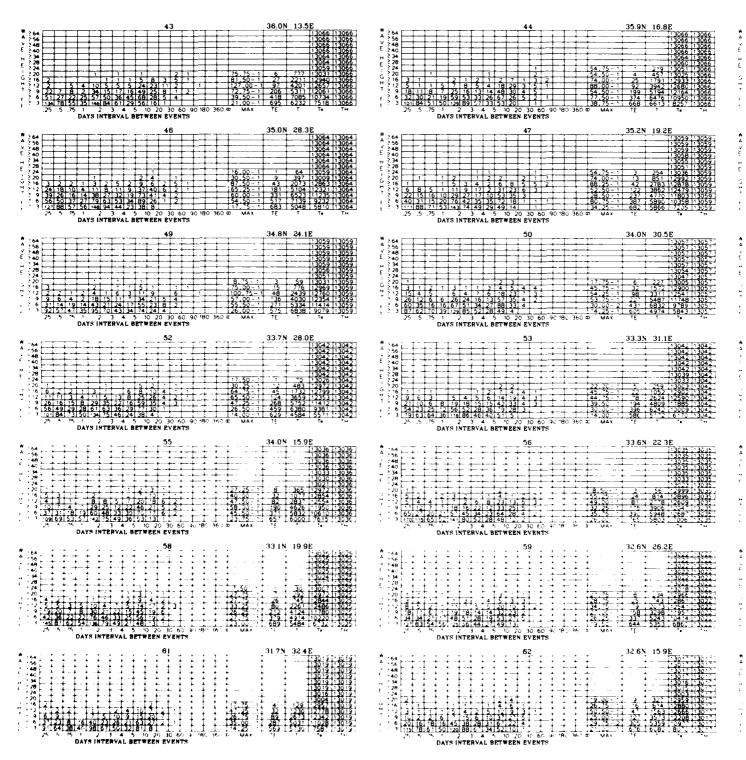


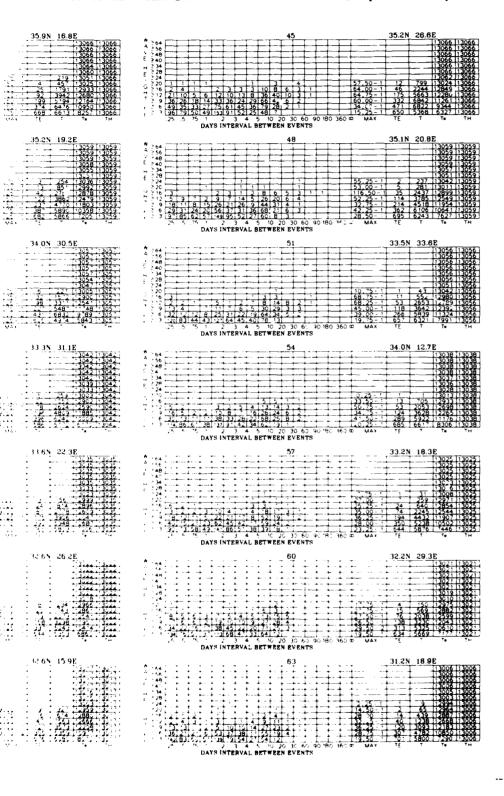
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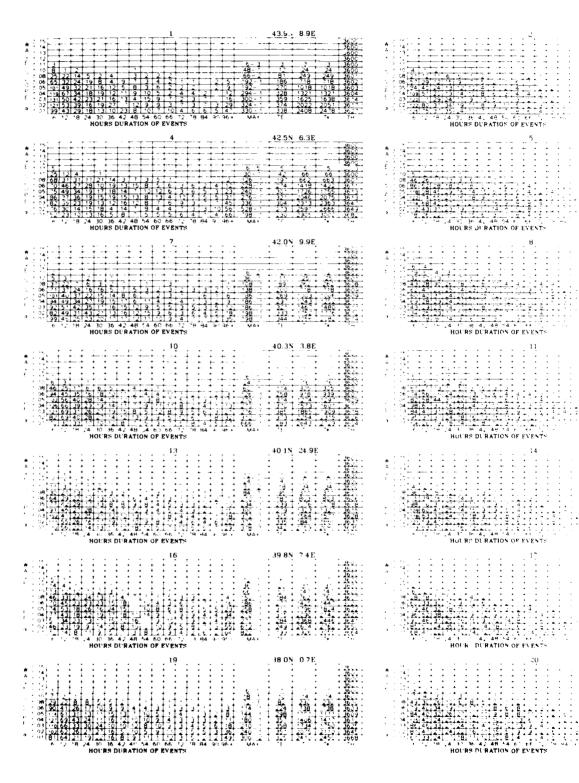


WAVE HEIG





WAVE SLOPE (α) DURATIONS



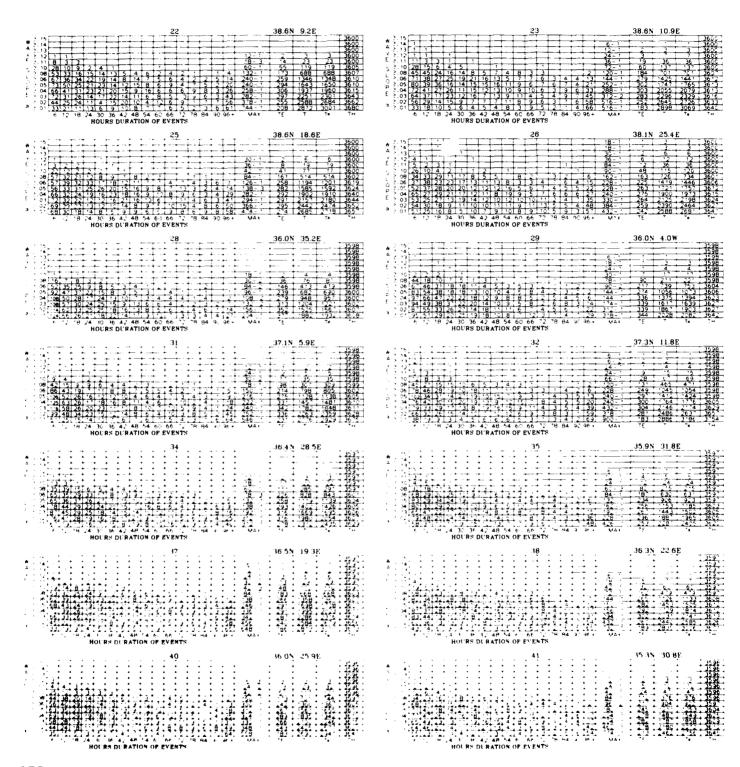
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WINTER

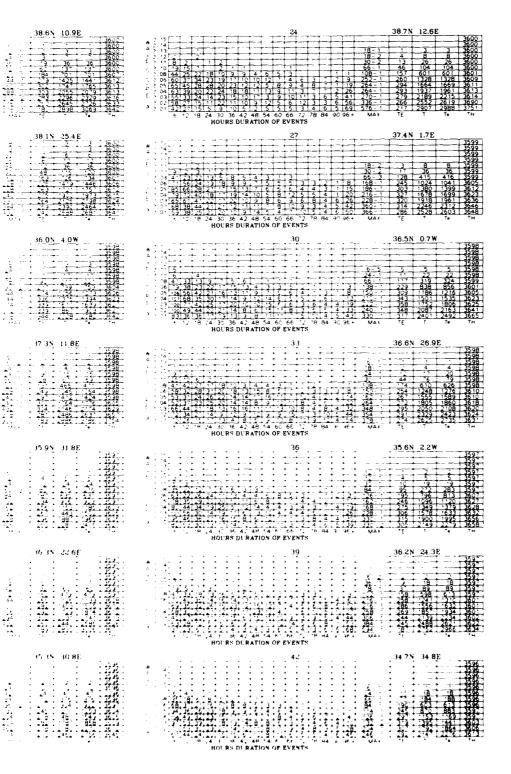
43.3N 15.3E 43.3N 15.3E 43.3N 15.3E 43.3N 15.3E 43.3N 15.3E 44.2N 15.3N 15.3E 45.2N 15.3N 15.3N 15.3E 45.2N 15.3N 15.3E 45.2N 15.3N 15.3E 45.2N 15.3N 15.3E	3 42.3N 4.5E 42.3N 4.5E 5.00 5.00 5.00 6.00
5 41.6N 3.7E 100 100 100 100 100 100 100 100 100 10	6 41.9N 8 1E 15.5
H 41 IN 55E	9 40 1N 12E 16 2 16 2 16 2 16 2 16 2 16 2 16 2 16
HOURS DUBATION OF EVENTS 11 407N 117E 22 1 407N 117E 407N 117E	12 40 6N 18 8E 12 2 40 6N 18 8E 13 2 4 4 16 16 17 18 18 18 18 18 18 18 18 18 18 18 18 18
HOURS OF BATION OF FANKTS 17 (9.48) 15.2E	10 39 88 5 7 E
HOURS THE BATTON OF EVENTS	18 39 3N 17 8F 16 16 16 16 16 16 16 16 16 16 16 16 16 1
20 OH 48 111	HOLEN DURATION OF EVENTS

WINTER

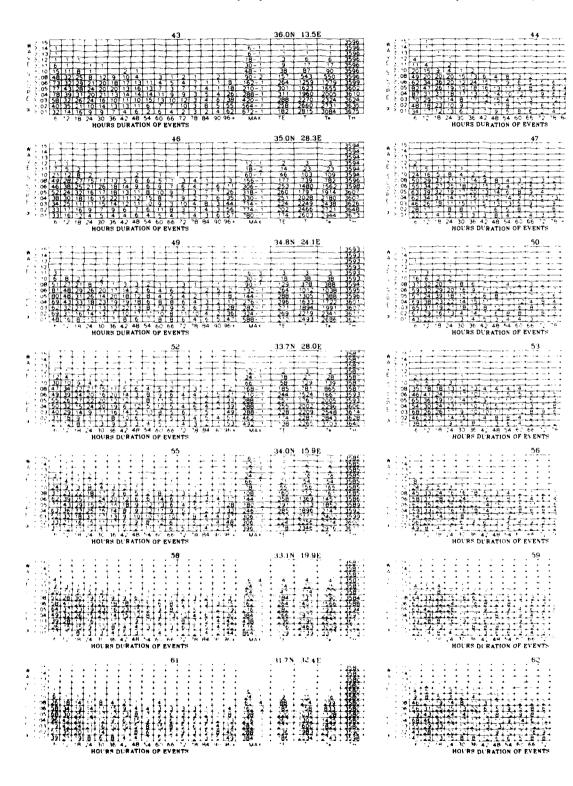
WAVE SLOPE



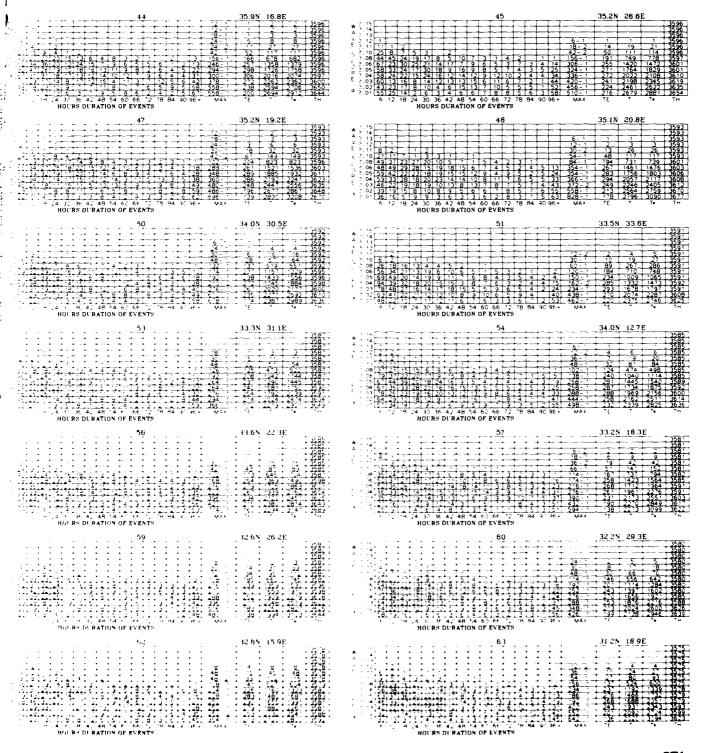
VE SLOPE (α) DURATIONS (Cont'd)

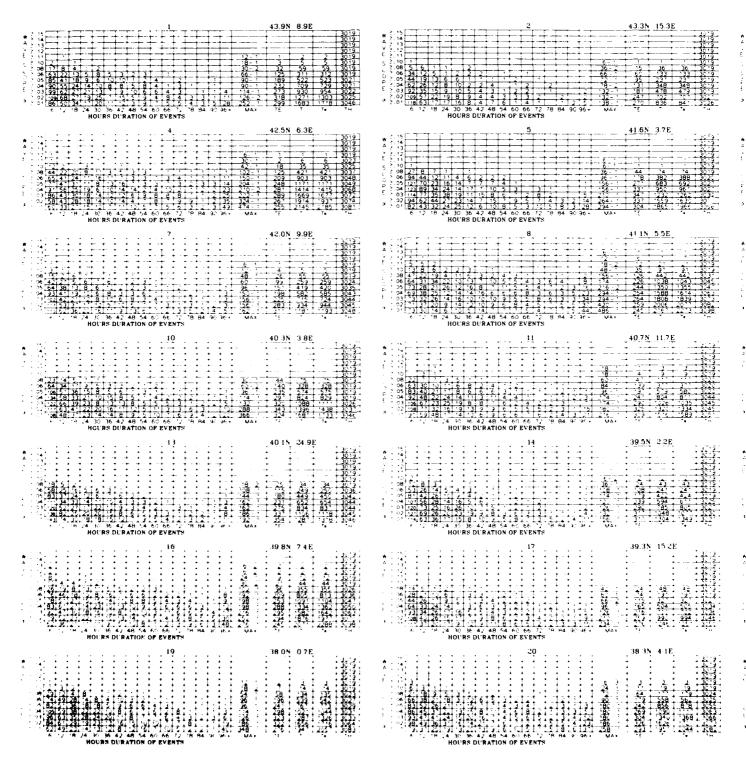


WAVE SLOPE (α) DURATIONS (Cont'd)

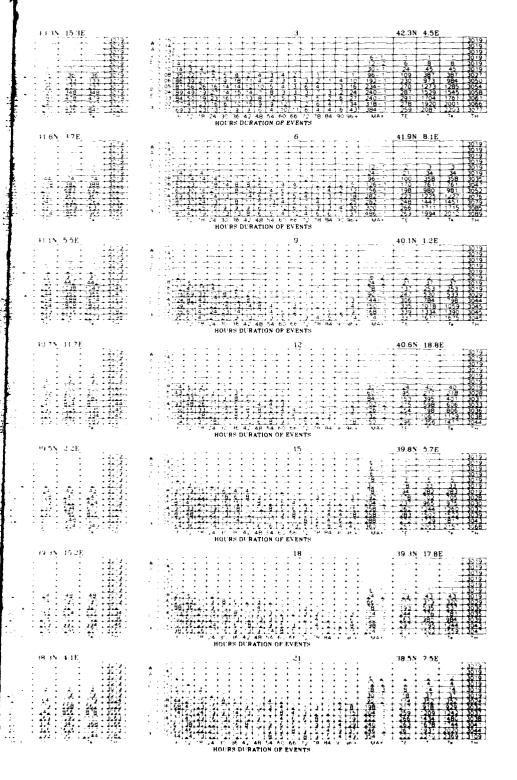


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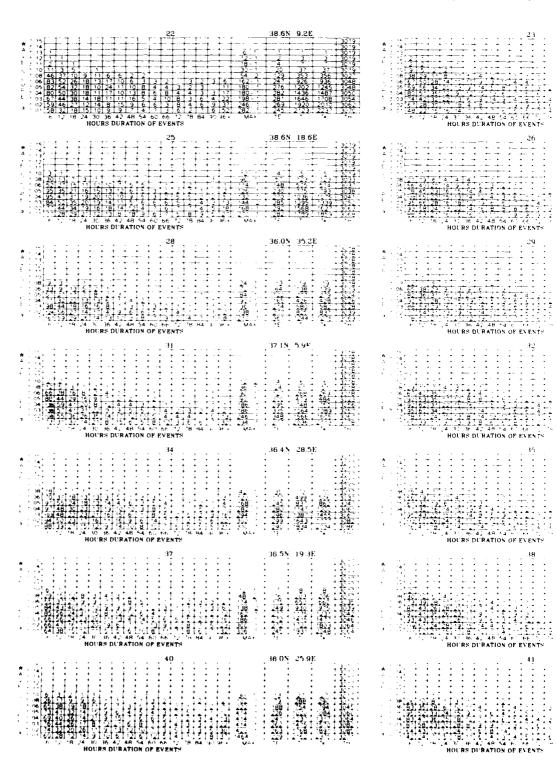




WAVE SLOPE (α) DURATIONS

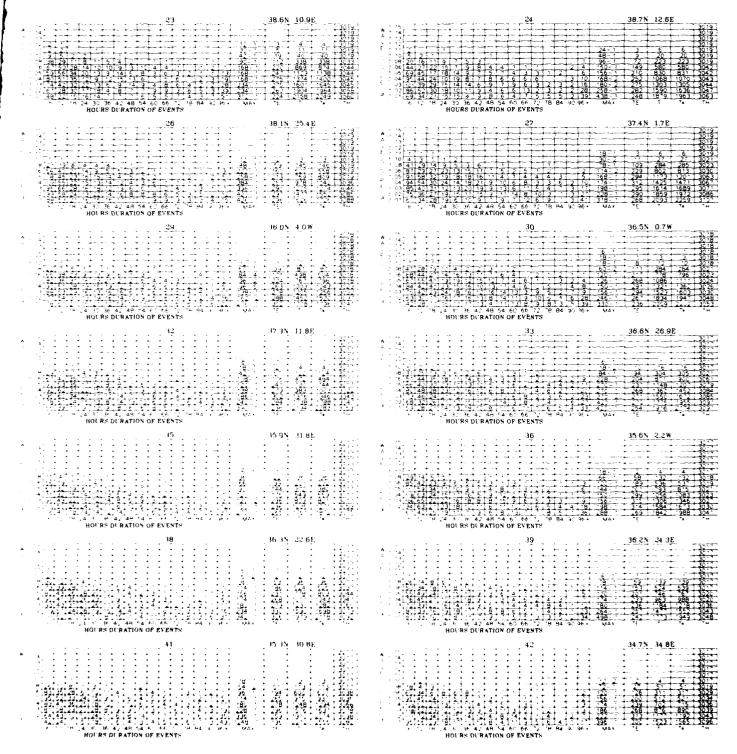


WAVE SLOPE (α) DURATIONS (Cont'd)



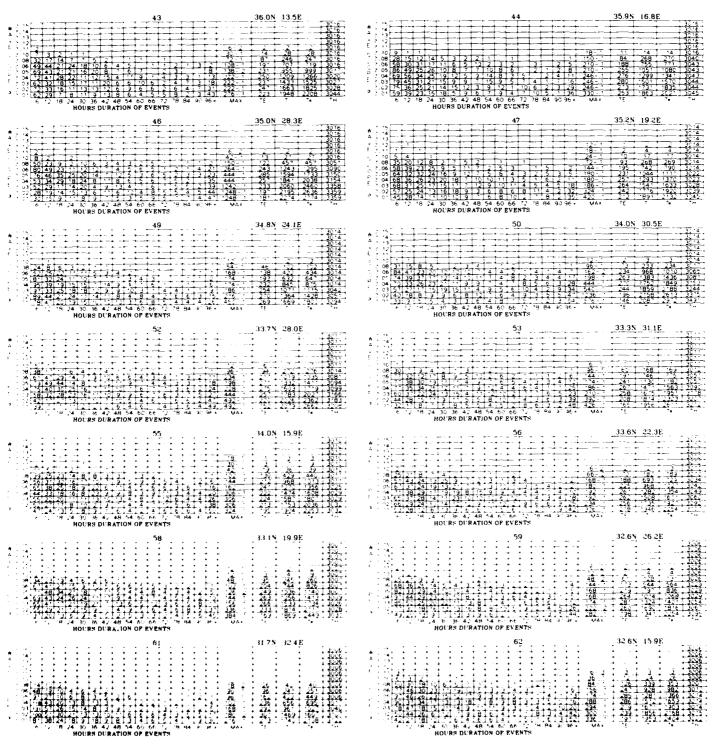
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SPRING

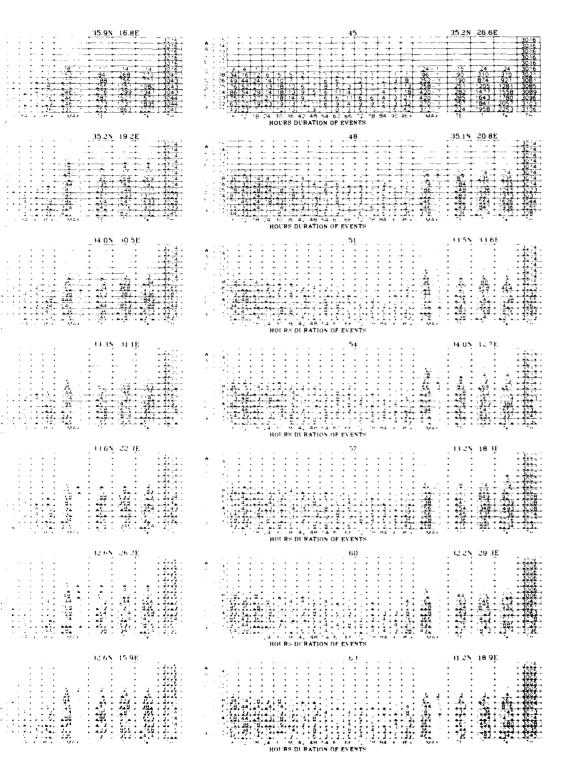


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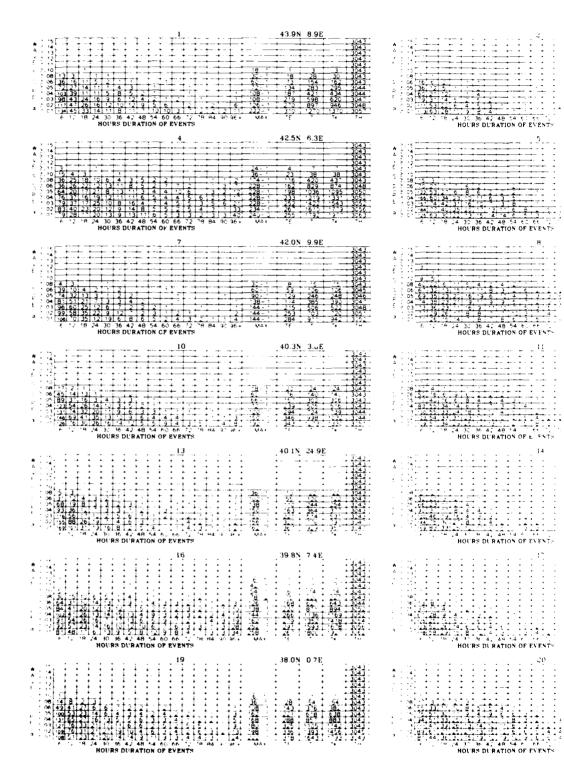
WAVE SLOPE (a)



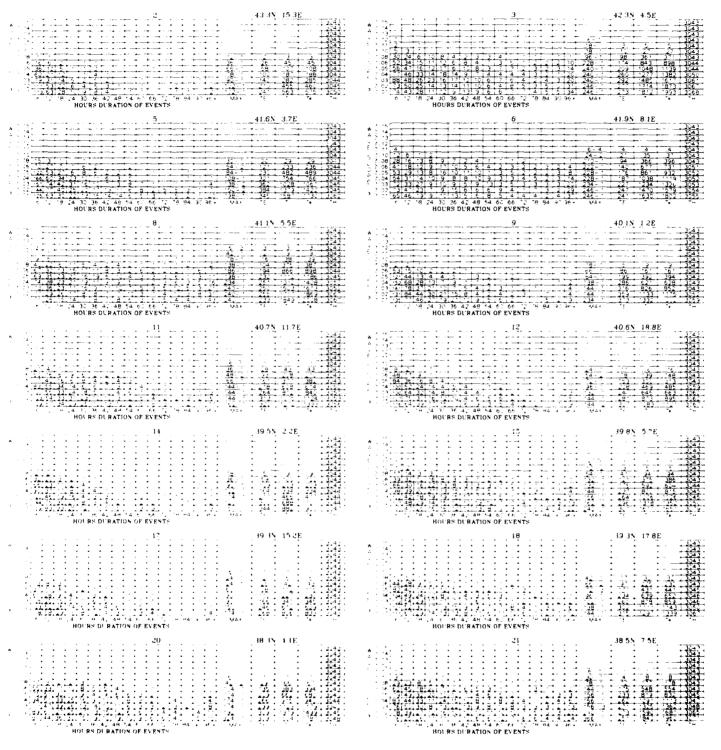
WAVE SLOPE (a) DURATIONS (Cont'd)



WAVE SLOPE (α) DURATIONS

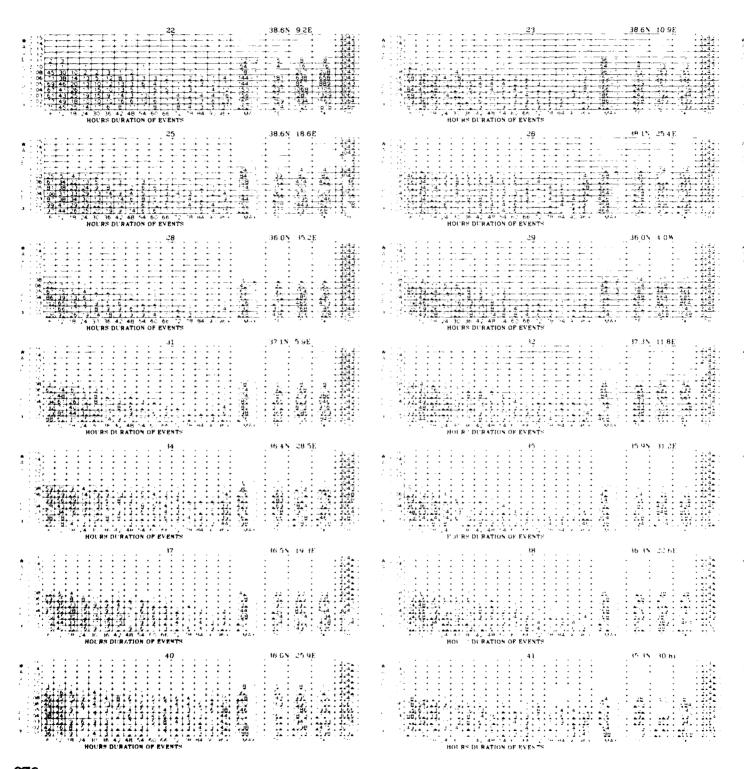


SUMMER

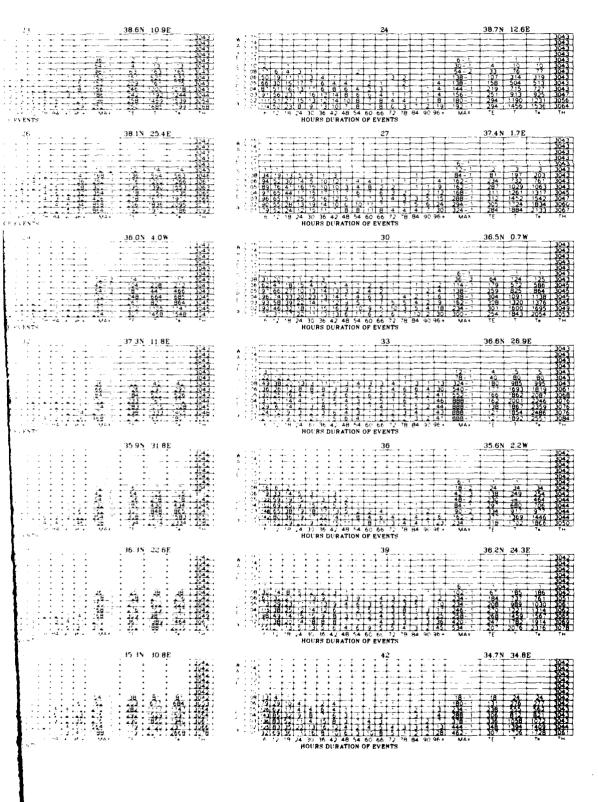


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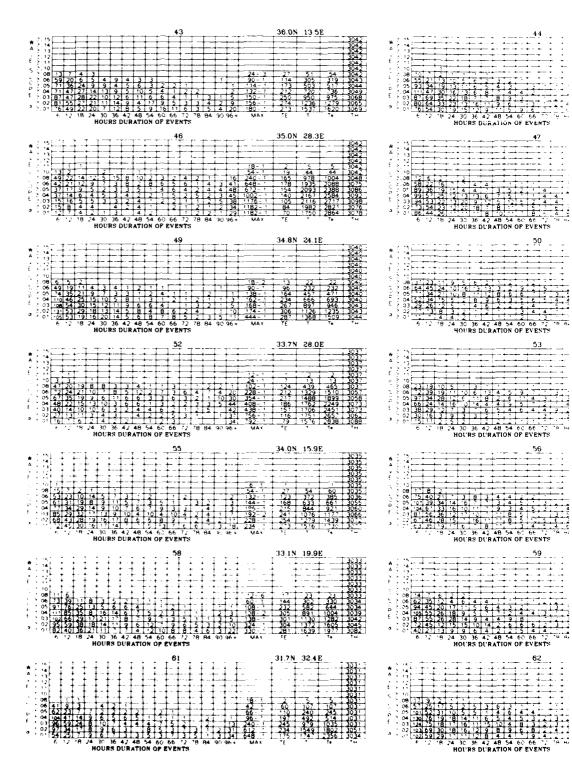
WAVE SLOPE (a)



WAVE SLOPE (α) DURATIONS (Cont'd)

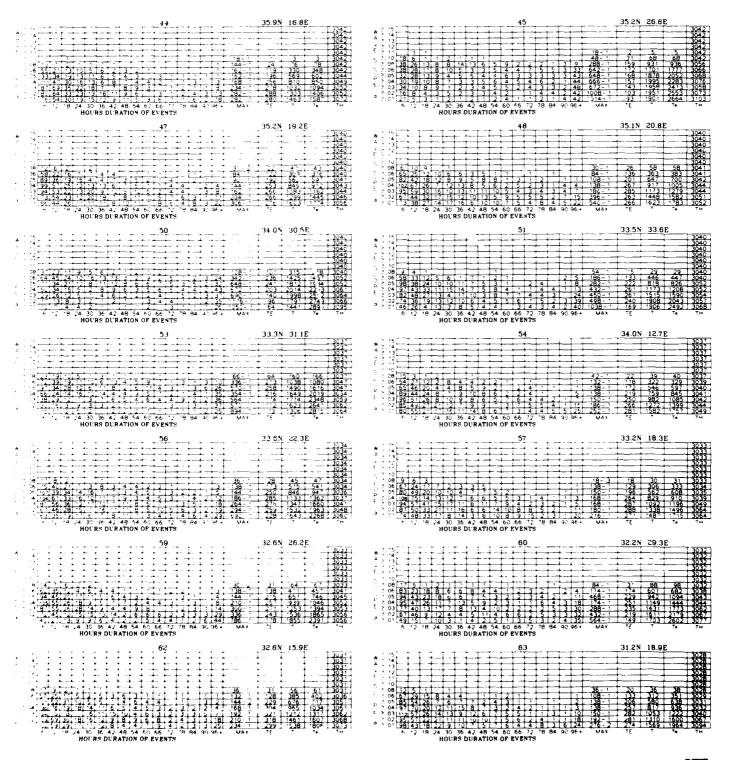


WAVE SLOPE (α) DURATIONS (Cont'd)

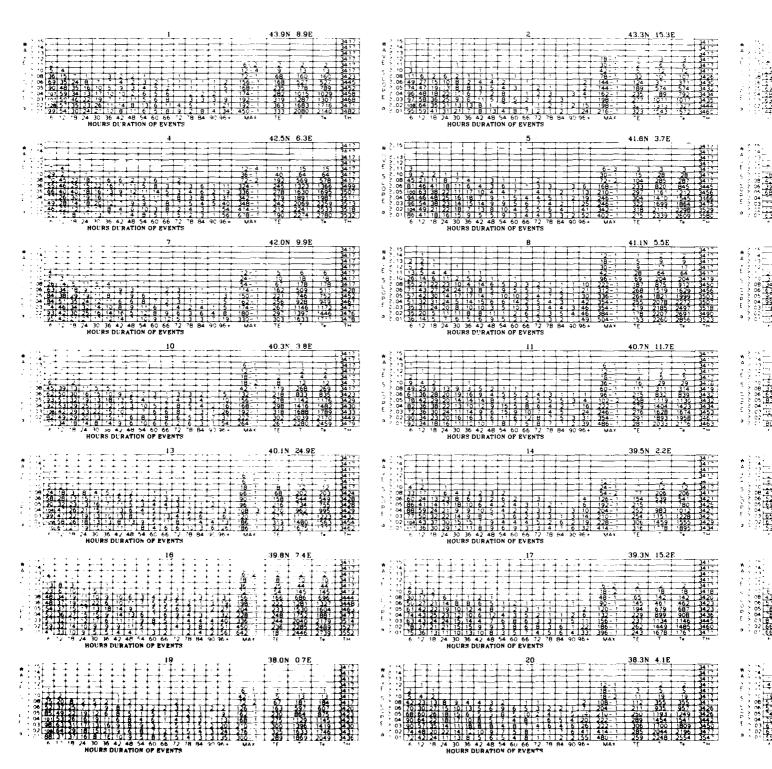


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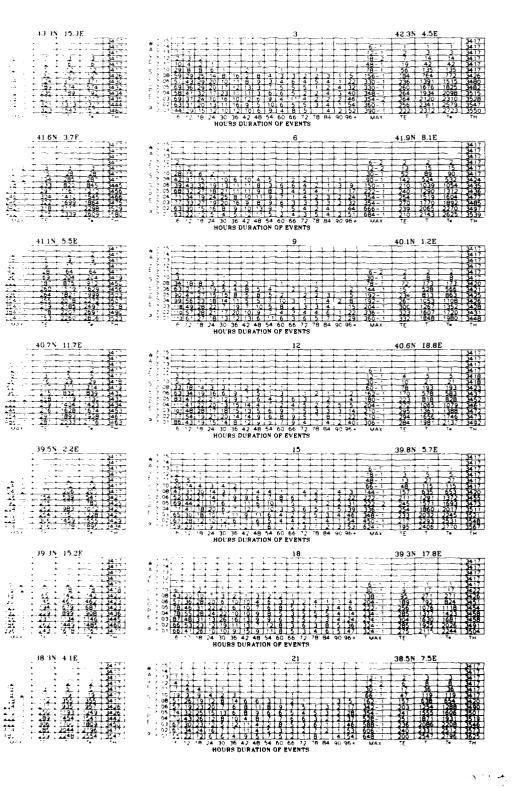
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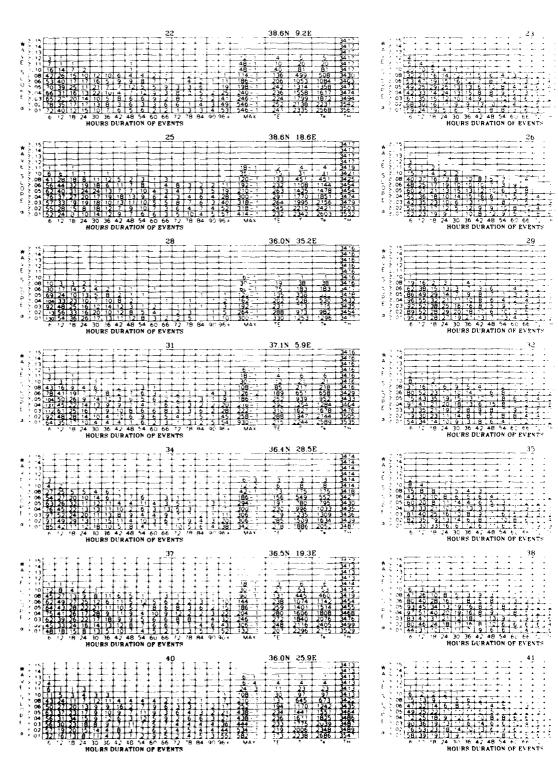
WAVE SLO



WAVE SLOPE (α) DURATIONS



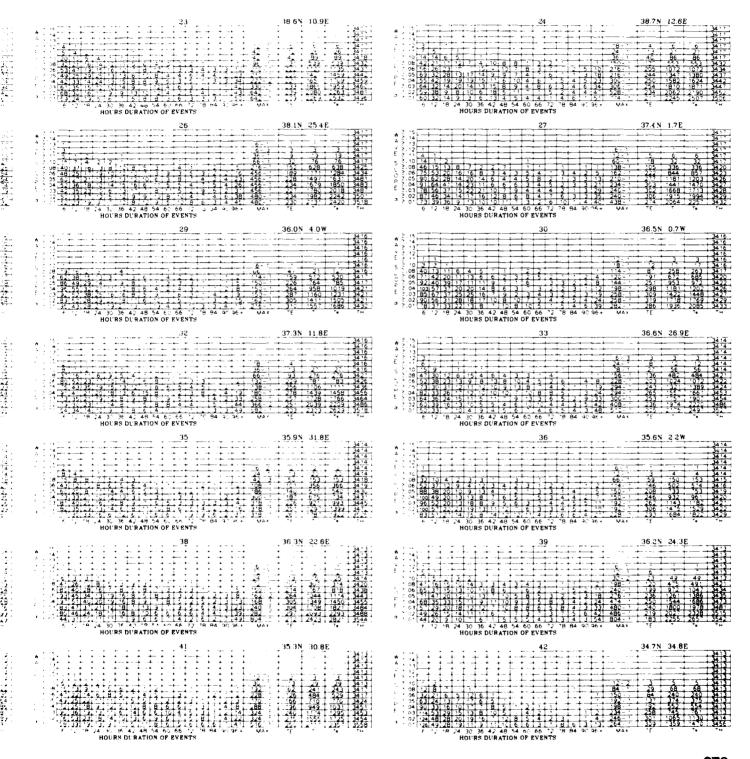
WAVE SLOPE (α) DURATIONS (Cont'd)



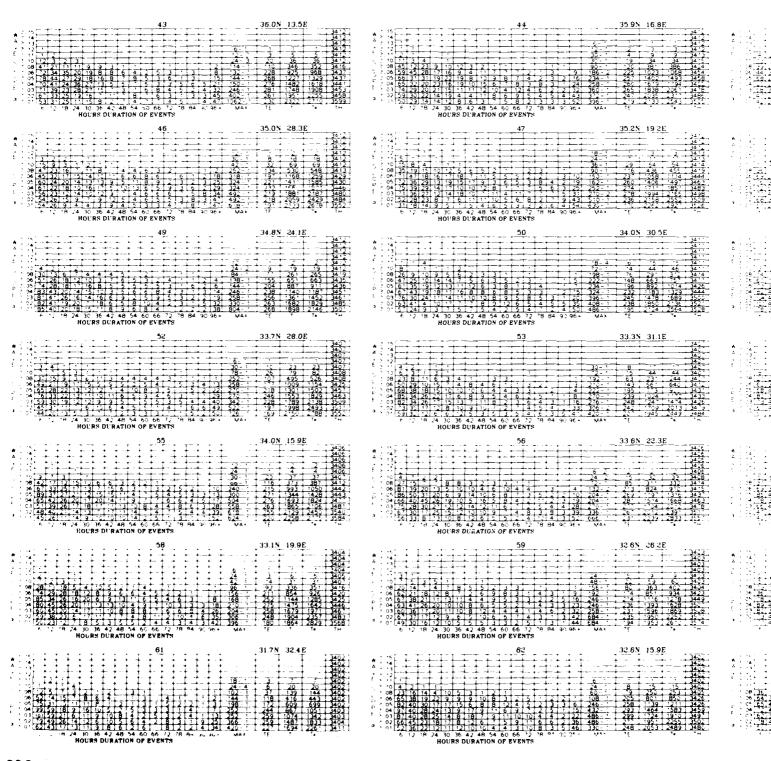
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TIONS (Cont'd)

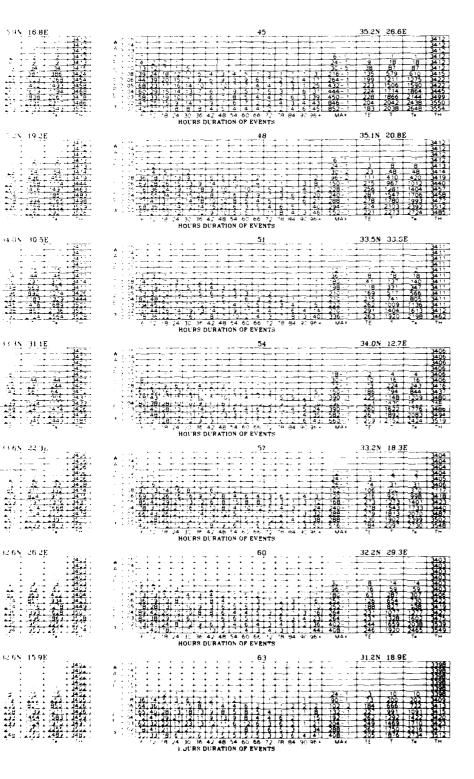
FALL



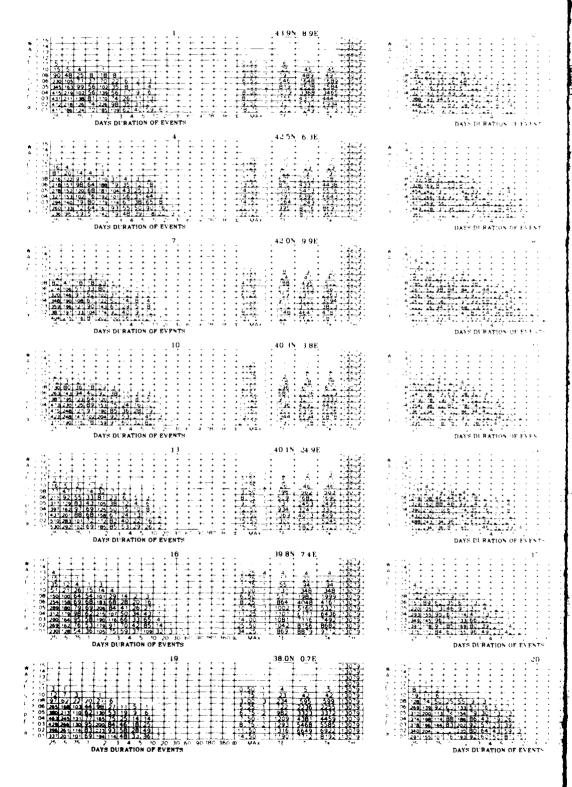
WAVE SLOPE (a) D



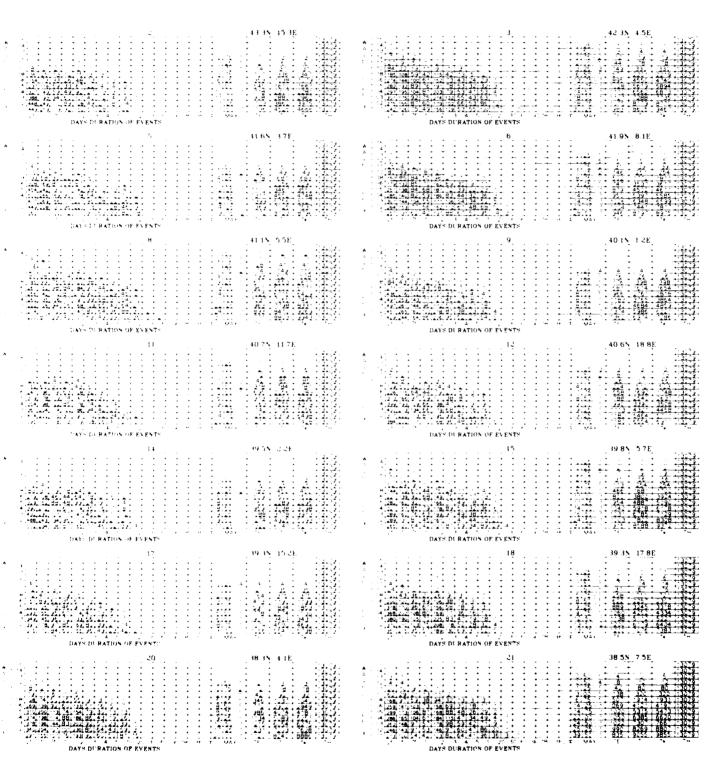
SLOPE (a) DURATIONS (Cont'd)



WAVE SLOPE (a) DURATIONS



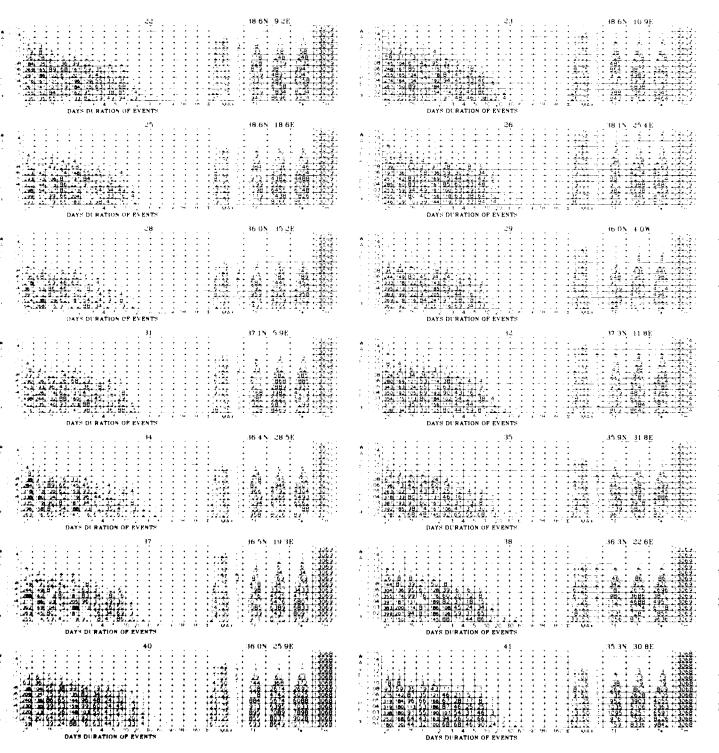
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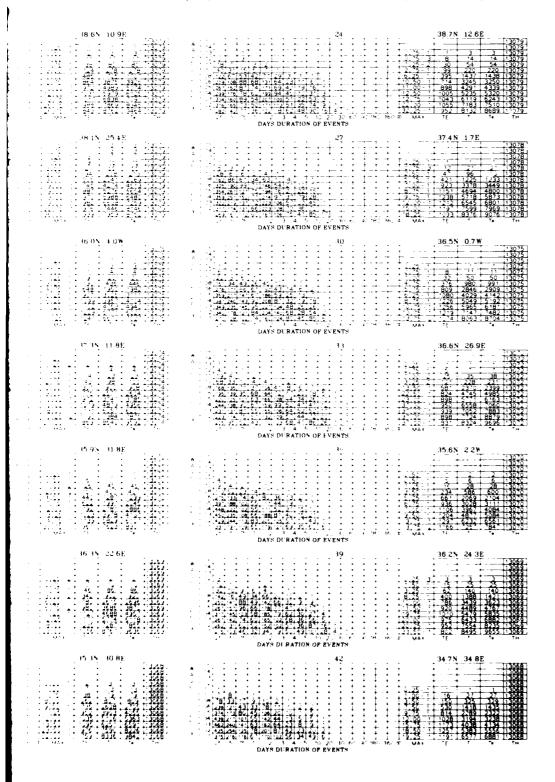
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WAVE SLOPE (a)

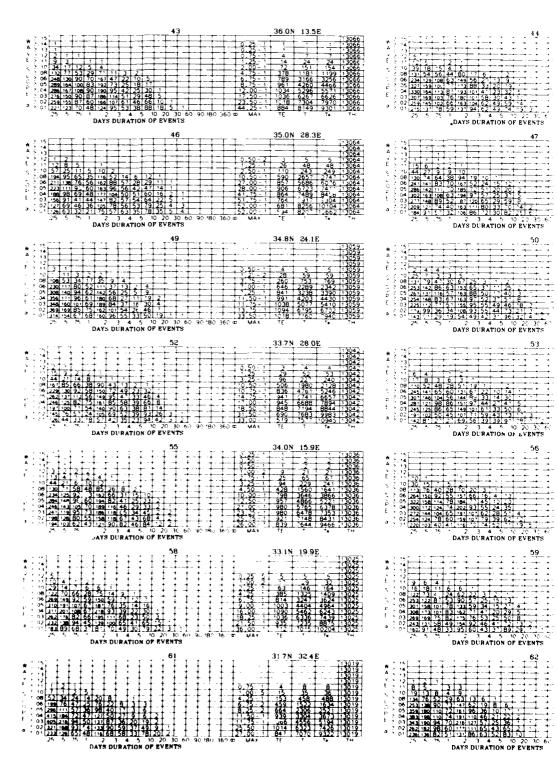




NAVE SLOPE (a) DURATIONS (Cont'd)

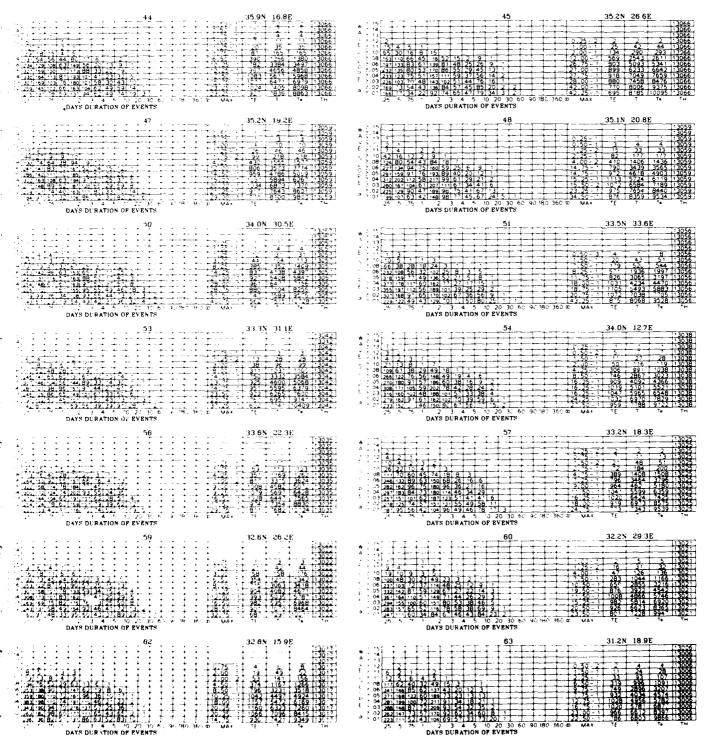


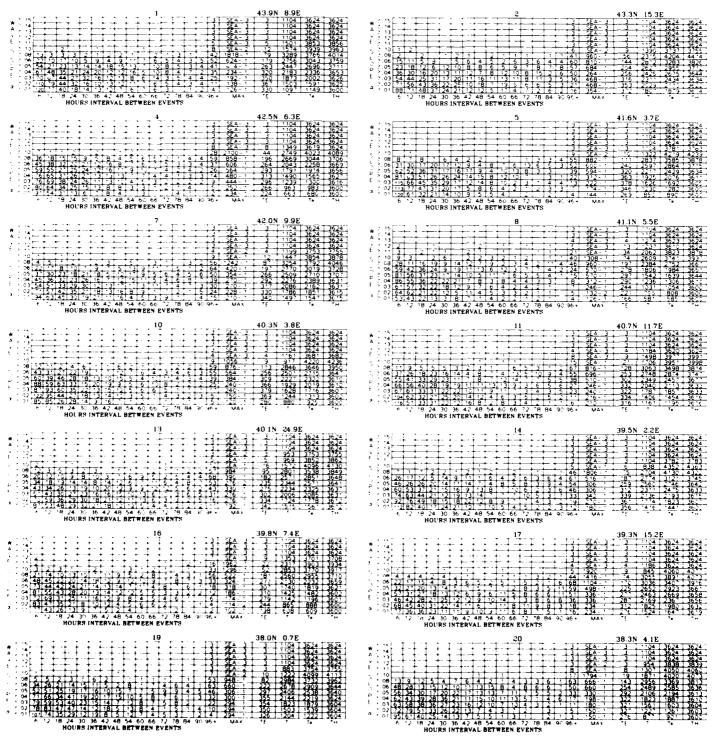
WAVE SLOPE (α) DURATIONS (Cont'd)



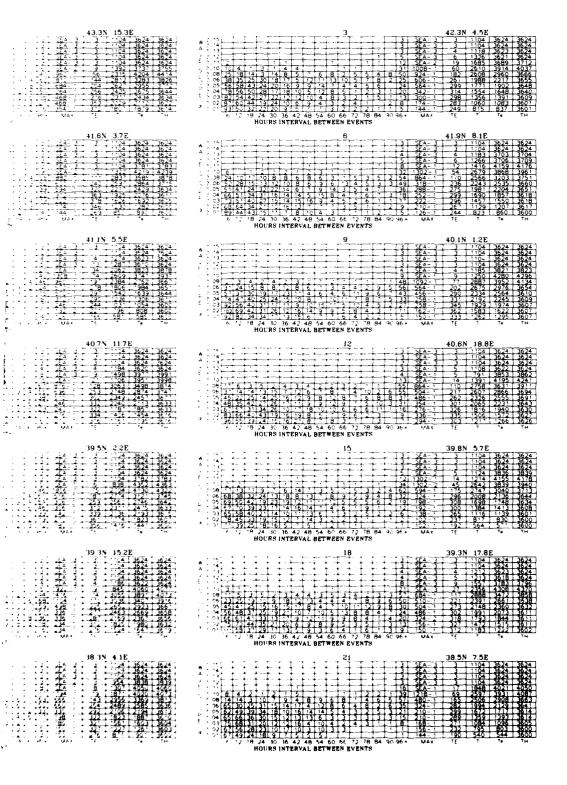
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ANNUAL

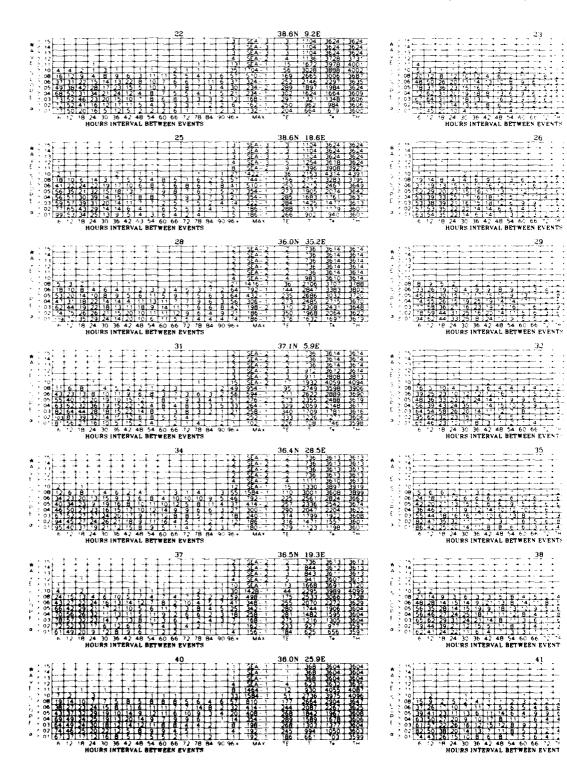




WAVE SLOPE (α) INTERVALS

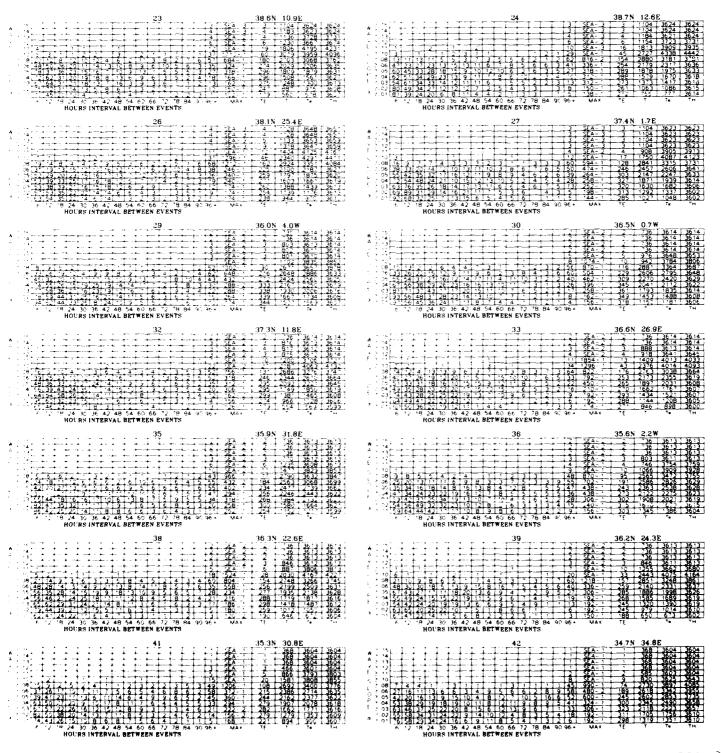


WAVE SLOPE (α) INTERVALS (Cont'd)



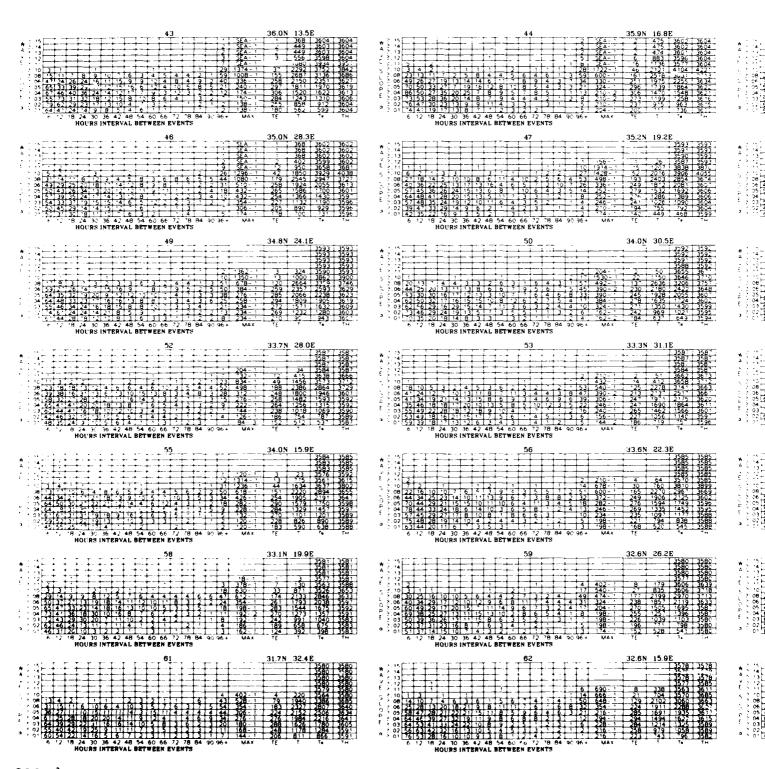
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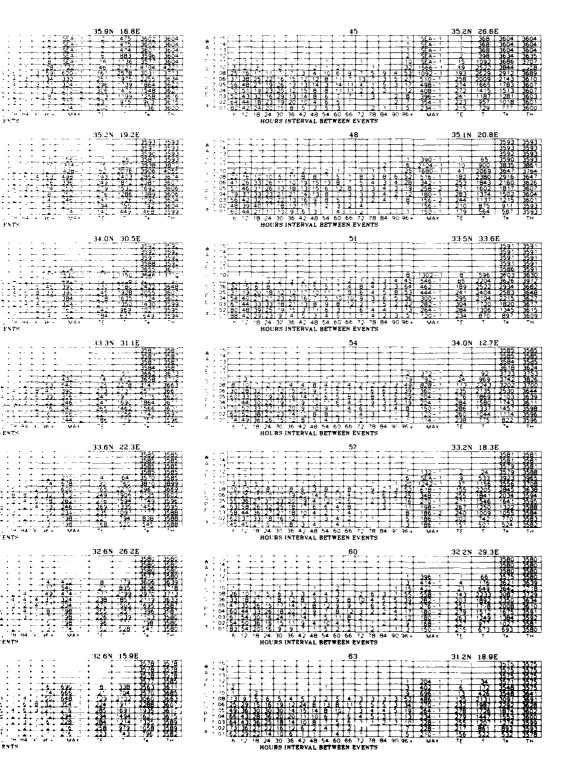


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WAVE SLOPE (a)

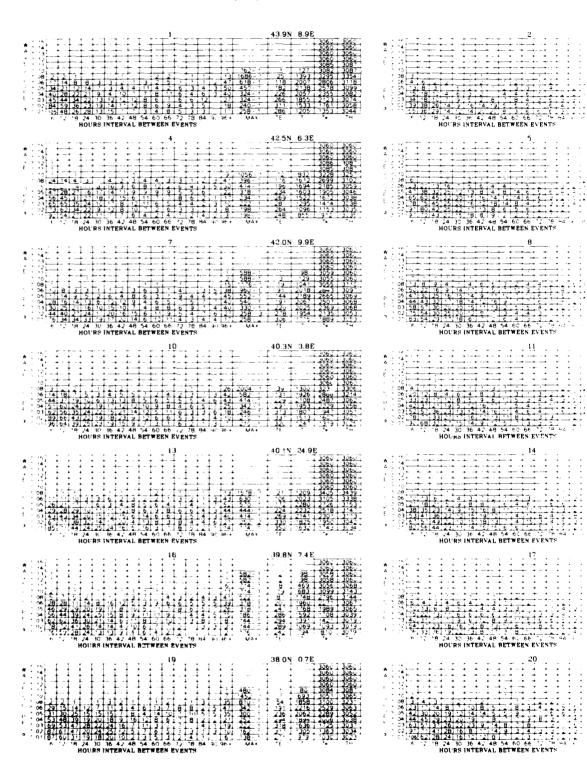


WAVE SLOPE (a) INTERVALS (Cont'd)



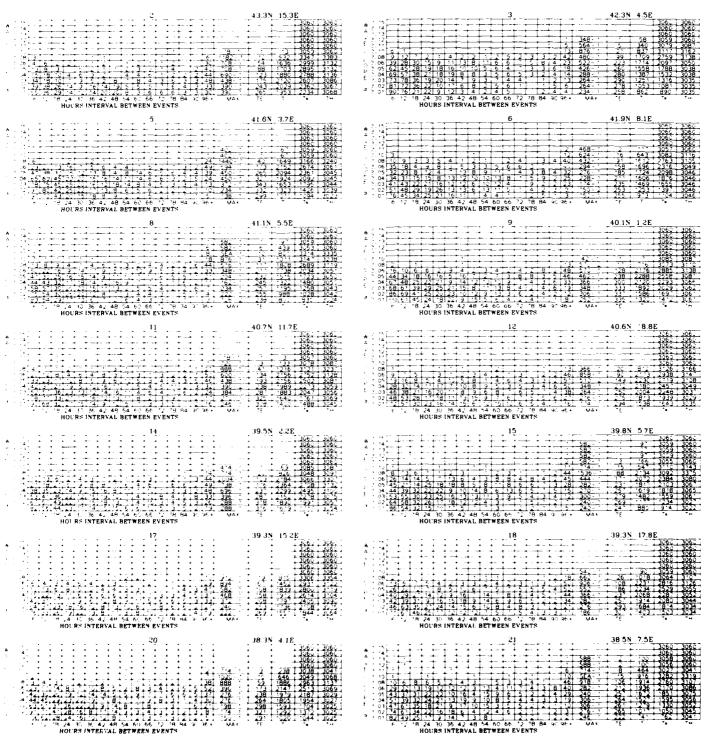
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WAVE SLOPE (α) INTERVALS



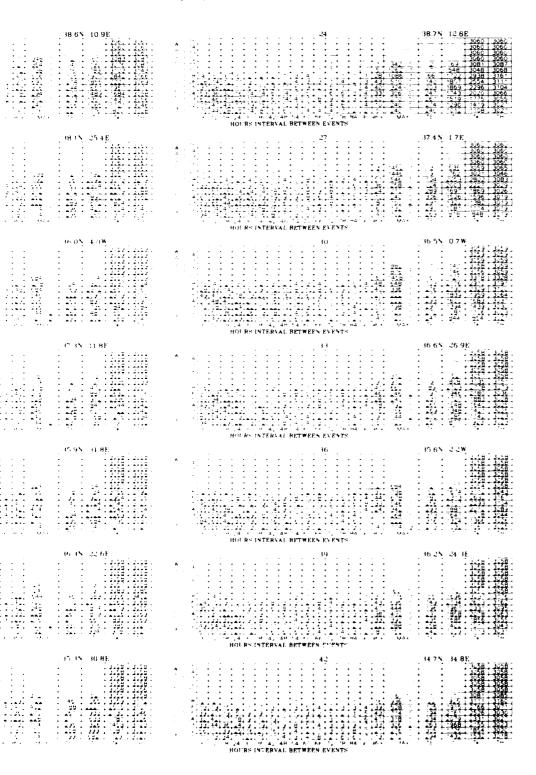
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SPRING

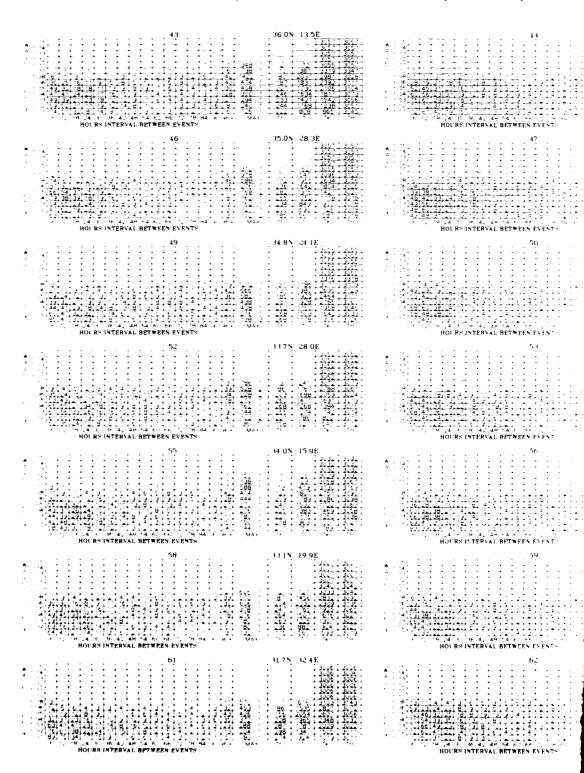


Je v 34 de	23 30.65 10.00
22 38 6N 9 2E 105 105 105 105 1	23 386 \ 10.9E
25 38 6N 18 6E 25 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	26 38 1N 25 4E
28 16 DN 35 2F. 16 DN 35 2F. 16 DN 35 2F. 16 DN 35 2F. 16 DN 35 2F. 16 DN 35 2F. 17 DN 35 2F. 18 DN 35 2F.	29 36 0N 4 0M
31 37 1N 5 9E 31 47 1N 5 9E 44 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	32 37 3N 11 8E
34 16 4 \ 28 5 F. 134 16 4 \ 28 5 F. 135 15 15 15 15 15 15 15 15 15 15 15 15 15	35 35.9% 31.8E
37 36 5N 19 3E 1.58 1.58 1.58 1.58 1.58 1.58 1.58 1.58	38 36 1N 22 6F. 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
40 36 0V 25 9E 30 10 10 10 10 10 10 10 10 10 10 10 10 10	41 35 3N 30 8E 1.58 3.58 3.0 8E 1.58 3.58 3.0 8E 1.58 3.58 3.0 8E 1.58 3.58 3.0 8E 1.58 3.58 3.0 8E 1.5

VAVE SLOPE (a) INTERVALS (Cont'd)

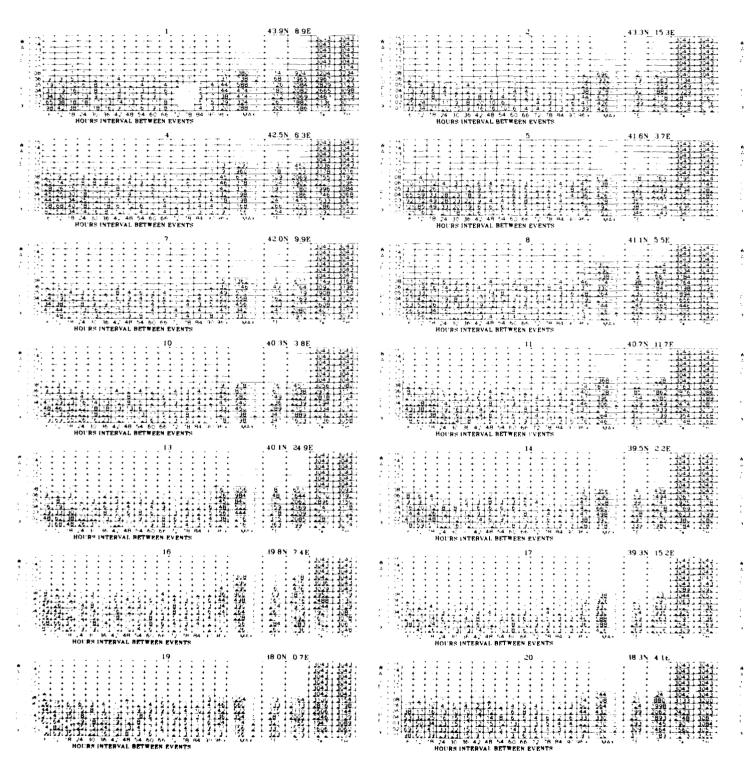


WAVE SLOPE (a) INTERVALS (Cont'd)

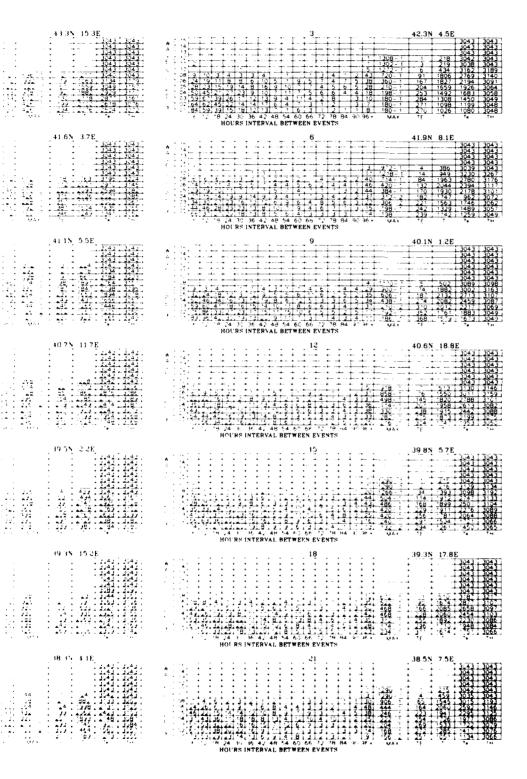


SPRING

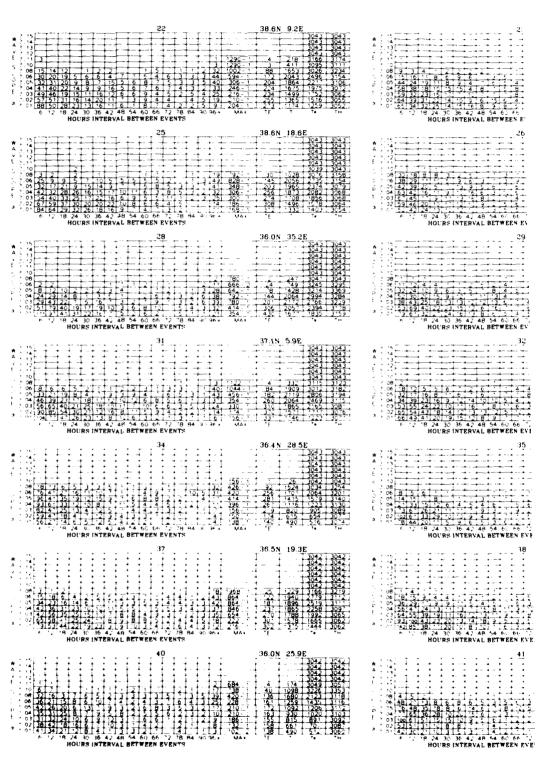
HOURS INTERNAL RETWEEN EVENTS	45 35.2N 26.6E 45 25.2N 26.6E 46 27 27 26 27 27 27 27 27 27 27 27 27 27 27 27 27
47 35 2N 19 2E 19	48 35 IN 20.8E
50 34 0N 40 5E	51 33.5K 33.6E 3.7E 3.7E 3.7E 3.7E 3.7E 3.7E 3.7E 3.7
HOLES INTERVAL BETWEEN EVENTS	HOURS INTERVAL BETWEEN EVENTS 77 14 ON 12 7E 4
06 13.68 22.3E 3.20 2.20 3.20 2.20 3.20 2.20 3.20 2.20 3.20 2.20 3.20 2.20 4.20 2	57 13.2N 18 JE 13.2N 18 JE 14.2 14.3 15.3 15.3 15.3 15.3 15.3 15.3 15.3 15
HOI RELIGIES ALBETHES EVENTS	600 3E 100 100 100 100 100 100 100 100 100 10
62 \$2.6N 15 9E	HOUR INTERVAL BETWEEN EVENTS



WAVE SLOPE (α) INTERVALS

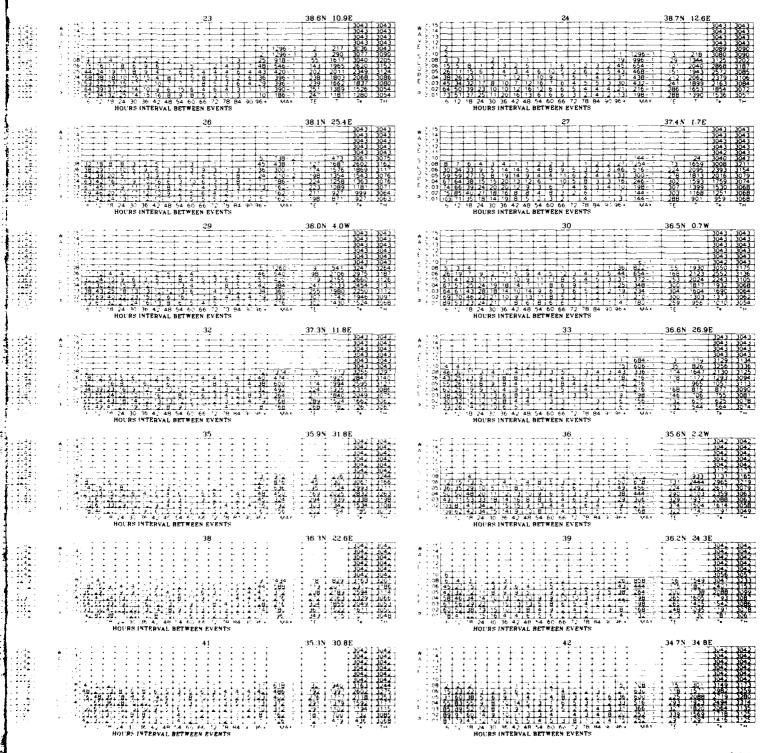


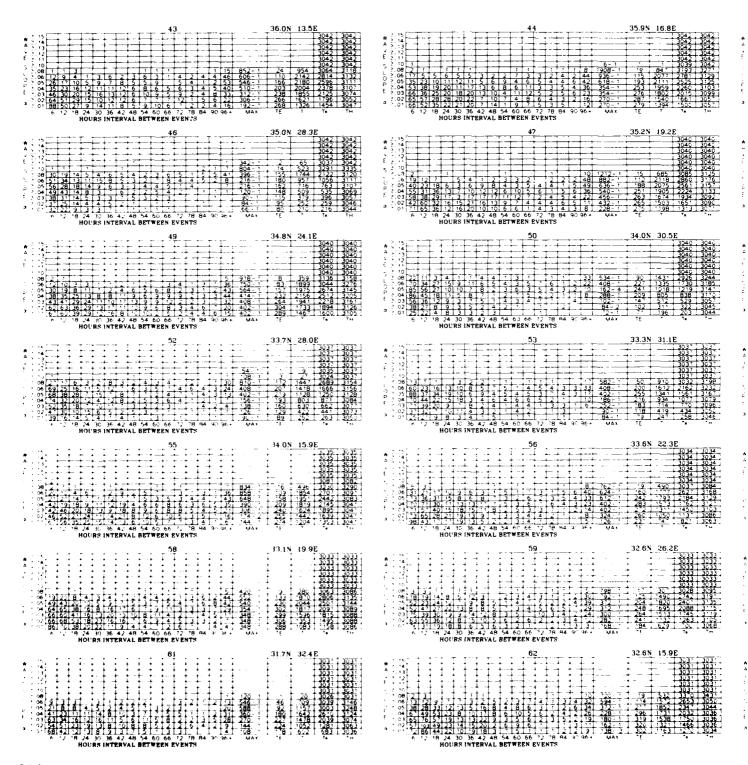
WAVE SLOPE (α) INTERVALS (Cont'd)



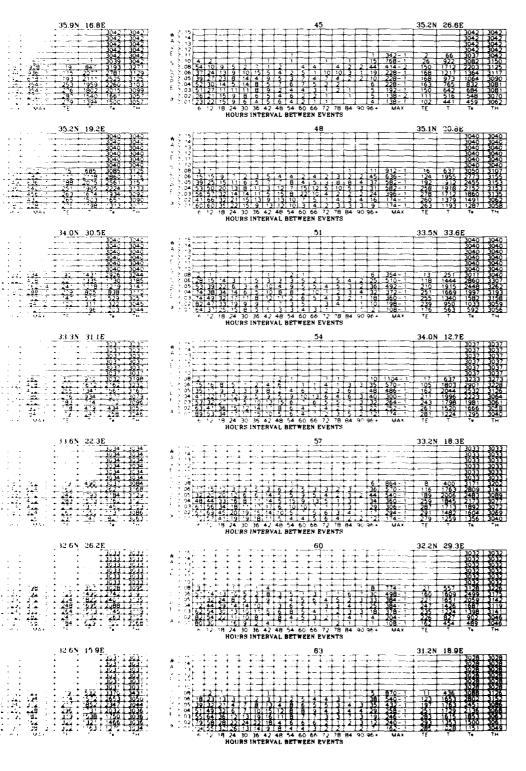
RVALS (Cont'd)

SUMMER



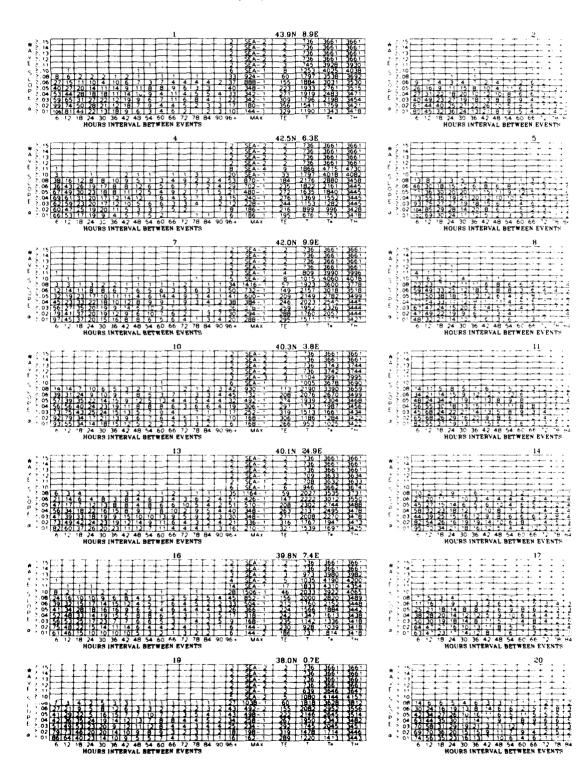


/AVE SLOPE (α) INTERVALS (Cont'd)



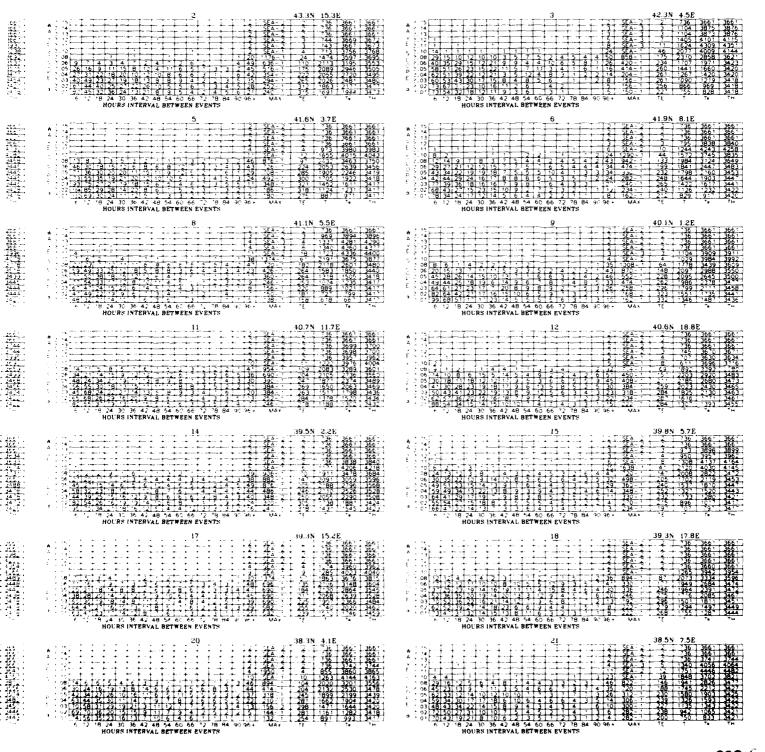
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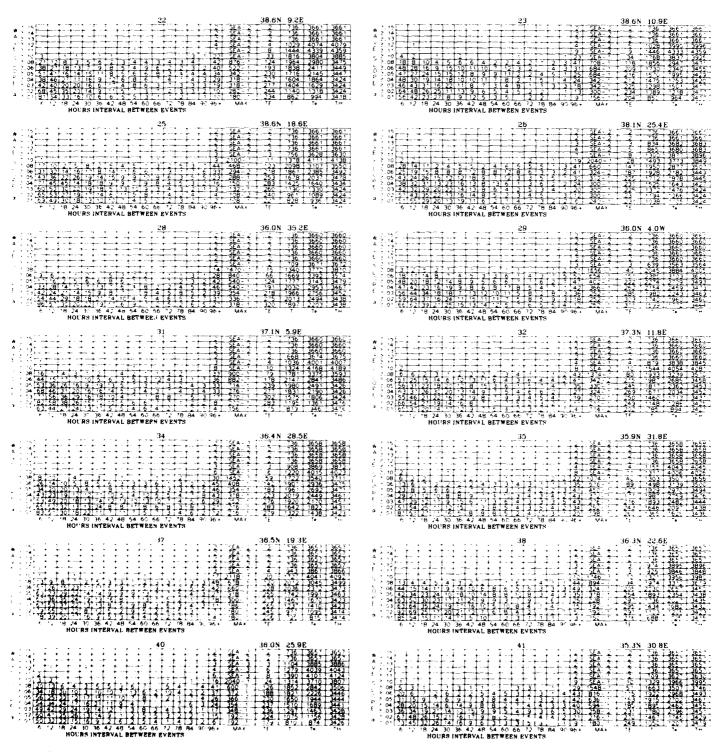
WAVE SLOPE (α) INTERVALS



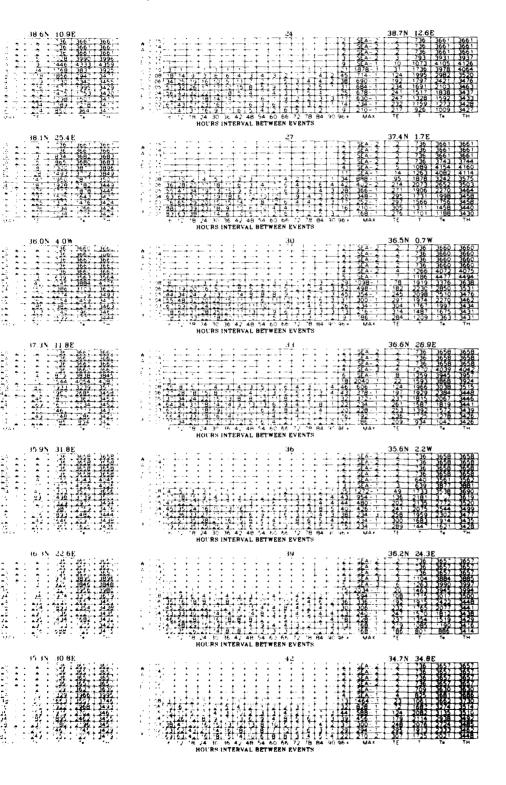
393 F

VALS FALL



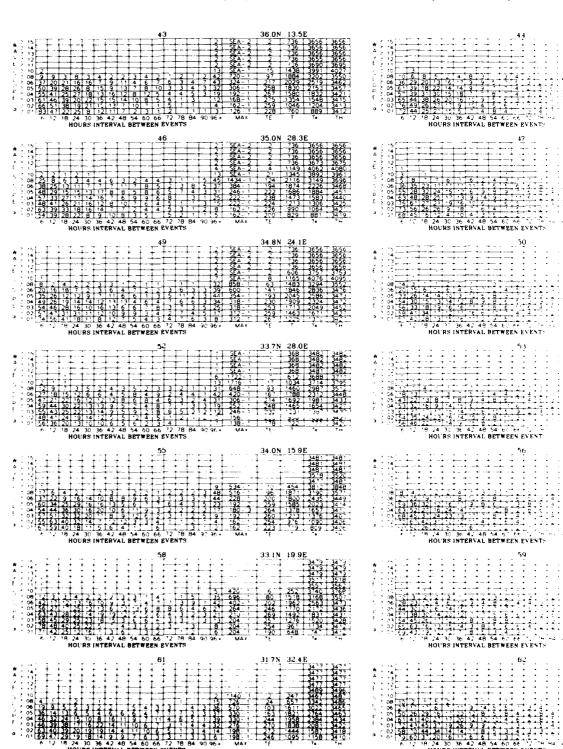


/E SLOPE (a) INTERVALS (Cont'd)

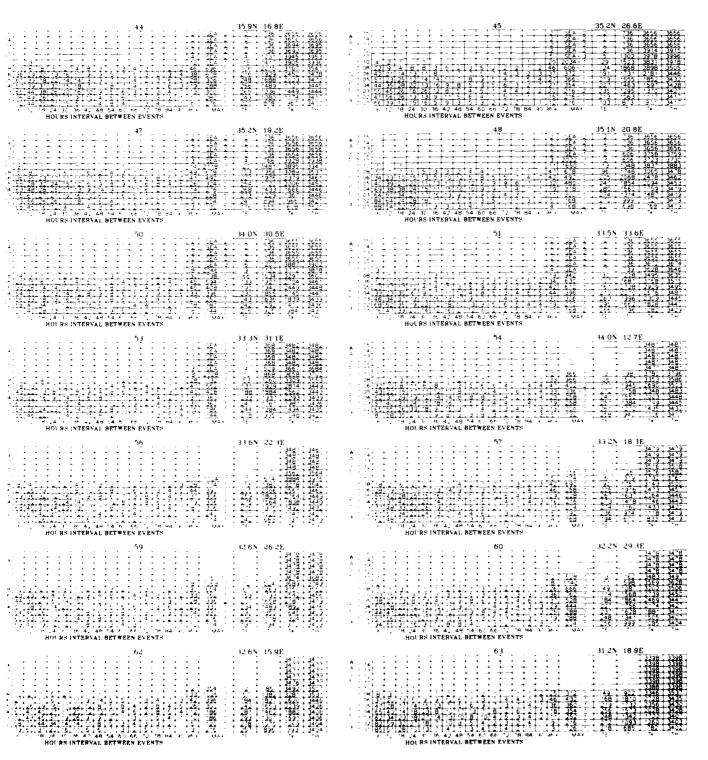


2000

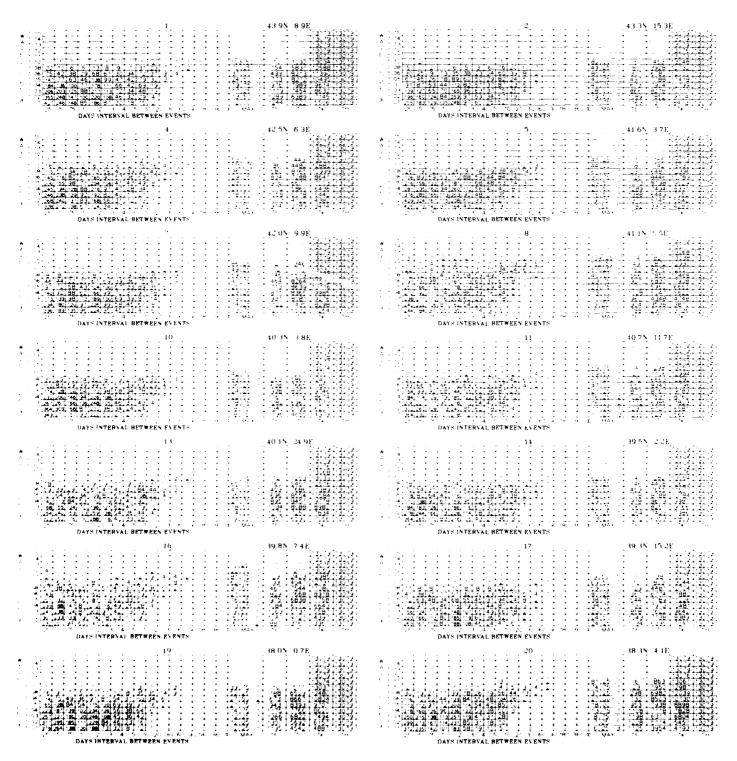
WAVE SLOPE (α) INTERVALS (Cont'd)



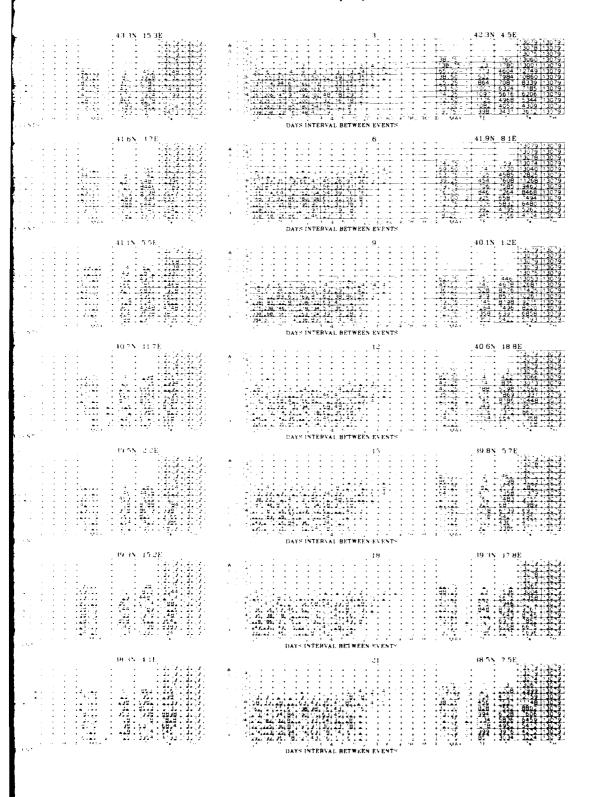
27.51



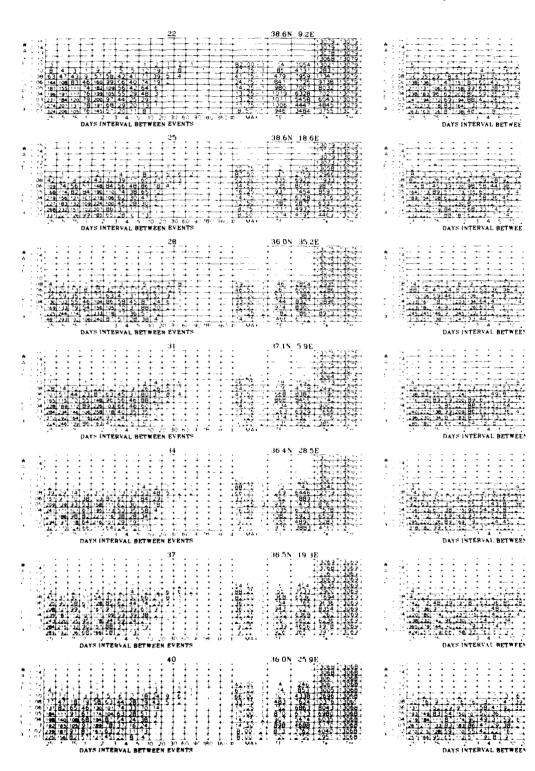
WAVE SLO



WAVE SLOPE (a) INTERVALS

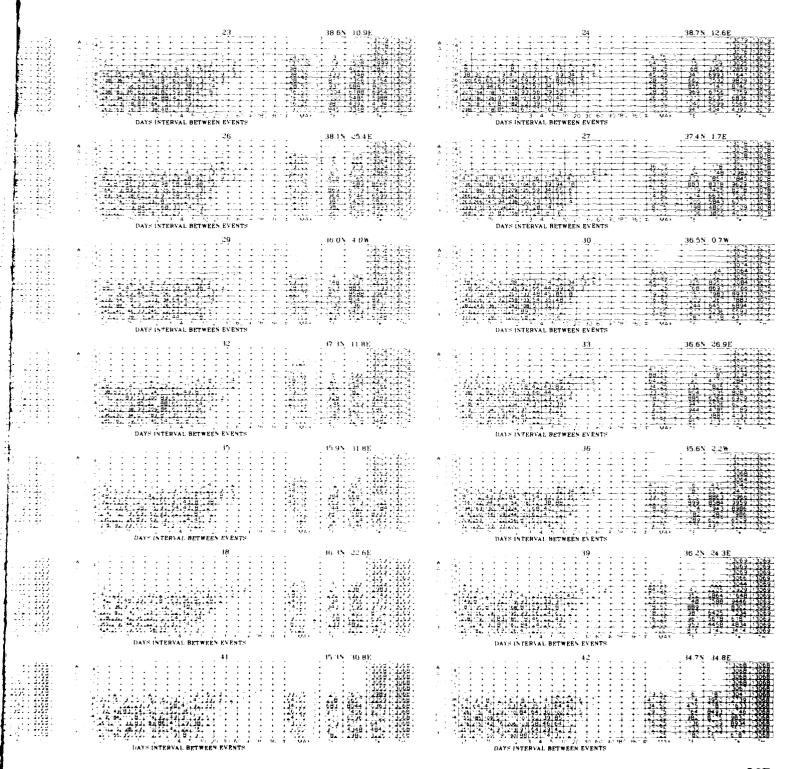


WAVE SLOPE (a) INTERVALS (Cont'd



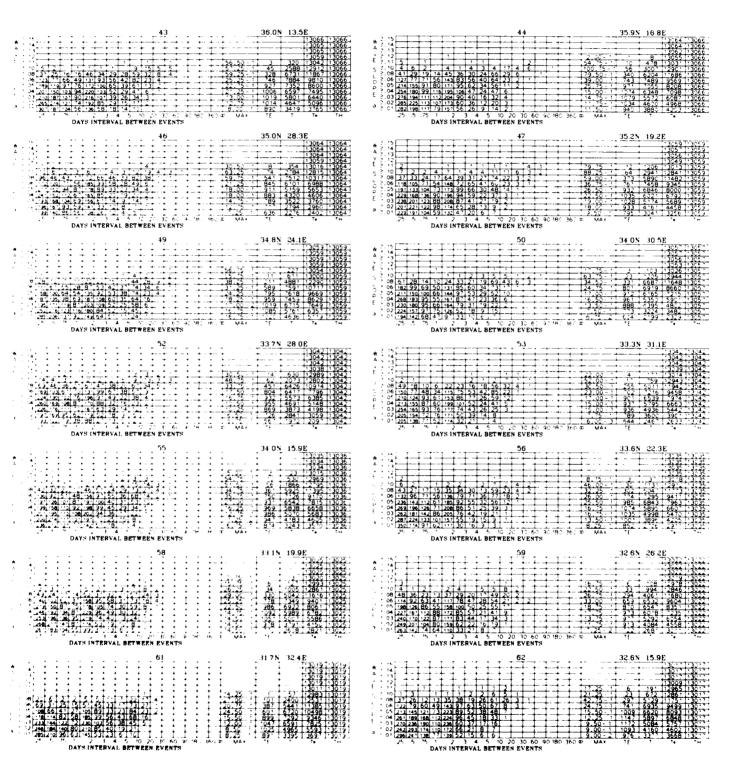
RVALS (Cont'd)

ANNUAL

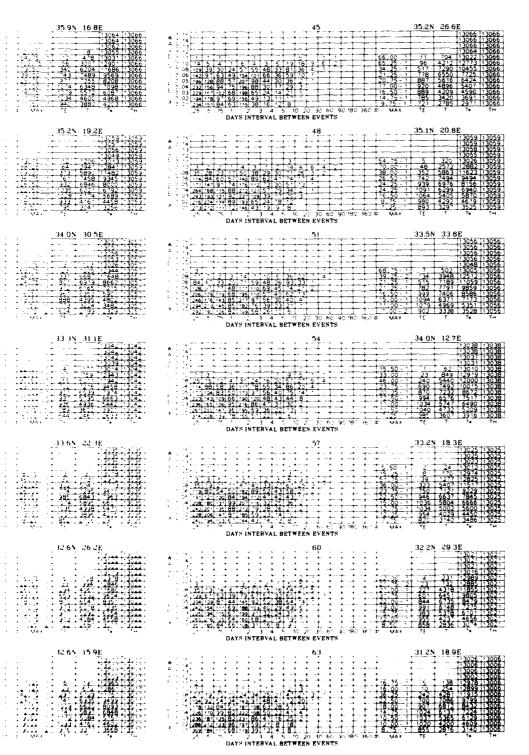


ANNUAL

WAVE SLOPE (a)



WAVE SLOPE (α) INTERVALS (Cont'd)



3 4 8 B

APPENDIX A SOWM DEVELOPMENT

Before 1975, FLENUMOCEANCEN relied on "singular" wave models to predict wind wave, and swell heights as well as their corresponding directions and periods. The basic weakness of the "singular" models is that they do not accurately depict the complex wave propagation in the larger oceans like the Atlantic and Pacific where several wave trains can coexist in one area at any given time.

The SOWM is a wave specification forecasting procedure that will describe the complex frequency-direction spectrum of waves in deep water with a reasonable resolution on a grid of points over the ocean. As originally planned, there were to have been four times as many grid points and twice the angular resolution for the spectra. The computer program exists for this higher resolution model, but it is not operational. Running time and memory allocation constraints made it necessary to reduce the number of grid points and decrease the angular resolution. This coarser grid can result in a misinterpretation of sub-grid scale features and fetch.

Since the SOWM is a general purpose deep-water model, it was not designed to include effects such as refraction, diffraction, shoaling, bottom and friction. consequence, SOWM output should be interpreted with a great deal of care for shallow water applications. Also, there are no wave-wave or wave-current interaction mechanisms; the latter have been observed to alter the wave fields in regions of a strong current like the Aguhlas Current and the Gulf Stream.

The grid of points were laid out on gnomonic subprojections of an icosahedron (a solid whose surface is 20 equilateral triangles) so as to allow great circle propagation. For each of the 20 triangles, a gnomonic projection is used. Thus, a straight line with any orientation on any of the 20 subprojections is a great circle. On the sphere, the sides of the equilateral spherical triangle intersect at an

angle of 72° and, thus, five tr common point. On a map, th equilateral triangle meet at ar each triangle is plotted projection.

The triangles are not orice way relative to the latitudes at the Earth. Instead, the icosal so as to maximize the number land. Fig. Al shows the 20 triverticies and edges appear projection. Each triangle consame area, and the marked distoprojection is evident.

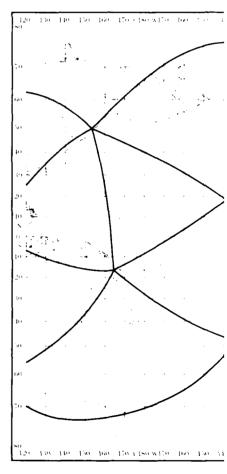


FIG. A1 The twenty All triangles

le of 72° and, thus, five triangles meet at a non point. On a map, the sides of the ilateral triangle meet at an angle of 60° , if a triangle is plotted as a gnomonic jection.

The triangles are not oriented in a simple relative to the latitudes and longitudes on Earth. Instead, the icosahedron was located as to maximize the number of verticies on d. Fig. Al shows the 20 triangles as their ticies and edges appear on a Miller jection 1. Each triangle covers exactly the e area, and the marked distortion of a Miller jection is evident.

Two sides of a triangle form a natural set of axes for each subprojection and the grid of points at which the SOWM spectra are computed are formed by the intersections of equally spaced lines drawn parallel to the two chosen sides of each subprojection as shown in Fig. A2. Each grid point, in principle, ought to be representative of wave spectra anywhere within the hexagon surrounding the grid point.

¹ A Miller projection is a cylindrical projection similar to a Mercator projection with less exaggerated spacing of the parallels at high latitudes.

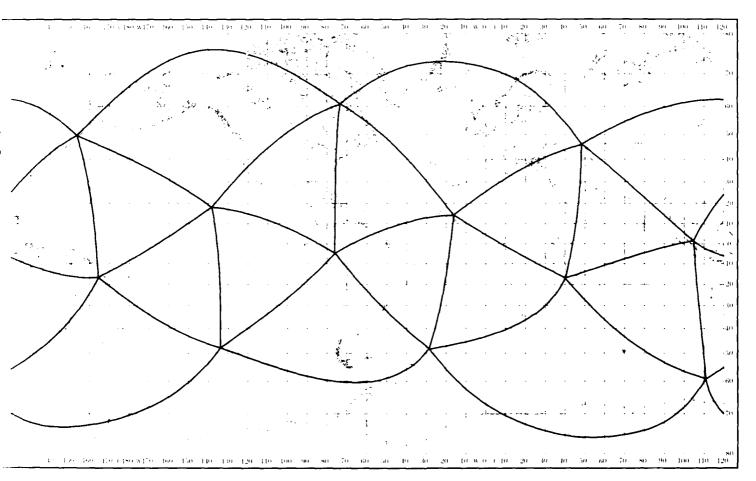


FIG. A1 The twenty equilateral triangles of the icosahedral gnomonic projection of the SOWM. All triangles are the same size on the Earth, but the Miller projection distorts them.

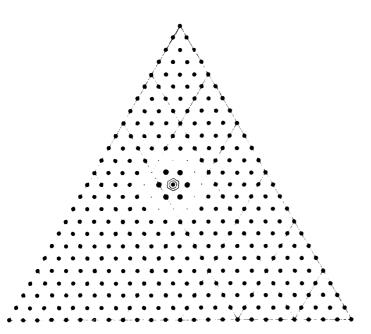


FIG. A2 The 325 grid points on a triangular gnomonic subprojection for the SOWM. Any straight line is a great circle. The hexagon around the circled dot shows the area represented by a grid point. The inner hexagon of heavy dots and the outer hexagon of X's show those grid points required to treat wave propagation effects at the circled point. (After Pierson, 1982)

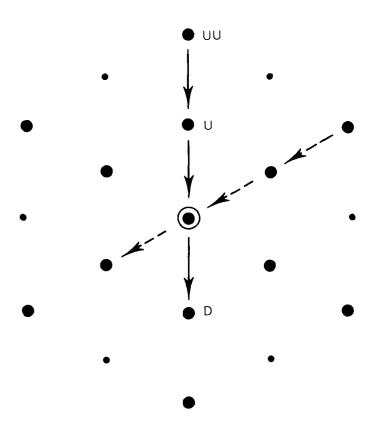
The great circle property is indicated by the fact that waves can travel to a given grid point along a great circle path from any one of the six surrounding grid points, thus accounting for six of the 12 direction bands in the model. The other six direction bands have directions of travel halfway between those for each of the primary directions. These spectral components are effectively treated as if they come from a source on the inner hexagon surrounding each grid point at a point halfway between two grid points. The distance involved is thus only about 85% of the primary distance as shown in Fig. A3.

Land boundaries and a prescribed ice limit act as sinks for spectral components. Grid points just south of the equator are treated as an artificial land boundary to provide appropriate sinks for southward moving spectral components and artificially fetch limited waves

for southerly winds at the equator. No swell from the Southern Hemisphere exists in the model, although tney could be appreciable just north of the equator during the Southern Hemisphere winter. Also, there is no specific provision for tropical cyclones in the model.

Once the grid, the spectral resolution, and the time step are prescribed, the model can compute what the spectrum will be at each grid point x hours later, given an initial wave spectrum and the winds at all grid points at the time, $t = t_{\rm O}$.

In the SOWM, this is accomplished by computing: (1) how much the wind-generated sea



SIX PRIMARY DIRECTIONS

FIG. A3 Grid points involved in propagation. The large d point a downward propagating spectral compone downstream point are shown. For secondary dir at the open circles — for one time step. The shift

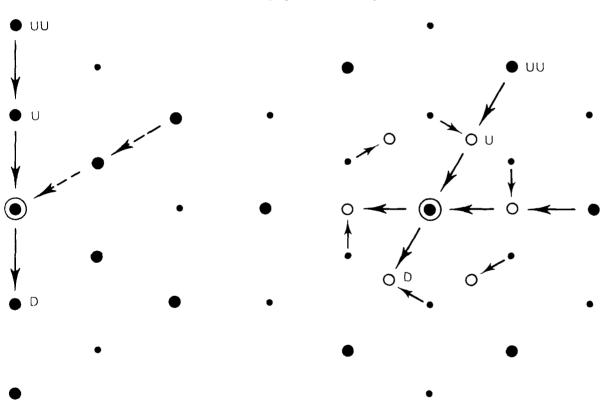
the equator. No swell emisphere exists in the ould be appreciable just r during the Southern so, there is no specific cyclones in the model.

e spectral resolution, and escribed, the model can rum will be at each grid given an initial wave at all grid points at the

this is accomplished by much the wind-generated sea

will increase or grow (if at all) during the next time step at each grid point; (2) how much the waves traveling against the wind $(\pm 90^{\circ})$ will be dissipated; (3) how far each spectral component will propagate at a representative group velocity along a great circle path in x hours; and, then reassembling the spectra for the end of the time step.

For brevity, these steps are called Grow, Dissipate, and Propagate. For the SOWM hindcasts at the end of a six-hour time step, within the resolution of the model, the new spectra at the grid points represented the waves at t=t+6 hours; new winds were then used, and the processes of Grow, Dissipate, and Propagate were repeated.



RY DIRECTIONS

SIX SECONDARY DIRECTIONS

olved in propagation. The large dots on the left are for the six primary directions. For the circled and propagating spectral component requiring an upstream point, an upper upstream point and a ant are shown. For secondary directions, the points on the inner hexagon are treated as if located these for one time step. The shift is reversed for the next time step. (After Pierson, 1982)

-1 I^2

APPENDIX B PARAMETER DERIVATIONS

The output from a SOWM hindcast includes a directional variance spectrum at each grid point as represented by 12 equally divided direction bands and 15 frequency bands of varying widths as depicted in Tables Bl and B2. The direction bands are unique for each grid point, but the frequency bands remain constant for all grid points (Table B2). The lowest possible frequency in a SOWM spectrum is 0.0388 Hz which corresponds to a period of 25.7 seconds.

Conversely, the highest frequency is which corresponds to a period of 3.24 The SOWM generates 'energy variances' cell within the 180 element matrix f wind fields. There is a certain confusion inherent in the terminolog variances' since the values within eac not energies. It is necessary t somewhat to appreciate the roots terminology.

In a steady Sea State the recor waves (a continuous time series of the fall of the sea surface at a point)

TABLE B1

AN EXAMPLE OF A DIRECTIONAL VARIANCE SPECTRUM

Wind Direction = 160° Wind Speed = 21.5 kn

Central Frequency (hz)

Direction (deg)	.308	.208	.158	.133	.117	.103	.092	.081	.072	.067	.062	.056	.050	.044	.039
96.6								,							
66.6															
36.6															
6.6															
336.6					i					,					
306.6										'					i L
276.6	1			.01	.06	.10	.15	.42	.15	.02		.02			{
246.6	.04	.13	.18	.13	.13	.11	.05	.03	.01			.01		 	
216.6	.06	.20	.35	.29	.33	.18	.06	.02						<u> </u>	}
186.6	.06	.20	.37	.30	.28	.01	.09	.02		-				})
156.6	.04	.14	.20	.14	.12	.01	.03	.01			ļ			;	{
126.6	.03	.08		.04	.03										
Frequency Spectrum	.23	.75	1.10	.91	.95	.41	.38	.50	.16	.02		.03			

Derived parameters: $H_{m_0} = 9.3$ ft., $T_p = 8.57$ s., $\alpha = 0.085$, PWD = 212° , $\rho_c = 0.77$

responds to a period of 3.24 seconds. generates 'energy variances' in each in the 180 element matrix from input ds. There is a certain amount of inherent in the terminology 'energy' since the values within each cell are gies. It is necessary to digress to appreciate the roots of this gy.

steady Sea State the record of the continuous time series of the rise and he sea surface at a point) does not

NCE SPECTRUM

- 21.5 kn

 $^{\circ}$, $ho_{
m c}$

0.77

7	.062	.056	.050	.044	.039	Directional Total
!						
?		.02				.93
		.01				.82
						1.49
						1.33
						.69
						.18
2		.03				5.44 Total (ft ²)
L						-(1(-)

repeat itself exactly from one wave to the next because the waves are a superposition sinusoids with many different frequencies and Every wave record of directions of travel. finite length as a function of time, however, can be decomposed into harmonics. The zeroth harmonic is the mean elevation of the sea and is assumed to be zero for the analysis since the contributions from much longer periods such as the tides are constants during the time of observation. The first harmonic, is a least squares fit of a sinusoid with a period equal to the wave record with its peak positioned such that its amplitude is maximized.

TABLE B2

BAND NUMBER, BAND WIDTH, CENTRAL FREQUENCY
(AS A FRACTION AND A DECIMAL), PERIOD, AND
BANDWIDTH BOUNDS (After Pierson, 1982)

DANDWIDTH BOONDS (After Fierson, 1962)											
Band Number	Band Width x 180	Central Frequency	Central Frequency	Period	Lower Bound x 180						
1	24	55.5/180	0.30833	3.24	43.5	67.5					
2	12	37.5/180	0.20833	4.8	31.	43.5					
3	6	28.5/180	0.15833	6.32	25.5	31.5					
4	3	24.0/180	0.13333	7.5	22.5	25.5					
5	3	21.0/180	0.11666	8.57	19.5	22.5					
6	2	18.5/180	0.10277	9.73	17.5	19.5					
7	2	16.5/180	0.09166	10.91	15.5	17.5					
8	2	14.5/180	0.08055	12.4	13.5	15.5					
9	1	13.0/180	0.07222	13.85	12.5	13.5					
10	1	12.0/180	0.0666	15.0	11.5	12.5					
11	1	11.0/180	0.06111	16.4	10.5	11.5					
12	1	10.0/180	0.0555	18.0	9.5	10.5					
13	1	9.0/180	0.050Ō	20.0	8.5	9.5					
14	1	8.0/180	0.0444	22.5	7.5	8.5					
15	1	7.0/180	0.0388	25.7	6.5	7.5					

harmonic has one maximum and minimum for the entire wave record. The second harmonic has a period of one-half the wave record with its two peaks positioned such that it too has maximum amplitude. Each subsequent harmonic can be thought of as a least squares fit of a sinusoid with the number of peaks and valleys (or the period) increasing (decreasing) corresponding to the harmonic number. By adding each harmonic to the preceding harmonics, harmonics or the 'Fourier Series' begin to resemble the wave record. If the number of observations on the wave record is N, then N/2harmonics will completely describe the wave record.

The average energy in the wave motion per unit area is described by:

$$E = \frac{1}{2} \rho g a^2 \tag{B1}$$

where ρ is the density of the ocean water, g is the acceleration of gravity, and a is the wave amplitude. Half of the energy is kinetic, and the other half is potential.

Recalling that each wave record can be decomposed into a number of harmonics, then if the amplitude of each harmonic is squared, multiplied by $(\frac{1}{2} \rho g)$, and plotted on a graph as the ordinate using the associated frequency or period of the harmonic as the abscissa, the resulting graph is a 'wave energy spectrum.' Initially it was customary to present spectrum in this manner (World Meteorological Organization, 1976), but since the magnitude of the right-hand side of Eq. Bl is dominated by (a^2) the multiplication of (ρg) is now omitted. This is the format of the data generated in the SOWM hindcasts. Each cell in Table Bl can be summed to yield the quantity $(1/2a^2)$. omission of (pg) transforms the 'wave energy spectrum' into an 'energy variance spectrum' or more appropriately 'variance spectrum,' since the sum of each cell in Table Bl will equal the variance of the spectrum of the wave record it is representing. Likewise, the area under a variance spectrum curve as derived from the frequency spectrum totals in Table Bl will equal the variance of the spectrum represented.

WAVE HEIGHT

In Table B1 each quantity within the cells of the table has units of ft2, and cells without any values contain component variances less than 0.01 ft². Such small values were considered insignificant, and were not retained in the output generated from the SOWM hindcast. total variance of each spectrum can be converted to a spectral wave height parameter (H_{m_0}) which closely corresponds to the significant wave height $(H_{1/3})$. The significant wave height on a wave record is defined as the average height of the highest one-third of the wave heights. $(\overline{H}_{1/3})$ has been shown to quantity approximate the characteristic wave height 1964; observed visually (Cartwright, Nordenstrom, 1969). The spectral wave height parameter (H_{m_0}) from Rayleigh statistics is defined as:

$$H_{m_0} = 4 (m_0)^{\frac{1}{2}}$$
 (B2)

where m_{O} is the sum of the component variances of all cells of Table Bl. The quantity (m_0) is commonly referred to as the moment of order zero. The correspondence between $\rm\,H_{m_{0}}$ and $\rm\,\widetilde{H}_{1/3}$ is strictly valid for a spectrum with most of its energy or variance concentrated over a range of frequencies, but approximation in the cases with a broader sufficiently close spectrum is for practical applications (World Meteorological Organization, 1976).

WAVE PERIOD

The choice of the modal or peak wave period (T_D) is based upon the 'variance densities' of the point spectrum. 'Variance densities' with dimension of ft2-sec are obtained by dividing the variances by the frequency bandwidth. the SOWM the bandwidths vary in size from 0.00560 to 0.1333 Hz. After dividing by the bandwidth, the energies are standardized with respect to one another. T_{p} can then be obtained choosing the central frequency, corresponding period, associated with the peak variance density. In Table Bl, T_p is associated with the central frequency of 0.117 Hz, which equates to a period of 8.5 seconds. The problem

HEIGHT

antity within the cells f ft², and cells without nent variances less than values were considered not retained in the The e SOWM hindcast. pectrum can be converted t parameter (H_{mo}) which the significant wave ificant wave height on a s the average height of the wave heights. The een shown to roughly teristic wave (Cartwright, 1964; spectral wave height Rayleigh statistics is

 (B^2)

he component variances. The quantity (m_0) is the moment of order e between H_{m_0} and $\overline{H}_{1/3}$ spectrum with most of e concentrated over a equencies, but the cases with a broader tly close for most (World Meteorological

'ERIOD

odal or peak wave period variance densities' of iance densities' with obtained by dividing quency bandwidth. In so vary in size from fter dividing by the are standardized with Tp can then be obtained tral frequency, or ociated with the peak le Bl, Tp is associated y of 0.117 Hz, which 5 seconds. The problem

associated with an ill-defined modal period of a specific spectrum, as occurs when there is only a small difference between the variance densities of two or more frequency bands, is minimized due to the large number of spectra included in the summaries presented in this atlas.

WAVE SLOPE

The slope associated with very high waves is considered by many ship designers to be a major contribution to operational failures. The wave slope is often estimated using the ratio of the wave height (H) to the wave length (L). However, the relationship usually used to obtain the wave length:

$$L = 5.12T^2 \tag{B3}$$

where T is the wave period in seconds and L is the wave length in feet is valid only when the wave is a simple periodic sine wave. Pierson (1955) clearly states that Eq. B3 does not hold for the irregular sea surface. The assumptions under which Eq. B3 was derived are violated outside of the wave tank. An alternative method of estimating the wave slope is needed. Since the SOWM provides a frequency spectrum of wave energy this information is used directly in this atlas to calculate a wave slope parameter (α).

The wave slope parameter, α , is defined by:

$$\alpha = (m_{\underline{\lambda}})^{1/2}/g \tag{B4}$$

where m_4 is the moment of order four (the fourth moment). The moments are defined by:

$$m_{n} = \sum_{i=1}^{\kappa} v_{i} \omega_{i}^{n}$$
 (B5)

where ω is the circular frequency, n is the order of the moment, V_1 is a component variance, and κ is the number of frequency bands. The parameter α is the root mean square of the absolute slope at any fixed point. Cummins and bales (1980) derived the wave slope parameter α . It should be noted that α is more strongly influenced by the shorter, higher frequency components of the spectrum than by the

larger, longer, but not so steep waves near the modal frequency. Thus, a "rough sea" as measured by α , does not necessarily imply a "high sea." Information regarding the significance of its range of values can be calculated from the derivation of the root mean square wave slope of a regular wave. The resulting equation is (Gentile, 1982):

$$\alpha = \sqrt{\frac{\pi}{2}} \frac{\frac{H_W}{W}}{L_W}$$
 (B6)

where H_W is the wave height (crest to trough) and L_W is the wave length. Information in Table B3 is based upon Eq. B6.

TABLE B3

APPROXIMATE VALUES OF WAVE LENGTH
TO WAVE HEIGHT FOR ASSOCIATED VALUES
OF THE WAVE SLOPE PARAMETER (a)

Wave Slope Parameter (a)	Ratio Wave Length (L) to Wave Height (H)	Angle of Wave Slope Tan ⁻¹ (H/L)
0.01	222.0	0.30
0.02	111.0	0.59
0.03	74.0	0.80
0.04	55.5	1.0"
0.05	44.4	1.3°
0.06	37.0	1.50
0.08	27.8	2.10
0.10	22.2	2.6"
0.11	20.2	2.8"
0.12	18.5	3.10
0.13	17.1	3.3"
0.14	15.9	3.6°
0.15	14.8	3.9^{o}

PRIMARY WAVE DIRECTION DIRECTIONALITY

The primary wave direction (PWI-directionality (c) are two parameter derived from the directional spectrum opposed to the frequency spectrum tot definition of the PWD is taken direct FLENUMOCEANCEN's 1981 version operational SOWM computer program 1981). The PWD is determined by a process. First, the maximum variance the directional totals is identified, one of the twelve directional bands. following true-false tests are persequence.

$$V_{m} > \sqrt{2} \begin{bmatrix} 12 \\ \Sigma \\ i=1 \end{bmatrix} V_{i}$$
 i $\neq m$

$$V_{m,m+1} > \sqrt{2} \begin{bmatrix} 12 \\ \Sigma \\ i=1 \end{bmatrix} V_i$$
 $i \neq m$

$$V_{m,m+1,m-1} > \sqrt{2} \begin{bmatrix} 12 \\ \Sigma \\ i=1 \end{bmatrix} i \neq m$$

where i is one of the 12 directional V_{m+1} is the higher of the directional variances.

If Eq. B7 is true, then the

RIMARY WAVE DIRECTION AND DIRECTIONALITY

The primary wave direction (PWD) and the tionality ($_{\rm C}$) are two parameters which are ed from the directional spectrum totals as the total the frequency spectrum totals. The direction of the PWD is taken directly from the PWD is taken directly from the PWD is total source of their tional SOWM computer program (Lazanoff, The PWD is determined by a multi-step so. First, the maximum variance ($V_{\rm m}$) in insectional totals is identified, where m is the twelve directional bands. Next, the wing true-false tests are performed in the.

$$> \sqrt{2} \left[\sum_{i=1}^{12} V_i \right] \quad i \neq m$$
 (B7)

$$\int_{1}^{\infty} \frac{1}{1} > \sqrt{2} \left[\sum_{i=1}^{2} V_{i} \right] i \neq m$$
 (B8)

is one of the 12 directional bands, and is the higher of the two adjacent ional variances.

: Eq. B7 is true, then the I is the

direction associated with V_m . If B7 is ralse, Eq. B8 is tested; and thusly for Eq. B9. For the first successful test of Eq. B8 or B9, the vectors defined by the directions and variances of the quantities on the left-hand side of the inequalities are summed and the resultant direction defined as the PWD. If Eq. B9 is false, then the PWD is not defined, and a confused sea state is assumed. The methodology used for defining the PWD is somewhat arbitrary, but the technique has proved quite useful operationally (Lazanoff, 1981).

The degree of directionality is defined by:

$$\rho_{c} = (\rho_{x}^{2} + \rho_{y}^{2})^{\frac{1}{2}}$$
 (B10)

where

$$\rho_{c} = (1/m_{o}) \sum_{i=1}^{12} V_{i} \sin \theta_{i}$$
 (B11)

$$\rho_{y} = (1/m_{o}) \sum_{i=1}^{12} V_{i} \cos \theta_{i}$$
 (B12)

The angle 0 is the direction associated with the variances in the directional spectrum totals. The directionality has a value of one for an unidirectional sea state, and a value of zero when there is a completely symmetric distribution of variance around the compass. This parameter has the same properties as the 'constancy' parameter, often used in climatological wind summaries.

APPENDIX C

SOME APPLICATIONS OF CONTINGENCY TABLES

l. Question: What is the Climatological probability of having wave heights less than 20 ft at $41^{\circ}N$, $004^{\circ}E$ in Autumn?

Sample Application: A war at sea exercise is planned for 10 through 19 November at 41°N, 004°E. order to complete all phases of the exercise within the 10 day period available, at least 7 days (not necessarily consecutive) with significant wave heights less than 20 feet are needed. Based on climatology, will 10 days probably be enough time to complete all phases of exercise?

Answer:

Proceed to the November wave height and wind speed contingency table for the grid point nearest to 41°N. 004°E. From Table 1 or Fig. 1 (Mediterranean map) we find that this is the contingency table for sequence number (For illustrative purposes contingency table from "Legends for Tables" is used in the following solution.) climatological probability of having wave heights <20 ft can be found by adding the percent frequency of occurrences in the "T" or total column for wave heights <20 ft. The result is 2+3+9+14+20+17 = 65%. This means that on the average 65% of the time waves less than 20 ft will be encountered during November. Since 10 days have been allowed for the exercise on average 10 X .65 = 6.5 days will significant wave heights than 20 ft. Thus based

climatology, 10 days probably not be enough tir complete the exercise. How if the exercise period coul extended to 11 days, on av 7.2 days (.65 X 11) would less than 20 ft waves and exercise could probably completed.

2. Question:

How can the tables be utiliz predict the efficiency o vessel, system, or operation a given area and time of year?

Answer:

Operational enhancement environmental tuning may realized through the foll procedure:

- (a) Identify the de acceptable joint frequency occurrence for the parameter interest, i.e., wave height wind direction, wave height wave slope, etc.
- (b) Extract the joint pe frequency of occurrence for parameter(s) of interest from appropriate contingency table the desired time interval (meseason, or annual), for area(s) of interest.
- (c) Derive probabilities efficiency by determining percent of the time that identified environmentations fall within desired operable limits.

3. Question:

How can the tables be used assess how the environment have been a contributing fi in the failure or damage (system, operation, or equip-(Note: This does not pertain failures due to a spe episode, but rather to fai. which result from cumula stresses over a signif: portion of the "lifespan").

timatology, 10 days will robably not be enough time to omplete the exercise. However, of the exercise period could be a ktended to 11 days, on average a 2 days (.65 X 11) would have be as than 20 ft waves and the kercise could probably be empleted.

bw can the tables be utilized to redict the efficiency of a cassel, system, or operation, for a ligiven area and time of the rear?

perational enhancement by avironmental tuning may be palized through the following e rocedure:

g i) Identify the desired teeptable joint frequency of currence for the parameters of factors, i.e., wave height and lind direction, wave height and live slope, etc.

Extract the joint percent percent percent percent percent for the immeter(s) of interest from the expropriate contingency table for the desired time interval (month, ason, or annual), for the per(s) of interest.

Derive probabilities of ficiency by determining the ficent of the time that the lentified environmental editions fall within the fixed operable limits.

sess how the environment may been a contributing factor the failure or damage of a stem, operation, or equipment? This does not pertain to three due to a specific foode, but rather to failures ich result from cumulative resses over a significant ration of the ship's lifespan").

Answer:

Inputs to assess environmental impact on a system of operation may be gathered by:

- (a) Identify the area(s), time (month) of failure or damage.
- (b) Identify the wind and wave conditions which if exceeded would probably cause damage or failure.
- (c) Derive the percent of occurrence of conditions, exceeding those conditions identified in Step 2, for the corresponding area(s) and time (Silver and Bales, 1983).

4. Question: How can these tables assist in ship design?

Answer: For example, U. S. Navy ship designers follow four steps when applying the information contained in this atlas to design.

(a) Define the mission of the vessel, and determine the significant wave heights in which the mission must be performed at required levels of efficiency.

EXAMPLE

	Maximum Allowable Ship Motion							
Operation of Aircraft		50 j	roll		<13			
Continuous Total Mission			rol1		13-			
Limited Operation		150	rol1		20-			
Survivability		N/A			>46			
(b) Identify the area(s)	of		5.	Question:	How c			
operation.					in pl			
(c) Extract wave height perc								
	ave			Answer:	Ship			
2018 4114 11111111 1111111111111111111111	fod				enhar			
	the				atlas			
appropriate area(s). This can	ı be				simil			
done monthly and annually.					desig			
(d) To calculate ship respon					ocear			
derive the percentage					desi			
,					time			
unsuccessful mission operation	_				(a)			
using the percent frequencies occurrence of the signific					the s			
wave height operating envelopment					heigh			
with the joint frequencies					speci (b)			
occurrence of significant w					geogr			
height and modal wave per					(c)			
(Bales, 1983; Comstock, Bal					which			
and Gentile, 1982). If					(e.g.			
percentages of success derived					occui			
Step (d) are unsatisfactory					heigh			
	the				occui			
-					extra			
vessel's hull configuration					the			
meet the operating envelope.					tabl			
					-			

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EXAMPLE

	mum Allowa Motion	able	Significant Wave Height
41	5° roll 10° roll 15° roll N/A		<13 ft (4m) 13-20 ft (4-6m) 20-30 ft (6-9m) >46 ft (14m)
) of	5.	Question:	How can these tables be utilized in planning a ship trial?
Wave alleriod the the fan be toonses of and heon by fis of y icant milopes tas of the wave ceriod at ales, cethe defin for the toye		Answer:	Ship trial planning can be enhanced through the use of this atlas by following a procedure similar to that used by the ship designer to identify areas of the ocean likely to provoke the desired ship motions at a given time of the year. (a) The first step is to define the seaway (upper and lower wave height limits) best suited for specific tasks of the ship trial. (b) Identify the general geographic area of the trial. (c) Identify the times (months) which have acceptable probability (e.g., 50%, 75%, 80%, etc.) of occurrence of the desired wave heights. Probabilities of occurrence can be derived by extracting the wave height from the wave height contingency tables.

APPENDIX D

DURATION AND INTERVAL TABLES

In the seasonal tables, durations intervals that are underway at the beginning of a season are treated as if they began on the first day of the season. The other alternative, going backwards in time into the previous season to search for the actual beginning time, was considered less appropriate for planning purposes. When a mobile platform (ship) arrives at a location at some arbitrary time, duration of the current episode previous to ship's arrival is not usually important. ship is affected only by the number of hours the episode is likely to continue for the time the ship remains in that vicinity. It is not particularly important that the beginning of a season was used for the start-up of duration or interval frequencies, whereas, actual operations may be scheduled to begin at times other than the beginning of the season; episodes are likely to occur in a near-random manner through the course of specific seasons. In terminating durations and intervals, episodes that carried beyond the end of the season were counted until they actually ended or they continued for more than one season (90 days), whichever occurred first. This prevents episodes from becoming artificially short simply due to the ending of the season. For example, if a plan calls for a ship to be at a specific location near the end of the season and remain in that vicinity for several weeks into the next season, the planner only needs to check the table for the season in which he plans to arrive and not a subsequent table for some later season.

In the summary tables covering all seasons, durations and intervals that are underway at the beginning and end of the period of record are not counted. These summary tables represent the wind or wave environment at a fixed position over the 10-year hindcast period. By assuming a stable climate and using appropriate statistical procedures, these tables can be used to estimate conditions which would affect a fixed platform for the expected lifetime of the

platform at a fixed position.

Missing data were not replaced wit estimated values. When missing data were encountered, the ongoing and subsequent episode were excluded from the duration and intervative frequencies. This tends to reduce the number of very long-duration events common to the summar tables covering all seasons. It has littleffect on the statistics for shorter duratic phenomena.

Definitions of column trailers in the duratic and interval tables (see 'Legends for Tables' are as follows:

- MAX: The maximum duration (c interval) in hours, followed t the number of times an episode c that length occurred. abbreviation "SEA" th in seasonal tables represent episodes that lasted one seasc or longer.
- TE: The number of events satisfyin the stated criteria. An even begins with the wind speed, wav height or slope increasing to the given threshold.
- TI: The number of intervals. Thes are episodes not satisfying the stated criteria. An interval begins with the wind speed, was height or slope falling below the given threshold.
- T: The total number of hindcast that were included in (TE) c (TI).
- T*: The total number of hindcast that met the stated criteria This is more than T if missir data made the duration of interval impossible to determine It can be used to determine the probability of encountering the conditions specified (I computing T*/TH).

position.

were not replaced with When missing data were going and subsequent episodes the duration and interval tends to reduce the number of events common to the summary seasons. It has little stics for shorter duration

rn trailers in the duration (see 'Legends for Tables')

maximum duration (or rval) in hours, followed by number of times an episode of length occurred. The reviation "SEA" in the sonal tables represents des that lasted one season over.

number of events satisfying stated criteria. An event ins with the wind speed, wave int or slope increasing to the en threshold.

number of intervals. These pisodes not satisfying the ted criteria. An interval ins with the wind speed, wave the or slope falling below the on threshold.

total number of hindcasts twere included in (TE) or

total number of hindcasts to met the stated criteria. It is more than T if missing a made the duration or cryal impossible to determine. It is used to determine the bability of encountering the ditions specified (by buting T*/TH).

TH: The total number of hindcasts examined.

If the number of the 'duration of events' or 'intervals between events' exceeds 999, the symbol 'K' is used to denote thousands, and the ' \geq ' symbol is used to denote greater than or equal to. For example, \geq 1K implies greater than or equal to 1,000 durations or intervals. In order to correctly interpret the tabulations, specific examples of the various types of duration and interval tables are provided in the 'Legends for Tables.'

When answering questions using the duration and interval tables, it is important distinguish between questions that require the use of the number of episodes and those that require the number of hindcasts. questions regarding the percentage of time at or above, or below, certain thresholds require the use of the number of hindcasts. On the other hand, questions concerned with the percentage of episodes at or above, or below, thresholds demand the use of frequencies, where a one-day episode and a 60-day episode will each count as one episode.

The following examples are provided to illustrate applications of the tables. The numbers in the examples are extracted from the sample tables in the legends. Regardless of the type of parameter used (wind speed, wave height or slope), the procedures are not altered.

APPLICATIONS OF DURATION AND INTERVAL TABLES

Question: Of all the events with winds of 34 knots or more during a particular season, what percentage had durations of longer than one day?

Sample Application: Winds have just increased to gale force (34 knots or more) at a ship's location. What is the climatological probability that the gale force winds will persist longer than one day?

events number of (or episodes) >34 knots is 39 (from the TE column of the duration table in the 'Legends Tables'). The number of events of winds >34 knots lasting more than one day is 1 + 3 + 1 + 1 =6. The percentage of events with winds >34 knots lasting one day or more is thus 6 39 \times 100% = 15.4%.

Question: What percentage of the time during a particular season can waves greater than or equal to 20 ft be expected to persist longer than 24 hours?

Answer:

Sample Application: Carrier flight operations have been scheduled for a specified operating area during particular a season. Flight operations need to commence within 24 hours of arrival within the operating area. They cannot be conducted if the significant wave height is 20 ft or more. What is the climatological probability that the carrier will be unable to conduct flight operations in the operating area for more than 24 hours due to high seas?

Answer: This problem involves computations using hindcasts from seasonal duration rather than episodes from the duration table since we are answering a question regarding the percentage of time. solution can be found by computing the joint percentage as follows: (percent of waves >20 ft times percent of >20 foot waves that persist longer than 24 hours). Note that the percent of >20 foot waves that lasted <24 hours plus the percent of >20 foot waves that lasted >24 hours is 100% so we can compute

whichever is eas from 100% Percentages are the difference becaused by missing Compute the percentages that lasted this example it find the percent then subtract from the percent we require the call total number of this criterion.

This procedure is

Duration	Hindcasts Per Event	Frequ (From
6 hours 12 hours 18 hours 24 hours	1 X 2 X 3 X 4 X	
	Thus, the waves that (63 175) percent of >24 hours 64.0%. Step 2. Tfeet is (181 12 Step 3. T14.6% = 9.	laste X 100: ≥20 f is he per (T*/TH 36) X he ans
	NOTE: If for a pe seasons an would be to for each seexpected do	riod appro calca eason

Question: Considering all between events

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whichever is easier and subtract 100% if necessary. Percentages are used because of the difference between T and T* caused by missing data. Step 1. Compute the percent of >20 foot waves that lasted >24 hours. this example it will be easier to find the percent for <24 hours then subtract from 100% to obtain the percent we require. requires the calculation of the total number of hindcasts meeting this criterion.

This procedure is as follows:

)uration	Hindcasts Per Event		Frequency (From Table)		Hindcasts ≥20 ft Lasting ≤24 Hours
					
6 hours	1	Х	7	=	7
li hours	2	Χ	2	=	4
l8 hours	3	Х	8	=	24
14 hours	4	X	7	-	28
			TOTAL:		63

Thus, the percent of ≥ 20 foot waves that lasted ≤ 24 hours is (63 175) $\times 100\% = 36.0\%$. The percent of ≥ 20 foot waves lasted ≥ 24 hours is 100% - 36.0% = 64.0%.

Step 2. The percent of waves ≥ 20 feet is (T*/TH) X 100% or (181 1236) X 100% = 14.6%. Step 3. The answer is 64.0% X 14.6% = 9.4%

NOTE: If an answer is required for a period which spans two seasons an approximate procedure would be to calculate the answer for each season to get a range of expected duration or intervals.

Question: Considering all the intervals between events with significant

wave heights greater than or equal to 9 feet during a specific season, what percentage persisted more than 24 hours?

Sample Application: A tug has just arrived at the location of a salvage operation. Seas are less than 9 ft. In order to successfully conduct the salvage operation, the significant wave height must remain less than 9 ft for at least 24 hours. What is the climatological probability that the operation can successfully be conducted?

Answer: This problem involves the use of the seasonal interval tables, since we want intervals between wave height >9 ft. The number of intervals between events of waves >9 ft is 72 (from the TI column of the interval table). intervals between of events (episodes) of wave height >9 ft lasting 24 hours or less is $\overline{12} + 13 + 5 + 8 = 38$. The percentage of intervals between waves >9 ft lasting 24 hours or less is thus $(38 72) \times 100\% =$ 52.8%. In other words, 52.8% of all the episodes with waves <9 ft persisted 24 hours or less, and the percentage of <9 ft wave episodes lasting longer than 24 hours is 100% - 52.8% = 47.2%. climatological the probability that the operation can successfully be conducted is 47.2%.

4. Question: What percentage of the time can significant wave heights less than 12 ft be expected to persist longer than two days?

Sample Application: A particular location is being considered as an ASW (anti-submarine warfare) exercise area. Significant wave heights

less than 12 ft are required for the exercises, which normally last at least two days. annual basis, what percentage of the time could exercises be successfully conducted at the location?

Answer:

This problem requires the use of hindcast frequencies from interval table which summarizes seasons. We proceed following the steps outlined in Question 2. Step 1. Compute the percent of <12 ft waves that lasted >2 days. This requires estimation of the total number of hindcasts meeting this criterion. Estimation is necessary because beyond one day, the 0.25 day resolution of the hindcasts is lost in the summary process, so we must approximate the average number of hindcasts per interval. Since the 1 to 2 day interval includes episodes consisting of 1.25, 1.5, 1.75 and 2 days (that is 5, 6, 7, and 8 hindcasts), the average hindcasts per interval is

0.25 d 0.50 d

Interv

0.75 d 1 day 1-2 da which normally of days. On an exercises be aducted at the

sires the use of ncies from the which summarizes We proceed eps outlined in p 1. Compute the ft waves that This requires e total number of g this criterion. ecessary because , the 0.25 day he hindcasts is ary process, so at the average sts per interval. 2 day interval s consisting of and 2 days (that 8 hindcasts), the s per interval is 6.5. In this example it will be easier and more accurate to find the percent for ≤ 2 days then subtract from 100 to obtain the percent we require. The procedure is as follows:

Interval	Hindcasts per Interval		equency rom Tab		Hindcasts Not ≥12 Ft Lasting ≤2 Days
0.25 day	1	х	53	=	53
0.50 day	2	X	34	-	68
0.75 day	3	X	25	=	75
l day	4	X	15	=	60
1-2 days	6.5	X	52	=	338
		TO	TAL:		594

Thus, the percent of $\langle 12 \rangle$ foot waves that lasted $\langle 2 \rangle$ days is $(594 -9056) \times 100\% = 6.6\%$. The percent of $\langle 12 \rangle$ foot waves that lasted $\langle 2 \rangle$ days is 100% - 6.6% = 93.4%.

Step 2. The percent of waves <12 ft is (T*/TH) X 100% or (10761-13606) X 100% = 79.1%. Step 3. The answer is 93.4% X

79.1% = 73.9%.

- P.

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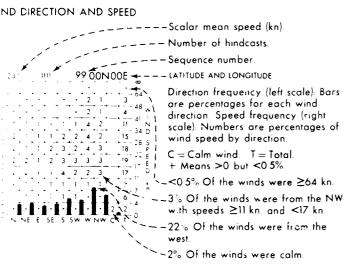
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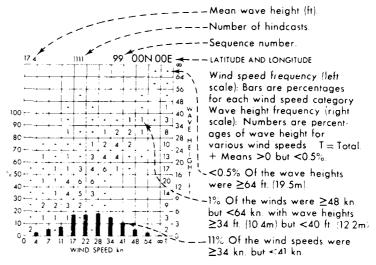
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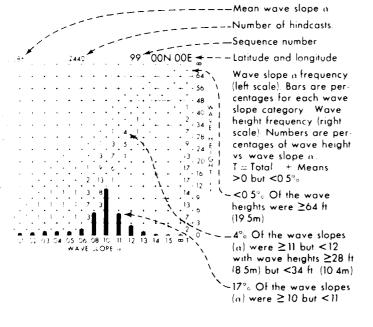
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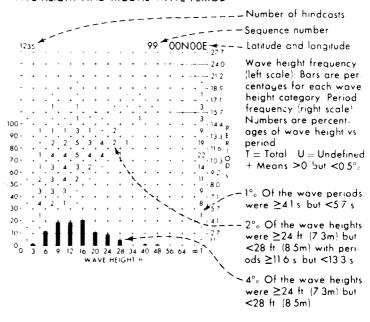
WAVE HEIGHT AND WIND SPEED



AVE HEIGHT AND WAVE SLOPE a

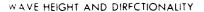


WAVE HEIGHT AND MODAL WAVE PERIOD



feet 0 3 6 12 20 28 34 40 48 56 64 meters 0 1837 61 85 122 146 171 195

10F 5



----Mean directionality

___Number of hindcasts

-Sequence number

Latitude and longitude

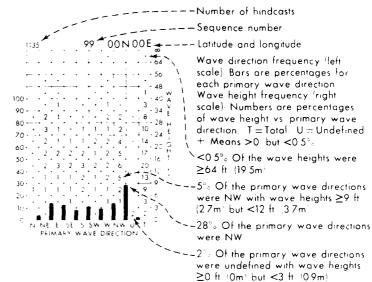
Directionality frequency (left scale): Bars are percentages for each directionality category. Wave height frequency (right scale): Numbers are percentages of directionality values vs. wave height T=Total. + Means > 0 but < 0.5%.

<0.5° Of the wave heights were ≥64 ft 19.5m²

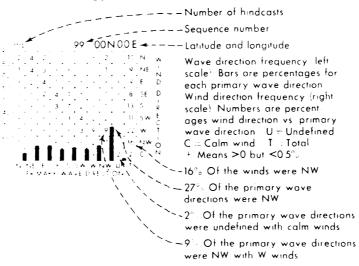
-12. Of the directionality values were ≥95 but ≤100 with wave heights ≥9 ft (27m) but <12 ft (37m) and 2% of the directionality values were ≥90 but <95

-28° of the directionality values were ≥85 but <90

WAVE HEIGHT AND PRIMARY WAVE DIRECTION



PRIMARY WAVE DIRECTION AND WIND DIRECTION



feet 0 3 6 12 20 28 34 40 48 56 64 meters 0 18 37 61 85 12 2 14 6 17 1 19 5 0 9 2 7 4 9 7 3 10 4

2 OF 5

WIND SPEED DURATIONS- SEASONAL

LATITUDE AND LONGITUDE SEQUENCE NUMBER 1235 ≥ 48 24.2 21. 48.1 39. 78.1 79. 96.2 101. 38 105 231 105 1235 236 1235 1 1 4 7 5 3 7811 /7 - 2 2 96 2 T i01 440 4 5 144 1 114 656 2 3 15 354 1 107 945 1 3 26 SEA 2 77 1078 25 SEA 2 4 1 1336 7 3 6 5 9 6 14 8 2 5 2 3 § ≥ 28 440 656 656 945 959 1078 1153 1273 1483 1483 1483 1483 4 3 4 2 5/12 18 24 30 36 42 54 60 66 72 78 84 90 96-

-1 Event with wind speeds ≥7 kn. persisted 12 hours; 26 events persisted ≥96 hours.

The longest event with wind speeds ≥7 kn. persisted for 1 season or more and it occurred 2 times. ——————— The longest event with wind speeds ≥48 km. persisted 18 hours / and it occurred 1 time ----

4) Events had wind speeds ≥4 kn. which comprised a total of 1,336

1,483 Hindcasts were examined, and 1,443 had wind speeds ≥4 kn ×

Durations for a particular season extend from the time the event begins (or the first day of the season if already in progress), and terminate when the event ends. Events become undefined if missing data is encountered. Durations lasting a season or more are categorized together. Durations may persist into the next season

WAVE HEIGHT INTERVALS - SEASONAL

SEQUENCE NUMBER LATITUDE AND LONGITUDE w 256 A 248 340 ≥54 1 2 1 4 3. 1. 3. 6. 2. 4.4 5. 4. 3. 5. 8. 3.4.3.8 o. HOURS INTERVALS BETWEEN EVENTS 24 30 36 There were 13 12 hour intervals between events of wave heights ≥9 ft (27m), 4 intervals persisted 96 hours or more

The longest interval between events of wave heights ≥6 ft (1.8m) was 132 hours and it occurred 1 time — -The longest interval between events of wave heights ≥64 ft. (19.5m) was 1 season or more and it occurred 9 times.—

There were 13 intervals between events of wave heights ≥3 ft (0.9m) which comprised a total of 23 hindcasts --

1,235 Hindcasts were examined, and 23 had wave heights <3 ft

Intervals for a particular reason extend from the time the event ends (or the first day of the season if the event is not in progress), and terminate when the event begins. Intervals become undefined if missing data is encountered. Intervals lasting a season or more are categorized together. Intervals may persist into the next season

WIND SPEED INTERVALS - SEASONAL

3EA 9 9 9 11 SEA 10 14 14 15 16 16 16 17 17 17 18 18 SEA 01 30 27 384 1 89 4 13 324 1 SEQUENCE NUMBER LATITUDE AND LONGITUDE 9 1116 1235 1235 14 1298 1364 1373 1 2 1 2 1 1 3 1 4 1 3 9 4 3 4 2 2 7 10 6 6 7 10 6 5 7 3 2 6 5 1 1 ≥ 48 ≥ 41 ≥ 34 1298 2 41 2 34 3 4 10 4 222 10 14 11 13 2 2 22 10 14 11 13 2 E ≥ 17 14 18 18 16 17 D ≥ 11 23 27 17 22 17 22 17 23 4 2 1 5 4 1 6 7 12 18 24 1. 2. 2. 2. 1540 1435 617 617 108 1 103 36 1 68 18 IN 32 18 24 30 36 42 48 54 60 66 72 78 84 90 96 HOURS INTERVAL BETWEEN EVENTS

There were 18 12-hour intervals between events of wind speeds ≥17 kn., 4 intervals persisted 96 hours or more

The longest interval between events of wind speeds ≥7 km was 36 hours and it occurred 1 time. -The langest interval between events of wind speeds ≥64 kn. was 1 season or more and it occurred 9 times.——

There were 32 intervals between events of wind speeds ≥4 kn which comprised a total of 40 hindcasts. ---

1,235 Hindcasts were examined, and 40 had wind speeds <4 kn

Intervals for a particular season extend from the time the event ends (or the first day of the season the event is not in progress), and terminate when the event begins. Intervals become undefined if missing data is encountered. Intervals lasting a season or more are categorized together. Intervals may persist into the next season

WAVE SLOPE a DURATIONS - SEASONAL

LATITUDE AND LONGITUDE > 13 20.20.00 4 10 3 9. 3. 3. 4. 2. ISEA 50 | SEA 43 | SEA 30 ISEA ISEA

 \sim 2 Events with $\alpha \geq$ 002 persisted 12 hours, 30 events persisted ≥96 hours

The longest event with $a \ge 0.13$ persisted 18 hours and it occurred,

The longest event with it ≥0.02 persisted for 1 season or more and it occurred 14 times -----

24 Events had $\alpha \ge 0.01$ which comprised a total of 2.477 hindcasts 2 2,659 Hindcasts were examined, and 2,641 had $\alpha \ge 0.01 = -$

Durations for a particular season extend from the time the event begins (or the first day of the season if already in progress and termi nate when the event ends. Events become undefined it missing data is encountered. Durations lasting a season or more a e-categorized together. Durations may persist into the next season

ABBREVIATIONS (See text for details)

MAX Maximum duration or interval, followed by the number of occurrences

TE or TI Total number of events or intervals

T. Total number of hindcasts included in TE or TI

Total number of hindcasts that met the stated criteria

TH Total number of hindcasts examined

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SPEED INTERVALS - SEASONAL

	1. ENTE NUMBER	LATITUDE	AND LONGITU	UD
			1116 1235 12	
				373
		SEA 61 30		591 540
	1 1 1 3 1 4 1 3 1 1 2 3 22 4 5 7 4 3 4 2 2 3 2 1 1 3 27	3841, 88		360
	4 1 13 7 10 8 8 7 1 2 2 4 13	324 1 [106]		288
71	(1) - 1 (6) (6) (10) (6) (5) (7) (3) (2) (2) (3) (1) (2) (2) (4)	240 1 113		264
		108 1 103 36 1 68		235 235
٠.		18 1 32		35
- :	4 30 36 42 48 54 50 66 72 78 84 90 96	MAX 🖥 TI🎉	ा कें ा∗कें।	TH Å
4 E	HOURS NITERVAL BETWEEN EVENTS	1	1, 1	. ;
9 ∨ €		\	- ' ' ' ' '	λi
Tr 4				Ì
eai	iere were 18 12-hour intervals between events	of wind	sneeds 11	١
	17 kn 4 intervals persisted 96 hours or more.	0	Vi special	١
			/ \	1
	- longest interval between events of wind spe	eds ≥7 k	<u>'n / </u>	j
	36 hours and it occurred 1 time. —————			i
), ,	e langest interval between events of wind spe	eds ≥64	kn. was j	Ĥ
645	eason or more and it occurred 9 times — — —			/
	ere were 32 intervals between events of wind	speeds ?	≥4 kn ∕ ́	!
	ch comprised a total of 40 hindcasts. ———			/
	35 Hindcasts were examined, and 40 had win	id speeds	s <4 kn '	•
	ervals for a particular season extend from the			
iat į	e first day of the season the event is not in	nno me	s) and term	ni.
ate,	when the event begins. Intervals become a	indefined	if missing	
	encountered Intervals lasting a season	or more	are	
Έ,	sprized together Intervals may persist into	the next	season	

.. OPE IL DURATIONS SEASONAL

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with in ≥0.02 persisted 12 hours, 30 events persisted The of hours sea ingest event with $a \ge 0.13$ persisted 18 hours and it occurred. orgest event with a ≥0.02 persisted for 1 season or more andirred 14 times -----Inte^{1,1} rents had a ≥0.01 which comprised a total of 2,477 hindcasts ⁷ > tindeasts were examined, and 2,641 had a ≥0.01 = --it or s for a particular season extend from the time the event 400 or the first day of the season if already in progress, and termi when the event ends. Events become undefined if missing data

sontered. Durations lasting a season or more are categorized

LATITUDE AND LONGITUDE

O 3/4 Durations may persist into the next season " in number of occurrences

30F5

WAVE HEIGHT DURATIONS - SEASONAL		
SEQUENCE NUMBER	LATITUDE AND LONGITUDE	
≥64	1235	
/ ≥56	1235	
≥48	1235	
^ ≥40, 1	61 1 1235	
≥34, 2, . 2, 1,	24 1 5 12 12 1235	
!≥28, 3, 2, 1, 1, . , 2, . , , ,		
'≥24, 3, 7, 2, 4, 1, 2,, 2,,	•	
$\frac{1}{2}$ $\frac{2}{2}$ $\frac{2}{7}$ $\frac{2}{7}$ $\frac{2}{7}$ $\frac{2}{7}$ $\frac{2}{7}$ $\frac{2}{7}$ $\frac{2}{7}$ $\frac{2}{7}$ $\frac{1}{7}$ $\frac{1}{7}$ $\frac{1}{7}$ $\frac{2}{7}$ $\frac{2}{7}$ $\frac{2}{7}$ $\frac{2}{7}$ $\frac{1}{7}$ $\frac{1}{7}$ $\frac{1}{7}$ $\frac{1}{7}$ $\frac{1}{7}$ $\frac{2}{7}$ $\frac{2}{7}$ $\frac{2}{7}$ $\frac{2}{7}$ $\frac{1}{7}$ $\frac{1}{7}$ $\frac{1}{7}$ $\frac{1}{7}$ $\frac{2}{7}$ $\frac{2}{7}$ $\frac{2}{7}$ $\frac{2}{7}$ $\frac{1}{7}$ $\frac{1}{7}$ $\frac{1}{7}$ $\frac{2}{7}$ $\frac{2}{7}$ $\frac{2}{7}$ $\frac{2}{7}$ $\frac{1}{7}$ $\frac{1}{7}$ $\frac{1}{7}$ $\frac{2}{7}$ $\frac{2}{7}$ $\frac{2}{7}$ $\frac{2}{7}$		
l ≥16, 3, 8, 2, 6, 2, 5, 3, 2, 4, 2, 3, 3, 2,2		
≥ 12 , 9, 9, 8, 6, 2, 3, 4, 2, 2, 6, 4, 3, 2, 2, 10		
$\frac{3}{2}$, 4, 9, 7, 5, 5, 3, 4, $\frac{1}{2}$, $\frac{1}{2}$, $\frac{1}{2}$, $\frac{1}{2}$, $\frac{18}{2}$	· · · · · · · · · · · · · · · · ·	
6/12 18 24 30 36 42 48 54 60 66 72 78 84 90 96.	I WAY MIEK TE IN K IHA	
·		
~4 Events with wave heights ≥6 ft. (1.8m) persis	ted 12 hours; 22 \ \ \	
events persisted ≥96 hours.	11 11	
evenis persisted _/o noors.	11 1/	
The langest event with wave heights ≥3 ft. (0.9	CE NUMBER LATITUDE AND LONGITUDE 1235	
	22-1	
	z.zm) persisted for j i	
6 hours and it occurred 1 time.—————		
22 Events had wave heights >3 ft (0.9m) which	h comprised a total	
	The comprised distally	
0, 1,024 minucusis. — — — — — — — — — — — — — — — — — — —		
1.649 Hindcasts were examined, and 1.626 had	l wave heights ≥3 ft /	
(0 9m)		
10 /m/		

Durations for a particular season extend from the time the event begins (or the first day of the season if already in progress), and terminate when the event ends Events become undefined if missing data is encountered. Durations lasting a season or more are categorized together. Durations may persist into the next season

WAVE SLOPE & INTERVALS . SEASONIAL

AV	SEQU	-					٧A	15	٠ 5	ŁΑ	50	N	٩L						r t T	IDE	AND	IONO	SITUDE
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2.15		+		- •		- •																	2558
? 14																						2661	2663
5 13			١.	١.								٦.						EA			2657		
≥ 10	. 1.	3.	2.	. 1.	4.			١.		١.		٦,	-1,	- 1		38	1	SE A	9.	54.	2708	2922	3012
3 11	. 12.	8.	3.	6	5.	5	١.	4.	2.	١.	2_	_5_		3	4	44		SEA	2	105			27.40
5 10	. 6	7.	15	11	7	4.	8		6.	3.	5	4	5.	5	,	34	Ľ	474	1	143	1755	1825	2616
≥ 08	23	18	10	13	7.	10	5	6	4	2	3	1	2	4	- 1	9	1	348	1	118	762	778	2496
3.06	21	18	18	8	4	3	2		2	4		- 1	2	- 1		_ 2	2.	150	ΠŢ	86	346	355	2450
. 95	25.4		12]	4	. 4	2	2	2	3	2	2		- :	_			.;	66	2	77	246		2445
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1.03	_20.i	8	5	4	3	-1.		1.	-		خدر		•	•			7	48	1	42	96	96	2442
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2.01			•	•	1	- 1		أنمر		•	•	•	•				*†	36		6	12	12	2440
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slopes ≥006, 2 intervals persisted 96 hours or more.

The longest interval between events of wave slopes ≥010 was 474 hours and it occurred 1 time ---The longest interval between events of wave slopes ≥015 was 1 season or more and it occurred 18 times --

There were 6 intervals between events of wave slopes ≥001 which comprised a total of 12 hindcasts

2,440 Hindcasts were examined, and 12 had wave slopes <0.01.-

Intervals for a particular season extend from the time the event ends (or the first day of the season if the event is not in progress), and terminate when the event begins. Intervals become undefined if missing data is encountered. Intervals lasting a season or more are categorized together. Intervals may persist into the next season

feet 0 3 6 12 20 28 34 40 48 56 64 meters 0 18 37 61 85 12 2 14 6 17 1 19 5

WIND SPEED DURATIONS - ENTIRE DATA SET

LATITUDE AND LONGITUDE SEQUENCE NUMBER 3 00 1 173 3 50 1 385 17 Events with wind speeds ≥4 kn. persisted 0.5 day; 57 events persisted >1 day but ≤2 days

The longest event with wind speeds ≥41 kn. persisted 1.75 days

and it occurred 2 times ---The longest event with wind speeds ≥34 kn. persisted 3 days and it occurred 1 time. - - -

442 Events had wind speeds ≥4 kn. which comprised a total of 12.384 hindcasts -----

13,606 Hindcasts were examined, and 12,640 had wind speed

Durations extend from the time the event begins and terminate when the event ends. Events become undefined if missing data is encountered

WAVE HEIGHT INTERVALS - ENTIRE DATA SET

	SEQUENCE NUMBER LATITUDE AND LO														LONG	HUDE					
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> . 4	3	4	75	٠,	5	7	3	` ?'	13	12	4	-11	1.	•	5	١	338 00	1 76	9465	13334	13606
3.0	7	8	7.	2	16	14	10	6	18	20	-11	0	1.	3	5	ì	232 25			12937	
2.0	18	17	116	6	32	26	13	14	33	31	11	4		2	2	1	205 75	1 226	9023	12204	13606
200	53	34	125	15	52	50	22	23	40	29	7	7	3	2	- 1	1	18075	1363	9056	10761	13606
76	` 57°	45	32	36	93	49	28	16	34	24	8	7	3	2		1	128 50	1 434	8187		13606
2.5	72	56	739	46	92	47	21	17	40	35	6	4	·	Ī	•	1	50 50	1,475	6395		13606
: 1	73	67	35	31	85	35	24	17	26	8	•			•	•		18 25	2 401	3133	3208	13606
	2.5	5	175	7	` :			. :	18	2	0 30	06.0	90	180	: 36	0 0	XAMJO	≯ 11,	K 1 >	€ T#`	¥ 1HΥ
DAYS INTERVAL BETWEEN EVENTS												\ \ \ \									

1 Interval between events of wave heights ≥34 ft. (10 4m) persiste 0.5 day, 2 intervals persisted >1 day but \le 2 days.

The longest interval between events of wave heights ≥3 ft (09m) was 18 25 days and it occurred 2 times - --The longest interval between events of wave heights ≥40 ft

was 308 25 days and it occurred 1 time.

There were 401 intervals between events of wave heights ≥3 ft (0.9m) which comprised a total of 3,133 hindcasts:

13,606 Hindcasts were examined, and 3,208 had wave heights <

Intervals extend from the time the event ends and terminate when the event begins. Intervals become undefined if missing data is encountered

WIND SPEED INTERVALS - ENTIRE DATA SET

SEQUENCE N	UMBER						LATITUDE	AND LON	
W≥64						2 2 2	8 ÖÖ İ 13		13606
	A ". '.					2, 2,411	0001.13	5944 1357	4 13000
N ≥ 41 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	/1 <u>1</u> 10, 4,	4, 1,	12 11	5 6	3	1 32	4001.58	8829 1347	5 13606
≥34 9 7 5 V	6, 22, 15,	19. 4.	30 27	9 7	2. 1	4 20	8 50 1, 167	9580_1317	3 13606
S ≥ 28 33 34 20 2	26 61 43	34 25	46_38	7 7	2 3	1, 18	1751 380	10399 1246	5 13606
≥ 22 68 63 38 5		44, 27	55 32	9 4	5_2	- 11	5751 613	10594 1107	0 13606
€ ≥17 113 98 103 7	75 197 96	42 24	67_36_	6 2		5	0251 859	8875 900	1 13606
D ≥11 210 180 150 10		38 24	20 6			16	5251 988	5108 513	4 13606
≥7 316 182 104 6	52 90 25	12 3	4				75 2 798	2376 238	7 13606
n ≥4 255 106 30 1	15 35 8	1	1				5 25 1 451	963 96	6 13606
25 5 75 1	1 2 3	4 5	10 20	30 60		360 m	AAX TI	R T] k T#	THE
		D,	ays inter	RVAL BE	TWEEN	EVENTS.		\ \	'. T
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1 Interval between events of wind speeds ≥48 km. persisted 0.5 day; 4 intervals persisted >1 day but ≤2 days.

The longest interval between events of wind speeds ≥4 kn. was 6.25 days and it occurred 1 time. --The longest interval between events of wind speeds ≥7 kn. was 8.75 days and it occurred 2 times. — —

There were 451 intervals between events of wind speeds ≥4 kn which comprised a total of 963 hindcasts.

13,606 Hindcasts were examined, and 966 had wind speeds <4 kn

Intervals extend from the time the event ends and terminate when the event begins. Intervals become undefined if missing data is encountered

WAVE SLOPE a DURATIONS - ENTIRE DATA SET

					_			
SEQUENCE	NUMBER					LATITUDI	AND LON	GITUDE
≥ 15 2 3						50 3 5	8 8	29016
≥ 14 12 5 3						75.3 20	31 3	29016
w ≥ 13 [25] 15 15	5 4					150 2 64	142 145	29016
A ≥ 12 48 47 32		1			• •	. 🗷 3 25 1 [180	525 53	29016
V ≥ 11 120 76 47		3 3				4 25 3 430	1633 1648	3 29016
≥ 10 210 139 104		31 15 16		-• •	7	9 50 1 878	4415 4450	29016
5 ≥ 08 216 128 104				• •		23 75 1 1411	14261 14460	29016
2 06 124 104 76				5 .	1	35 50 1 1311	20361 2090-	4 29016
P 2 05 135 81 70	55 200 138	110, 94 192	100 24	12	1	43 00 1 1211	21835 22909	29016
E ≥ 04 120 75 60					1	58 50 1 1111	22954 2442	29016
n ≥ 03 94 58 45					•	67751 895	23326 2566	3 29016
> 02 69 42 29	1. 64 46	51 32 106	68 44	34 9	1 .	7 90 75 1 613	22003 2690	5 29016
> 01 32 15, 11	3 19 10	15 10 34	40 13.	45 17		1 1361 75 1 267		
25 5 75		4 5 1	0 20 3	0 60 90	180 360	COLMAX TE	√ 1 √ 1 ₹	₹ TH¥
/	/	Da	YS DUR	ATION C	OF EVENTS	` \	1, 1	1

32 Events with $\alpha \ge 0.01$ persisted .25 day; 19 events persisted > day but ≤2 days.

The longest event with $\alpha \ge 0.12$ persisted 3.25 days and it occurred 1 time --The longest event with $\alpha \ge 0.13$ persisted 1.50 days and it occurred

267 Events had a \geq 0.01 which comprised a total of 20,760 hindcasts -----

29,016 Hindcasts were examined, and 28,054 had a ≥0.01

Durations extend from the time the event begins and terminate when the event ends. Events become undefined if missing data is encountered

ABBREVIATIONS (See text for details)

MAX Maximum duration or interval, followed by the number of occurrences

TE or Ti Total number of events or intervals

Total number of hindcasts included in TE or TI

Tw. Total number of hindcasts that met the stated criteria

TH. Total number of hindcasts examined

4 OF 5

INTERVALS - ENTIRE DATA SET

: between events of wind speeds ≥48 km. persisted 0.5^N oversals persisted >1 day but ≤2 days.

gest interval between events of wind speeds ≥4 kn. was and it occurred 1 time = = =

which comprised a total of 963 hindcasts

indicasts were examined, and 966 had wind speeds <4 kn extend from the time the event ends and terminate when thegins. Intervals become undefined if missing data is

FE a DURATIONS - ENTIRE DATA SET

3.6

:3

ats with $\alpha \gtrsim 0.01$ persisted 25 day, 19 events persisted >1 ≤ 2 days

pest event with $\alpha \ge 0.12$ persisted 3.25 days and it

gest event with a ≥013 persisted 1.50 days and it occurred

s had $n \ge 0.01$ which comprised a total of 20,760.

imper of occurrences

WAVE HEIGHT DURATIONS - ETITIZE DATA SET

-33 Events with wave heights ≥3 ft. (0.9m) persisted 0.5 day; 68 events persisted >1 day but ≤2 days.

The longest event with wave heights \geq 24 ft. (7.3m) persisted 2.5 days and occurred 1 time.

393 Events had wave heights \geq 3 ft. (0.9m) which comprised a total of 10,094 hindcasts.

Durations extend from the time the event begins and terminate when the event ends. Events become undefined if missing data is encountered.

WAVE SLOPE a INTERVALS - ENTIRE DATA SET

-2 Intervals between events of wave slopes ≥0.13 persisted 0.5 day, 1 interval persisted >1 day but ≤2 days.

The longest interval between events of wave slopes ≥0.15 was 16.25 days and it occurred 1 time.

The longest interval between events of wave slopes ≥0.01 was 5.25 days and it occurred 2 times.

There were 286 intervals between events of wave slopes ≥ 0.01 , which comprised a total of 961 hindcasts.

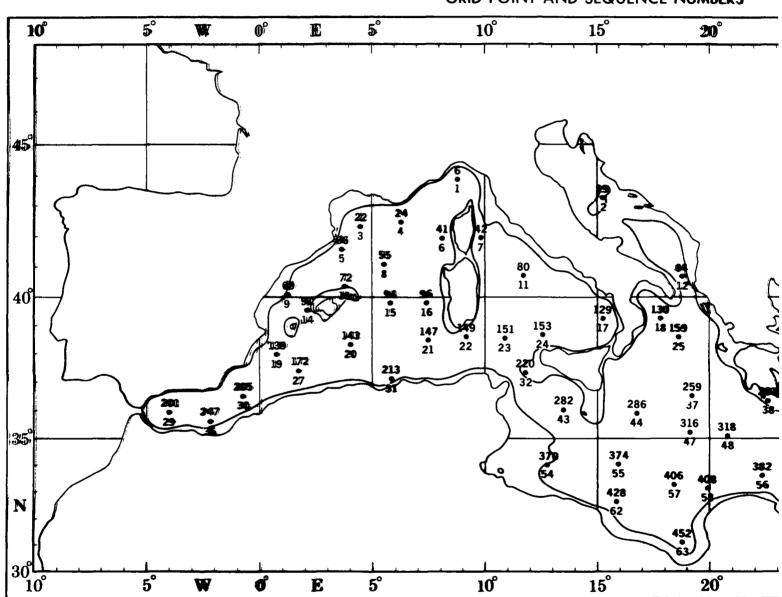
29,016 Hindcasts were examined, and 962 had wave slopes < 0.01

Intervals extend from the time the event ends and terminate when the event begins. Intervals become undefined if missing data is encountered.

feet 36 12 20 28 34 40 48 56 64 meters 0 18 37 61 85 122 146 171 195 0 9 27 4 9 7 3 10 4

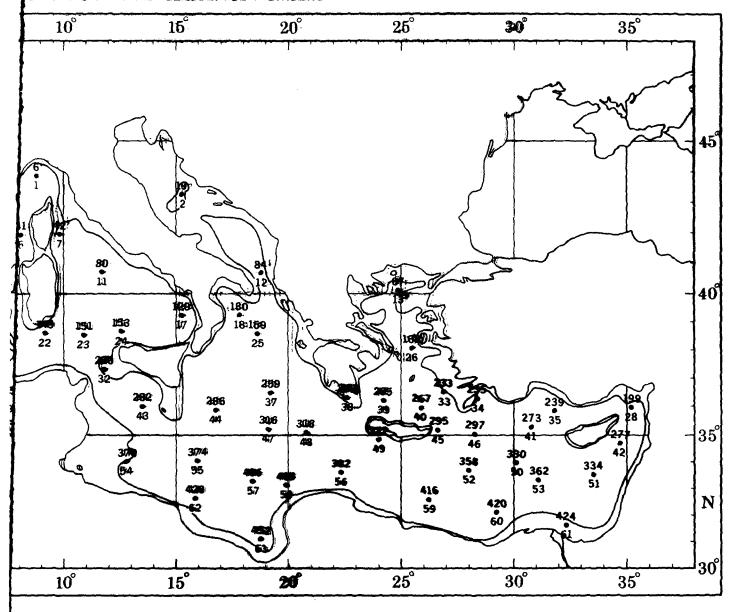
4 of 5

GRID POINT AND SEQUENCE NUMBERS



5 OF 5

GRID POINT AND SEQUENCE NUMBERS



5 OF 5